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APPENDICES

ศูนย์วิทยทรัพยากร จหาลงกรณ์มหาวิทยาลัย

APPENDIX A

SPECIFICATION OF ALUMINA SUPPORT (Al₂O₃) TYPE NKH-3

Table A.1 Chemical composition of alumina support type NKH-3

Chemical Composition	Weight percent
Al ₂ O ₃	60-70
SiO ₂	30-35
Fe ₂ O ₃	0.3-0.5
TiO ₂	0.5-0.7
CaO	0.1-0.2
MgO	0.2-0.4
Na ₂ O	0.3-0.4
K ₂ O	0.2-0.3
$ZrO_2 + HfO_2$	0.03-0.04

Table A.2 Physical properties of alumina support type NKH-3

Physical properties				
Bulk Density (g/ml)	1.3-1.5			
Apparent Specific Gravity	3.1-3.3			
Packing Density (lb/ft ³)	20-25			
Pore Volume (ml/g)	1.0-1.3			
Surface Area (m ² /g)	340-350			

APPENDIX B

CALIBRATION CURVES

The thermal conductivity detectors (TCD) independently connected with two gas chromatographs (SHIMADZU GC-8ATP and SHIMADZU GC-8AIT) were used to analyze the concentration of the sampling gases in the catalytic activity test and an experimental set for studying the nature of surface species. The calibration curves of oxygen, nitrogen and carbon monoxide are obtained from TCD of GC 8ATP whereas those of oxygen, methane, carbon dioxide, nitrous oxide, propene, propane and sulfur dioxide are obtained from TCD of GC 8AIT. It is noted that the operating condition of gas chromatograph for making the calibration curves is maintained to be similar to that for testing the reaction. These calibration curves are given in Figures B.1-B.10.

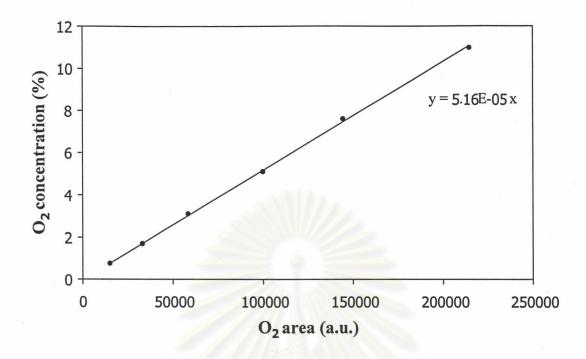


Figure B.1 The calibration curve of oxygen from TCD of GC 8ATP

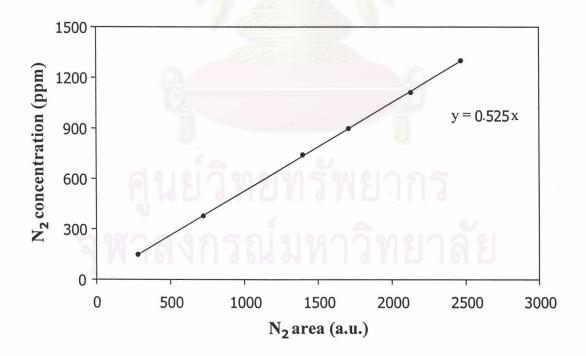


Figure B.2 The calibration curve of nitrogen

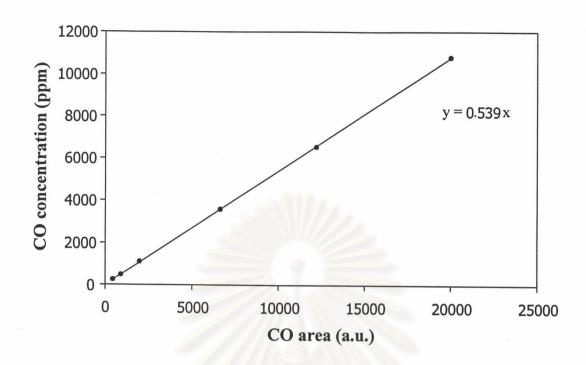


Figure B.3 The calibration curve of carbon monoxide

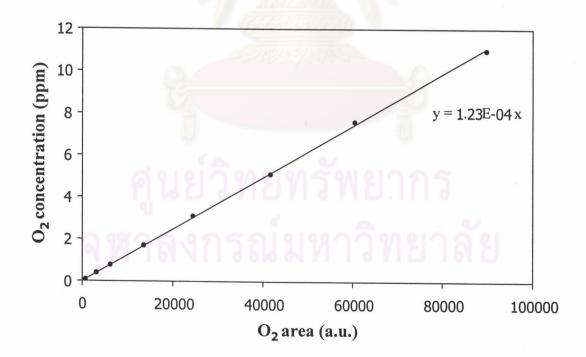


Figure B.4 The calibration curve of oxygen from TCD of GC 8AIT

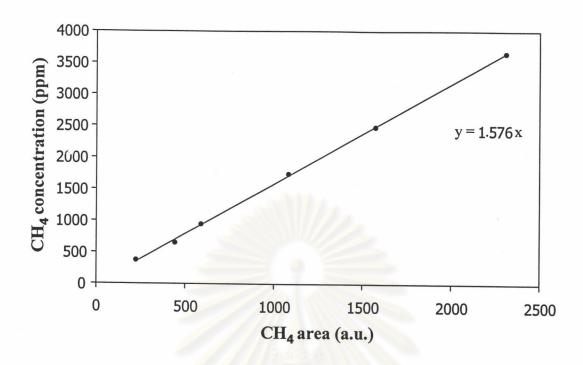


Figure B.5 The calibration curve of methane

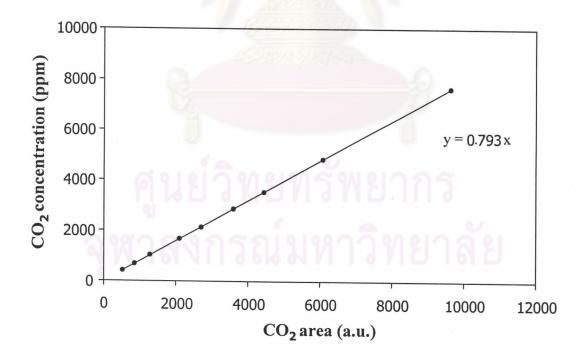


Figure B.6 The calibration curve of carbon dioxide

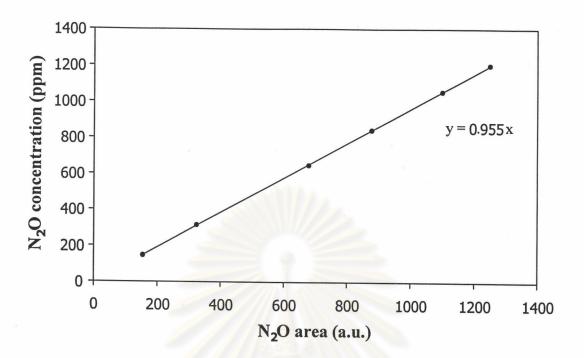


Figure B.7 The calibration curve of nitrous oxide

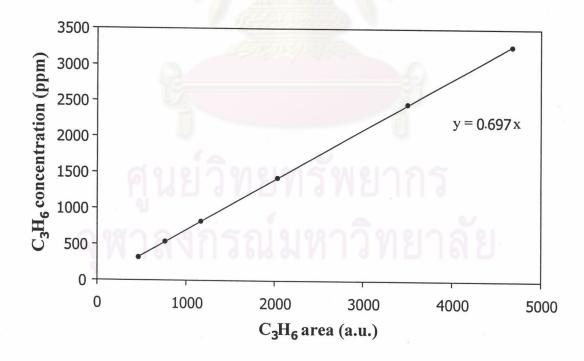


Figure B.8 The calibration curve of propene

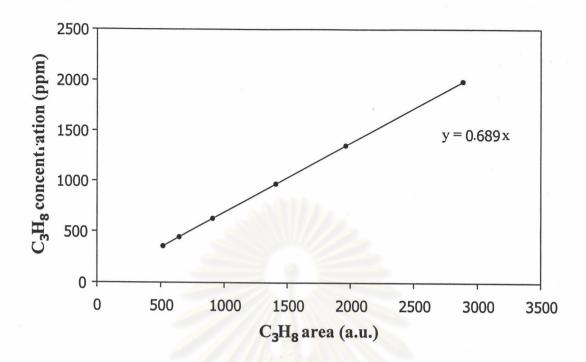


Figure B.9 The calibration curve of propane

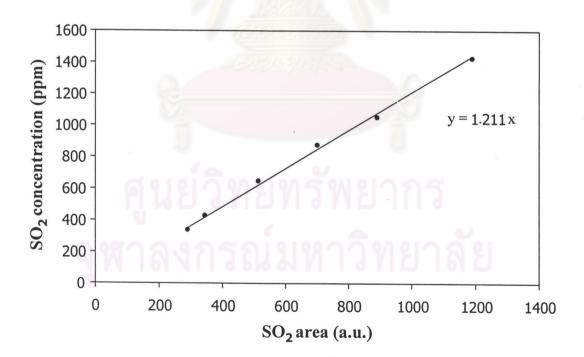


Figure B.10 The calibration curve of sulfur dioxide

APPENDIX C

SAMPLES OF CALCULATION

C.1 Calculation of Catalyst Preparation

The sample calculation shown below is for 1 wt% Pt -2 wt% M/Al₂O₃ (M = Li, Cr, Fe, Ni, Ga, Co, Sn or W). The hydrochloric acid is only added to the impregnation solution by 5%wt of the alumina support in case of the use of Sn as the second metal. The alumina support weight used for all preparations is 2 g.

If X g of the alumina support is used, so each 100 g of the catalyst is composed of

	Platinum	1	g
	Second metal (M)	2	g
	Alumina support	X	g
Then		1 + 2 + X = 100	g
		X = 97	g

In case of 1 wt% Pt - 2 wt% Sn/Al₂O₃ catalyst, if X g of the alumina support is used, so each 100 g of this catalyst is composed of

	Platinum	1	g
	Tin	neign Soulei 2 5	g
	Hydrocholoric acid	0.05×X	g
	Alumina support	\mathbf{x}	g
Then		$1 + 2 + 0.05 \times X = 100$	g
		X = 92.38	g

The platinum and the second metals are obtained from the different metal precursors; therefore, the real metal contents in each metal precursor are shown in Table B.1. It is remarked that the stock solution of chloroplatinic acid hexahydrate has the concentration of 1 g in 25 ml of water and concentration as well as density of hydrochloric acid solution is 37%v/v and 1.19 g/ml, respectively.

Table C.1 The actual metal contents in various metal precursors used in this work

Metal MW of metal Metal precurso	MW of	Metal proguracy	MW of metal	Purity	Metal
	ivietal precursor	precursor	(%)	Content (%)	
Pt	195.080	H ₂ PtCl ₆ ·6H ₂ O	517.90	98.5	37.10
Li	6.941	LiNO ₃	68.94	95.0	9.56
Cr	51.996	Cr(NO ₃) ₃ ·9H ₂ O	400.15	97.0	12.60
Fe	55.847	Fe(NO ₃) ₃ ·9H ₂ O	404.02	99.0	13.68
Ni	58.690	Ni(NO ₃) ₂ ⋅6H ₂ O	290.81	99.0	19.98
Ga	69.720	Ga(NO ₃) ₃	255.70	100.0	27.27
Co	58.933	Co(CH ₃ COO) ₂ ·4H ₂ O	249.08	99.0	23.42
Sn	118.710	SnCl ₂ ·2H ₂ O	225.63	97.0	51.03
W	183.850	(NH ₄) ₁₀ H ₂ (W ₂ O ₇) ₆	3060.59	99.0	71.36

The calculation procedure of the amount of each ingredient for the required composition of 1 wt% Pt - 2 wt% M/Al₂O₃ catalyst is shown in an example of 1 wt% Pt - 2 wt% Sn/Al₂O₃ catalyst as follows:

For 2 g of the alumina support used:

1. Platinum required
$$= (1\times2)/92.38$$
 g
 $= 2.165\times10^{-2}$ g
Chloroplatinic acid hexahydrate required
 $= 2.165\times10^{-2}\times100\times25/37.10$ ml
 $= 1.459$ ml

2. Tin required $= 2\times2/92.38$ g
 $= 4.33\times10^{-2}$ g
Stannous chloride dihydrate required
 $= 4.33\times10^{-2}\times100/51.03$ g
 $= 0.0849$ g

3. Hydrochloric acid and solution required

$$= 2 \times 0.05$$
 g

$$= 0.1$$
 g

The amount of hydrochloric and by volume

$$= 0.1/(1.19 \times 0.37)$$
 ml

$$= 0.227$$
 ml

As the pore volume of the alumina support is 1 ml/g, the total volume of impregnating solution that must be used is 2 ml by the requirement of dry impregnation method. The de-ionized water is added until the volume of impregnating solution is 2 ml as equal to the volume of the alumina pore volume.

For the other catalysts, the calculation procedure is similar to that of 1 wt% Pt -2 wt% Sn/Al₂O₃ catalyst, except no addition of Hydrochloric acid.

C.2 Calculation of Specific Surface Area

From Brunauer-Emmett-Teller (BET) equation

$$\frac{p}{n(1-p)} = \frac{1}{n_m C} + \frac{(C-1)p}{n_m C}$$
 (C.1)

Where, $p = Relative partial pressure of adsorbed gas, P/P_0$

P₀ = Saturated vapor pressure of adsorbed gas in the condensed state at the experimental temperature, atm

P = Equilibrium vapor pressure of adsorbed gas, atm

n = Gas adsorbed at pressure P, ml. at the NTP/g of sample

 n_m = Gas adsorbed at monolayer, ml. at the NTP/g of sample

 $C = \operatorname{Exp} \left[(H_{C} - H_{I}) / RT \right]$

 H_C = Heat of condensation of adsorbed gas on all other layers

 H_1 = Heat of adsorption into the first layer

Assume $C \rightarrow \infty$, then

$$\frac{p}{n(1-p)} = \frac{p}{n_m}$$

$$n_m = n(1-p)$$
(C.2)

The surface area, S, of the catalyst is given by

$$S = S_b \times n_m \tag{C.3}$$

From the gas law

$$\frac{P_b V}{T_b} = \frac{P_t V}{T_t} \tag{C.4}$$

Where, $P_b = Pressure at 0^{\circ}C$

 P_t = Pressure at t°C

 $T_b = Temperature at 0°C = 273.15 K$

 T_t = Temperature at t°C = 273.15 + t K

V = Constant volume

Then, $P_b = (273.15/T_t) \times P_t = 1 \text{ atm}$

Partial pressure

$$P = \frac{[Flow of (He + N2) - Flow of He]}{Flow of (He + N2)}$$

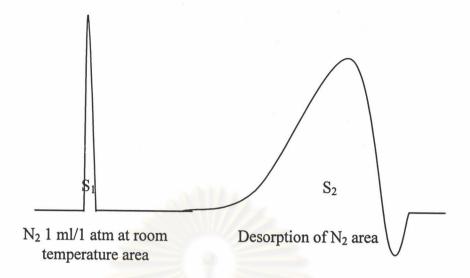
$$= 0.3 atm$$
(C.5)

For nitrogen gas, the saturated vapor pressure equals to

$$P_0 = 1.1 atm$$

then,
$$p = P/P_0 = 0.3/1.1 = 0.2727$$

To measure the volume of nitrogen adsorbed, n



$$n = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \text{ ml./g of catalyst}$$
 (C.6)

Where, $S_1 = N_2 1 \text{ ml/1 atm}$ at room temperature area

 S_2 = Desorption of N_2 area

W = Sample weight, g

T = Room temperature, K

Therefore,

$$n_{m} = \frac{S_{2}}{S_{1}} \times \frac{1}{W} \times \frac{273.15}{T} \times (1-p)$$

$$n_{m} = \frac{S_{2}}{S_{1}} \times \frac{1}{W} \times \frac{273.15}{T} \times 0.7272$$
(C.7)

Whereas, the surface area of nitrogen gas from literature equal to

$$S_b = 4.373 \text{ m}^2/\text{ml} \text{ of nitrogen gas}$$

Then,

$$S = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \times 0.7272 \times 4.343$$

$$S = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \times 3.1582 \text{ m}^2/\text{g}$$
(C.8)

C.3 Calculation of Metal Active Sites

To calculate the metal active sites of the catalyst measured by CO adsorption technique at room temperature, the following procedure is shown:

Let the weight of ca	atalyst used	= W	g
Integral area of CO peak after adsorption		= A	unit
Integral area of 50 µ	ul of standard CO peak	= B	unit
Amounts of CO ads	sorbed on catalyst	= B-A	unit
Volume of CO adso	orbed on catalyst	$= [(B-A)/B] \times 50$	μl
Volume of 1 mole of	of CO at 30°C	$= 24.86 \times 10^6$	μl
Mole of CO adsorbed on catalyst		$= [(B-A)/B][50/24.86 \times 10^6]$ mole	
Molecule of CO add	sorbed on catalyst		
	$= [2.01 \times 10^{-6}][(B-A)/B][$	6.02×10^{23}] molecule	S
Metal active sites	$= 1.21 \times 10^{18} [(B-A)/B][1/B]$	W] molecules of CO	D/g of catalyst

In addition, the platinum dispersion, which is the ratio between the apparent platinum molecules observed from the measurement of CO adsorption and the actual platinum molecules obtained from the measurement of atomic absorption spectroscopy, can also be calculated.

Example of the calculation of metal active sites and metal dispersion is shown as follows:

For 1 wt% Pt/Al₂O₃ catalyst,

The weight of catalyst used	= 0.1	g
Integral area of CO peak after 1st adsorption	n = 72	unit
Integral area of CO peak after 2 nd adsorption	n = 84	unit
Integral area of CO peak after 3 rd adsorption	n = 2269	unit
Integral area of 50 μ l of standard CO peak	= 2734	unit
Amounts of CO adsorbed on catalyst	= (3×2734)-72-84-22	69

= 5777

unit

μl

Volume of CO adsorbed on catalyst = $[5777/2734] \times 50$

= 105.65

Volume of 1 mole of CO at 30°C = 24.86×10^6 µl

Mole of CO adsorbed on catalyst = $[105.65/24.86 \times 10^6]$

 $=4.25\times10^{-6}$ mole

Molecule of CO adsorbed on catalyst

$$= [4.25 \times 10^{-6}] \times [6.02 \times 10^{23}]$$
 molecules

Therefore,

Metal active sites = $2.55 \times 10^{18} / 0.1$

 $=2.55\times10^{19}$

molecules of CO/g of catalyst

The actual percentage of platinum loading = 1 wt%

The actual platinum molecules = $0.01 \times 6.02 \times 10^{23}/195.08/0.1$

 $= 3.09 \times 10^{19}$ molecules/g of catalyst

Therefore,

The platinum dispersion = $2.55 \times 10^{19} \times 100/3.09 \times 10^{19}$

= 83

C.4 Calculation of NO and HC Conversions

In the catalytic activity test, the NO reduction and HC oxidation are evaluated in form of the conversions of NO and HC, respectively. Due to the lack of an instrument for directly detecting NO_x , NO conversion is calculated from N_2 and N_2O products analyzed by gas chromatographs. The following procedure is shown below:

The absolute NO conversion to N_2 and N_2O can be expressed as the reactions (C.9) and (C.10).

$$2NO \rightarrow N_2 + O_2 \tag{C.9}$$

$$4NO \rightarrow 2N_2O + O_2 \tag{C.10}$$

Therefore,

NO conversion to
$$N_2$$
 (%) = $(2[N_2]_{out}/[NO]_{in})\times 100$ (C.11)

NO conversion to N₂O (%) =
$$(2[N_2O]_{out}/[NO]_{in})\times 100$$
 (C.12)

Where,

 $[NO]_{in}$ = NO concentration in feed stream (ppm)

 $[N_2]_{out} = N_2$ concentration in product stream (ppm)

 $[N_2O]_{out} = N_2$ concentration in product stream (ppm)

From the calibration curves (Figures B.2 and B.7),

$$[N_2]_{out} = 0.525 \times [Area(N_2)]$$
 (C.13)

$$[N_2O]_{out} = 0.955 \times [Area(N_2O)]$$
 (C.14)

Where,

[Area(N_2)] = Area of N_2 peak from integrator plot on GC 8ATP

 $[Area(N_2O)] = Area of N_2O peak from integrator plot on GC 8AIT$

If the NO concentration in feed stream is equal to 1000 ppm (only used in this work),

NO conversion to
$$N_2$$
 (%) = $0.105 \times [Area(N_2)]$ (C.15)

NO conversion to
$$N_2O$$
 (%) = $0.191 \times [Area(N_2O)]$ (C.16)

The HC conversion is calculated as follows:

HC conversion (%) =
$$100 \times ([HC]_{in} - [HC]_{out})/[HC]_{in}$$
 (C.17)

Where,

 $[HC]_{in}$ = HC concentration in feed stream (ppm)

[HC]_{out} = HC concentration in product stream (ppm)

If $HC = C_3H_6$, from the calibration curves (Figure E.8),

$$[C_3H_6]_{in} = 0.697 \times [Area(C_3H_6)]_{in}$$
 (C.18)

$$[C_3H_6]_{out} = 0.697 \times [Area(C_3H_6)]_{out}$$
 (C.19)

Where,

 $[Area(C_3H_6)]_{in}$ = Area of C_3H_6 peak in feed from integrator plot on GC 8AIT $[Area(C_3H_6)]_{out}$ = Area of C_3H_6 peak in product from integrator plot on GC 8AIT

If the C₃H₆ concentration in feed stream is equal to 1000 ppm,

HC conversion (%) =
$$100 \times ([Area(C_3H_6)]_{in} - [Area(C_3H_6)]_{out})/[Area(C_3H_6)]_{in}$$
 (C.20)

Example,

$$[Area(N_2)] = 100$$

 $[Area(N_2O)] = 85$

If the NO concentration in feed stream is equal to 1000 ppm (only used in this work),

NO conversion to
$$N_2$$
 (%) = 0.105×100 = 10.5
NO conversion to N_2 O (%) = 0.191×85 = 16.2

Where,

$$[Area(C_3H_6)]_{in} = 1534$$

 $[Area(C_3H_6)]_{out} = 1128$

If the C₃H₆ concentration in feed stream is equal to 1000 ppm,

HC conversion (%) =
$$100 \times (1534-1128)/1534$$
 = 26.5

C.5 Calculation of the Amount of Surface Species

The amount of carbon in surface species on the catalyst surface obtained from the TPD step in an experimental set of three continuous steps is used to represent the amount of surface species. Hence, the amount of total surface species and particular surface species are calculated.

The concentration of CO_2 in Y-axis is initially converted as the molar flow rate of CO_2 by the assumption of ideal gas behavior as follows:

$$F_{CO_2} = C_{CO_2} \times v = [y_{CO_2} \times P] \times v/[R \times T]$$
 (C.21)

Where,

 F_{CO_2} = Molar flow rate of CO_2 (mole/min)

 C_{CO_2} = Concentration of CO_2 (mole)

v = Total volumetric flow rate (liter/min)

 y_{CO_2} = mole fraction of CO_2

P = Total pressure (atm)

R = Gas constant = 0.08206 (atm·liter/mole·K)

T = Absolute temperature (K)

Subsequently, the temperature in X-axis is converted as time through the heating rate of TPD step. The relationship between the molar flow rate and time is graphically obtained. Then the area under this curve gives the value of total CO₂ mole released from the catalyst surface. Finally, this value is converted to mass of carbon. The same method for CH₄ and CO curve is obtained and the summation of mass of carbon from CO₂, CH₄ and CO becomes the total amount of carbon in surface species.

APPENDIX D

LIST OF PUBLICATIONS

D.1 International Paper

- 1. Piyasan Praserthdam, Choowong Chaisuk, Apiwat Panit, and Kriangsak Kraiwattanawong, "Some aspects about the nature of surface species on Pt-based and MFI-based catalysts for the selective catalytic reduction of NO by propene under lean-burn condition", Applied Catalysis B: Environmental, to be published.
- 2. Piyasan Praserthdam, Choowong Chaisuk, and Pornsawan Kanchanawanichkun, "Comparative study of coke deposition on catalysts in reactions with and without oxygen", Research on Chemical Intermediates, 24(5), 605-612 (1998).

D.2 International Conference

- 1. Piyasan Praserthdam and Choowong Chaisuk, "Role of NO on propene and NO conversion over Pt/Al₂O₃ catalyst under lean-burn condition at low temperature", 2nd World Congress on Environmental Catalysis 1998, Miami Beach, Florida, U.S.A., Nov. 15-20, 1998, 402.
- 2. Piyasan Praserthdam and Choowong Chaisuk, "The effect of NO on coke formation over Pt catalyst in NO reduction by propene under lean-burn condition", Proceedings of region symposium on Chemical Engineering 1998, Manila, Philippines, Oct. 14-16, 1998, 146.
- 3. Piyasan Praserthdam and Choowong Chaisuk, "Comparative study of coke deposition on Pt catalysts in reactions with and without oxygen", 15th Canadian Symposium on Catalysis 1998, Quebec, Canada, May 17-20, 1998, 44.



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Applied Catalysis B: Environmental 1015 (2002) 1-15



Some aspects about the nature of surface species on Pt-based and MFI-based catalysts for the selective catalytic reduction of NO by propene under lean-burn condition

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Abstract

The nature of surface species for the selective catalytic reduction of NO by propene under lean-burn condition is relatively investigated on Pt/Al₂O₃ and Co-ZSM-5 catalysts. An experimental set of three continuous steps including adsorption, temperature programmed desorption (TPD) and temperature programmed oxidation (TPO) is performed to observe the particular behavior of surface species on both catalysts. The surface species on Pt/Al₂O₃ are almost totally released during TPD step, whereas those on Co-ZSM-5 are necessarily removed by the oxidizing gas on TPO step. It is suggested that the different nature of surface species on both catalysts should possibly play an important role on the reaction mechanism pathway. For Co-ZSM-5 catalyst, the surface species, which are formed by the interaction of NO, propene and oxygen, are distinctly assigned as the intermediate species in the NO reduction mechanism. On the other hand, for Pt/Al₂O₃ catalyst, the observation of several surface species and the investigation about their reactivities indicate that several reaction mechanisms are simultaneously proceeded at the same operating condition. © 2002 Published by Elsevier Science B.V.

Keywords: Pt/Al₂O₃; Co-ZSM-5; SCR of NO by propene; Lean-burn condition; Surface species; Reaction mechanism

1. Introduction

Nitrogen oxides (NO_x) are emitted primarily both from stationary and automotive sources and contribute largely to a variety of environmental problems such as the formation of acid rain and the resultant acidification of aquatic systems, the photochemical reaction in the stratosphere destroying the ozone in the atmosphere and the harmful impact for the respiratory sys-

* Corresponding author. Tel.: +66-2-218-6766; fax: +66-2-218-6769. E-mail address: gnowoohc@hotmail.com (C. Chaisuk). tem of human being [1]. To alleviate these problems, the emission of nitrogen oxides is seriously controlled. There are two major conventional catalytic technologies for the abatement of the emission of nitrogen oxides into the atmosphere. One is the selective catalytic reduction using ammonia as a reductant (NH₃-SCR) [2]. However, there are many problems associated with this process including ammonia slip, equipment corrosion, as well as danger in transportation and storage of ammonia. Hence, this technology can be conveniently used for only stationary sources such as power plants. The second technology is the three-way catalyst (TWC) that is highly efficient in the simultaneous

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removal of carbon monoxide, hydrocarbons and nitrogen oxides [3]. However, it requires an exhaust gas composition operating very close to the stoichiometric point. Thus, the emissions from diesel and lean-burn gasoline engines are not effectively controlled on this catalyst. From these reasons, neither of the above two catalytic technologies is applicable for the emissions from both mobile sources and stationary sources containing oxygen excess [4].

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The most attractive approach for the removal of NO_x is the catalytic decomposition of NO [5]. This method is feasible because no reducing agent is required. Thermodynamically, NO can decompose to dinitrogen under 800 °C but, kinetically, it remains stable in the absence of catalyst [6]. However, no suitable catalyst with a significant activity in real exhaust gases has been identified [7]. It is widely accepted that the poisoning of the catalyst surface by oxygen atom from the exhaust gas or from the decomposition itself is the main problem. Hence, the only way to reduce NO_x emission in lean exhaust gases is the injection of reducing agents into the exhaust gas stream [8,9].

In 1986, the outstanding activity for the catalytic decomposition of NO on Cu-ZSM-5 compared to the earlier known catalysts was reported by Iwamoto et al. [10]. This finding was remarkable but its catalytic activity dropped sharply with a decrease in the NO concentration and this catalyst suffered from severe deactivation in the presence of oxygen or sulfur oxides. It was later demonstrated that Cu-ZSM-5 showed a significant activity when it was used for a real lean-burn engine; moreover, the rate of reaction increased in the presence of oxygen. It was shown that the reaction taking place in this case was not the decomposition of NO but the reduction of NO by hydrocarbons contained in the emission gases. In 1990, Held et al.[11] and Iwamoto [12], independently proposed that the reduction of NO over Cu-ZSM-5 could be greatly enhanced in an excess of oxygen by the presence of small amounts of hydrocarbon. Following this discovery, many catalysts such as various kinds of solid acids and bases, including ZSM-5 loaded with metal ions, were demonstrated to be active catalysts for this reaction [13]. Generally, this reaction is the so-called selective catalytic reduction by hydrocarbon (HC-SCR).

Catalysts reported for this reaction so far can be classified into zeolites, metal oxides and noble metals. Various zeolites have a promising activity at high

temperature; however, there are major problems with these catalysts both in terms of thermal stability [14] and sensitivity to water [15]. On the other hand, metal oxides and noble metals are not adequate for the very demanding challenge of providing high activity and good selectivity but their activities are little diminished by sulfur oxides or water [16,17]. Hence, the development and design of SCR catalysts have been continuously investigated to overcome these limitations. Although there are many literatures reported to the success for testing this reaction on several catalysts, the outstanding knowledge about the reaction mechanisms and the active intermediate species is still ambiguous.

Generally, two main different mechanisms have been reported in the literatures, i.e. the NO decomposition mechanism [18-21] and the NO reduction mechanism [22-27]. The first mechanism has mainly been mentioned for the noble metal group catalysts, especially platinum-based catalysts. In this case, the hydrocarbons are contributed to remove the surface oxygen poisoning the active sites, while nitrogen product is dominantly formed via NO dissociation. Hence, the complex surface species such as organic nitro species are distinctly neglected and either N atom or NO molecule is addressed as the intermediate species for this mechanism [20]. On the other hand, the NO reduction mechanism is widely proposed to explain with various catalysts, especially zeolite group catalysts. Although its pathway may be different in details, the same significant concept is the complex surface species playing an important role for producing nitrogen. For example, the hydrocarbons react with oxygen to partially oxidized hydrocarbons, which are reactive by nitrogen dioxide to form nitrogen [23]. Additionally, the hydrocarbons may first react with nitrogen dioxide produced by NO oxidation to organic nitro species leading to the formation of nitrogen [27]. Thus, there are many types of surface species, e.g. organic nitro compound [27,28], isocyanate species [29-31] and oxygenated organic complex [32], independently assigned as the intermediate species for this mechanism. However, the influencing parameters, e.g. types of catalyst [1], reaction conditions [30] and types of reductant [33], should be carefully taken into account for considering in details about the reaction mechanism as well.

Typically, propene is used to be a model reductant gas to explain the reaction mechanism on various cat-

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alysts. Among the catalysts tested for the selective catalytic reduction of NO by propene, Pt/Al₂O₃ has extensively been studied in order to increase its catalytic activity and selectivity. However, the high rates of nitrous oxide formation and the narrow temperature window of the catalytic performance are crucial problems for application practice [34]. Nevertheless, mechanism studies from many literatures suggest that the selective catalytic reduction of NO by propene on this catalyst has not been clarified to take place through the NO decomposition or the NO reduction mechanism [34]. Consequently, an exact role of the catalytic surface species has not particularly been addressed to be the intermediate species or the spectator species upon such reaction. In case of Pt/Al₂O₃, the differences in mechanism studies, from a group of zeolite catalysts, have been raised because the reaction on zeolites is distinctly proceeded via the NO reduction mechanism. To understand a role of the catalytic surface species for this reaction better, Co-ZSM-5 catalyst is chosen to represent a group of zeolites for comparing to Pt/Al₂O₃ catalyst. Co-ZSM-5 is an attractive catalyst because its activity for the selective catalytic reduction of NO by methane is very high, compared to other ion-exchanged ZSM-5 catalysts. Although the introduction of the other hydrocarbons instead of methane has not much been studied, the previous works have been unanimous that the proposed mechanism for the selective catalytic reduction of NO by various hydrocarbons over Co-ZSM-5 is the same pathway [35-46]. It contains two main steps, i.e. the hydrocarbon activation leading to the N-containing intermediate species and the conversion of these species to final products.

From the earlier introduction, attempt to investigate the role of surface species on the reaction mechanism of the selective catalytic reduction of NO by propene is made over two catalysts, i.e. Co-ZSM-5 and Pt/Al₂O₃. In this work, the surface species are indirectly studied as described in the next section.

182 2. Experimental

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183 2.1. Catalyst preparation

A 1 wt.% Co-ZSM-5 catalyst was prepared by the ion-exchange of Na-ZSM-5 having Si/Al molar ratio of 25 (ALSI-PENTA Zeolithe GmbH, Alustr.50,

92421 Schwasdorf, Germany) with 0.01 M aqueous solution of cobalt(II) acetate at 80 °C for 24 h under continuous stirring. After the ion-exchange process, the sample was thoroughly washed with deionized water for 3–5 times to remove some ions using a centrifuge separator, dried at 110 °C overnight and calcined in air at 540 °C for 3.5 h.

A 1 wt.% Pt/Al₂O₃ catalyst was prepared by incipient wetness impregnation method. The alumina support used in this study was obtained from Sumitomo Aluminum Smelting (type NKH-3) and the metal salt precursor was chloroplatinic acid hexahydrate (H₂PtCl₆·6H₂O) obtained from Wako Pure Chemical Industries. After impregnation, the sample was dried at 110 °C overnight and calcined in air at 500 °C for 3 h.

2.2. Catalytic evaluation

The aim for this catalytic test is to investigate the nature of surface species for the selective catalytic reduction of NO by propene on both Co-ZSM-5 and Pt/Al₂O₃ catalysts. All experiments were conducted by using a quartz tubular downflow reactor with 0.6 cm inside diameter. The effluent gases were analyzed by a gas chromatograph (SHIMADZU GC 8A) equipped with molecular sieve 5 Å column for separating oxygen, nitrogen and carbon monoxide and porapak QS column for separating carbon dioxide, nitrous oxide and hydrocarbons. Prior to the catalyst test, 0.2 g of Co-ZSM-5 was pretreated in helium at 500°C for 1 h, whereas 0.1 g of Pt/Al₂O₃ was reduced in hydrogen flow at 500 °C for 1 h and subsequently treated under 10% oxygen in helium at 500°C for 1 h. An experimental set of three continuous steps was performed, i.e. first-adsorption step for producing the surface species, second-temperature programmed desorption (TPD) step for removing the weakly adsorbed surface species and third-temperature programmed oxidation (TPO) step for testing the reactivity of the remaining deposits to the oxidizing gas. During the first step, the sample was exposed to the selected reactant gas mixture containing 0-1000 ppm NO, 0-2000 ppm propene and 0-10% oxygen diluted in helium at a given temperature until saturation. The TPD experiment on the second step was subsequently carried out from 100 to 800 °C under helium flow. Afterwards, the removal of deposits was performed by heating the sample from 100 to 800 °C under various oxidizing

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gases, i.e. 1000 ppm NO, $1\% \text{ O}_2$ and the gas mixture of 1000 ppm NO and $1\% \text{ O}_2$.

235 3. Results and discussion

236 3.1. Co-ZSM-5 catalyst

237 3.1.1. The catalytic behavior for time on stream 238 experiment

First, the catalytic behavior for the selective catalytic reduction of NO by propene on Co-ZSM-5 was studied by considering the time on stream experiment. The gas mixture used in this experiment contained 1000 ppm NO, 2000 ppm propene and 10% oxygen diluted in helium. Fig. 1 shows the nitrogen product concentration from the reactor outlet in this experimental set. At the beginning step, the gas mixture was immediately introduced into the system at 550 °C. It was obviously seen that the nitrogen concentration detected from reactor outlet gradually decreased at the initial time (0-30 min), and then reached a constant value. After 150 min, the gas mixture was subsequently switched off and the sample was cooled down from 550 to 400 °C under helium flow. Next, the gas mixture was again switched into the reactor at this temperature (400 °C). It was observed that the nitrogen concentration diminished as a function of time after introducing the gas mixture. Interestingly, the nitrogen concentration was close to 0 value within 1 h. After that, the gas mixture was switched off and the reaction temperature was raised to 550 °C under helium atmosphere. Like the previous step, the gas mixture was again introduced to the reactor at this temperature (550 °C). It was clearly found that the initial nitrogen concentration at 550 °C in the second test was much higher than that in the first test and then it dramatically decreased with time. Finally, the nitrogen concentration reached to a constant value, which was approximately equal to the nitrogen concentration in the first test. Presumably, NO conversion to nitrogen at 550 °C reached the steady value at this stage. It was believed that the decrease of nitrogen concentration at both temperatures was due to the deposits. It was expected that the negligible effect of deposits was existed at the high temperature (550 °C). On the other hand, it was speculated that these deposits may hardly be removed at lower temperature; therefore, the nitrogen production was significantly suppressed at 400 °C. These results were corresponding with the work reported by Chen et al. [47] who observed the decrease of NO conversion at 300 °C as a function of time on stream for the selective catalytic reduction by iso-butane and n-butane over Fe-ZSM-5. Additionally, they suggested that the deactivation was accounted for the formation of active deposits, which significantly blocked the accessible sites for NO adsorption. Thus, the reaction, which was catalyzed by the iron sites, will be hindered [43]. Comparing the initial NO conversion at 550 °C between the first test and the second one, it was obvious that the second test gave much more NO conversion than the first one. There were two

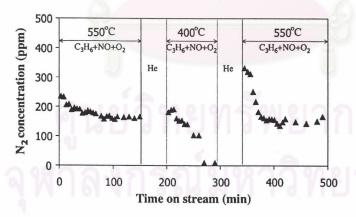


Fig. 1. The nitrogen concentration from the reactor outlet as a function of time on stream for the selective catalytic reduction of NO by propene on Co-ZSM-5 at 400 and $550\,^{\circ}$ C. The gas reactant composition $1000\,\mathrm{ppm}$ NO, $2000\,\mathrm{ppm}$ C₃H₆ and 5% O₂, GHSV = $2000\,\mathrm{h^{-1}}$.

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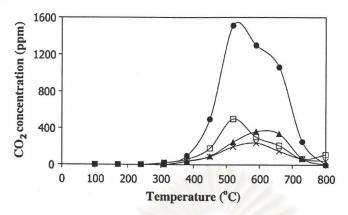


Fig. 2. The carbon dioxide concentration released during TPO by O_2 on Co-ZSM-5 after dosing various adsorbed gas mixtures at $100\,^{\circ}$ C: (×) $2000\,\text{ppm}$ C_3H_6 , (\square) $2000\,\text{ppm}$ $C_3H_6 + 1000\,\text{ppm}$ NO, (\blacktriangle) $2000\,\text{ppm}$ $C_3H_6 + 5\%$ O_2 , (\blacksquare) $2000\,\text{ppm}$ $C_3H_6 + 1000\,\text{ppm}$ NO + 5% O_2 .

possible explanations for this observation. First, the deposits, kinds of intermediate species, can react with the reactant gases to produce nitrogen product. In the other case, the deposits can decompose themselves to nitrogen product when the reaction temperature was high enough. Furthermore, the latter case was in accordance with the report by Walker [37] who mentioned that the carbonaceous deposits merely acted as reductant for impinging on NO or NO₂. However, it can be concluded from these results that the deposits should be reversible, viz. the NO reduction activity could be recovered when the reaction temperature was high enough that these deposits could be removed.

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3.1.2. The formation of intermediate species

From the earlier introduction, it was suggested that the formation of intermediate species should play an important role on the NO reduction mechanism. These intermediate species may be produced by various ways, for example, the only hydrocarbons being the active carbonaceous species [48], the hydrocarbons reacting with oxygen leading to the production of partially oxidized hydrocarbon species [23], and etc. This part showed the formation of intermediate species on Co-ZSM-5 by varying the adsorbed gas mixture in absorption step. The procedure for testing was described in Section 2.

Four sets of gas mixture $(C_3H_6, C_3H_6+NO, C_3H_6+O_2)$ and $C_3H_6+NO+O_2)$ were used as a testing gas in the adsorption step. Co-ZSM-5 was dosed by each gas set at $100\,^{\circ}\text{C}$ until the saturation. After that, TPD

and TPO by only oxygen steps were continuously proceeded to investigate the characteristic of the surface species. It was noted that the surface species were entirely removed on TPO step, while no species was released during TPD step. TPO spectra of Co-ZSM-5 catalyst dosed by the adsorbed gas mixture are illustrated in Figs. 2 and 3. It was observed that carbon dioxide and nitrogen were only two types of the product gases emitted from reactor on TPO experiments. Hence, the amounts of such gases should refer to the total amount of the deposits on catalyst surface. Fig. 2 obviously shows that the amount of carbon dioxide from C₃H₆ + NO + O₂ experiment set was much more than that from the other three systems. This result implied that the most possibility for the formation step of intermediate species was the cooperation of the three reactant gas species, i.e. NO, propene and oxygen. The nitrogen removed during TPO step could also support this explanation as illustrated in Fig. 3. It was clearly seen that nitrogen would be emerged from only $C_3H_6 + NO + O_2$ system. Therefore, it can be concluded that the intermediate species for the selective catalytic reduction of NO by propene on Co-ZSM-5 catalyst were necessarily formed by the interaction of NO, propene and oxygen.

Chang and McCarty [44] found that co-adsorption of NO and oxygen led to a substantial increase in the amount of NO_x adsorbed on the catalysts irrespective of cation type or degree of metal loading. Similar behavior over Co-ZSM-5 catalyst that NO

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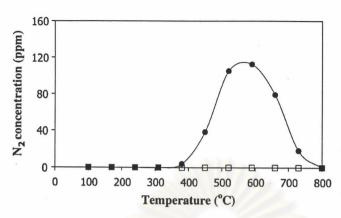


Fig. 3. The nitrogen concentration released during TPO by O2 on Co-ZSM-5 after dosing various adsorbed gas mixtures at 100 °C: (2000 ppm $C_3H_6 + 1000$ ppm NO, (\blacksquare) 2000 ppm $C_3H_6 + 1000$ ppm NO + 5% O₂.

was hardly adsorbed at the reaction temperatures was also reported, but the interaction between NO and Co cations was greatly enhanced in the presence of oxygen [39]. In addition, Pinaeva et al. [45] suggested that Co ion located at the interface of Co clusters and zeolites was found to react with NO in the presence of oxygen to form anchored NO2 delta+ species stabilized on Co-ZSM-5 under the reaction conditions. Therefore, it can be proposed from these results that the initial step for the selective catalytic reduction of NO by propene in the presence of oxygen excess on Co-ZSM-5 catalyst was the adsorption of NO_y species formed by the interaction of NO and oxygen. These species will subsequently interact with propene and

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form nitrogen-containing deposits, which should be the intermediate species of such reaction; however, the formation of intermediate species may mainly depend on types of hydrocarbon reductant as well.

3.1.3. The removal of intermediate species

In order to study the image of the removal of intermediate species for the selective catalytic reduction of NO by propene in the presence of oxygen excess over Co-ZSM-5, TPO experiment step was independently conducted by varying oxidizing gases (NO, O2 and NO + O2). In this part, Co-ZSM-5 catalyst was exposed by only gas mixture of C₃H₆ + NO + O₂ at 100 °C. Figs. 4 and 5 show the concentrations of car-

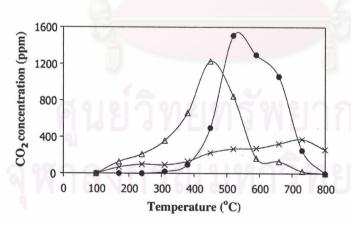


Fig. 4. The carbon dioxide concentration released during TPO by varying oxidizing gases on Co-ZSM-5 after dosing 2000 ppm $C_3H_6 + 1000 \text{ ppm NO} + 5\% \text{ O}_2 \text{ at } 100^{\circ}\text{C}$: (×) 1000 ppm NO, (•) 1% O₂, (\triangle) 1000 ppm NO + 1% O₂.

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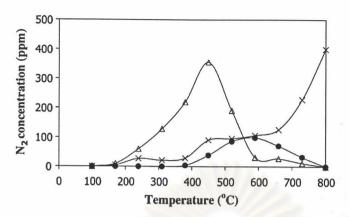


Fig. 5. The nitrogen concentration released during TPO by varying oxidizing gases on Co-ZSM-5 after dosing 2000 ppm C₃H₆ + 1000 ppm NO + 5% O₂ at 100 °C: (×) 1000 ppm NO, (●) 1% O₂, (△) 1000 ppm NO + 1% O₂.

bon dioxide and nitrogen on TPO step, respectively. As seen in Fig. 4, a small amount of carbon dioxide was emerged by using only NO as the oxidizing gas. When the oxidizing gas became either only oxygen or a gas mixture of NO and oxygen, a large amount of carbon dioxide was distinctly obtained. These results implied that the removal of intermediate species was effectively occurred in the presence of oxygen. Interestingly, when a gas mixture of NO and oxygen was used instead of only oxygen, the intermediate species could be removed at lower temperature region. Therefore, it can be concluded that the cooperation of NO and oxygen possibly accelerated the removal of intermediate species.

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Although the amount of carbon dioxide emerged during TPO step by only oxygen or a gas mixture of NO and oxygen was not much different, the nitrogen concentration for both cases was remarkably different as illustrated in Fig. 5. TPO step by a gas mixture of NO and oxygen showed that the amount of nitrogen product was largely released at lower temperature. This result implied that the increase of nitrogen product could be attributed to nitrogen atom in NO feed, which can interact with the remaining intermediate species and produce nitrogen. Hence, the obtained nitrogen product was generated from nitrogen atoms both in the intermediate species and in the oxidizing gases. This was in agreement with the literature reported by Chen et al. [43]. From their results obtained by the isotopic labeling technique on Fe-ZSM-5, it was found that one nitrogen atom in every nitrogen 409 product came from the deposits, while the other came from the gas phase nitrogen dioxide.

In addition, TPO step performed by using NO as the oxidizing gas significantly provided the nitrogen product at high temperature as also shown in Fig. 5. However, such nitrogen should not be produced by the deposits since there was no carbon dioxide detected at the same temperature as seen in Fig. 4. It was believed that this nitrogen could be produced through the NO decomposition, which favored at very high temperature under the absence of oxygen. This result was corresponding with the work by Wang et al. [46] who observed that NO was reduced in oxygen-free feed over Co-ZSM-5 at high temperature. From their results, it was suggested that NO could be reduced on Co²⁺ ion without nitrogen dioxide formation.

3.2. Pt/Al₂O₃ catalyst

3.2.1. The catalytic behavior for temperature programmed reaction

Fig. 6 shows the temperature programmed reaction profiles of Pt/Al_2O_3 catalyst for $C_3H_6 + O_2$ and $C_3H_6+NO+O_2$ systems. It was clearly observed that the C_3H_6 light-off temperature for $C_3H_6 + O_2$ system was lower than that for $C_3H_6 + NO + O_2$ system. This result was corresponding with the references suggested that at low temperatures NO blocked the active sites responsible for propene oxidation [49,50]. Con-

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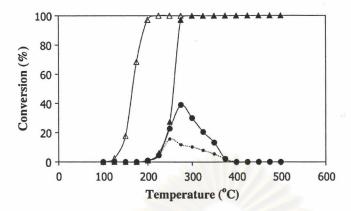


Fig. 6. The temperature programmed reaction profiles of Pt/Al_2O_3 for $C_3H_6 + O_2$ and $C_3H_6 + NO + O_2$ systems; the gas reactant composition 1000 ppm C_3H_6 and 5% O_2 for $C_3H_6+O_2$ system: (\triangle) C_3H_6 conversion, and 1000 ppm NO, 1000 ppm C_3H_6 ; 5% O_2 for NO fore $C_3H_6 + NO + O_2$ system: (\blacktriangle) C_3H_6 conversion, (\blacksquare) NO conversion, (\longrightarrow) NO conversion to N_2 , GHSV = 60000 h⁻¹ for both.

sidering the $C_3H_6 + NO + O_2$ system, the onset of NO reduction and the peak in the NO conversion were closely related to the oxidation of propene. Conversion of propene and of NO both began at the same temperature and raised together until NO reduction reached a maximum value at approximately similar temperature where the propene oxidation was complete. This coincidence of propene and NO conversions was a general phenomenon within lean- NO_x catalysis [20].

3.2.2. The nature of surface species

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For the inhibition of propene activation by NO obtained from temperature programmed reaction results, it was interesting to study the influence of NO on the formation of surface species over Pt/Al₂O₃ catalyst. The characterization of surface species was investigated by an experimental set containing three continuous steps, i.e. adsorption, TPD and TPO by only oxygen. Two sets of gas mixture (C₃H₆ + O₂ and C₃H₆ + NO+O₂) were first used in adsorption step at 100 °C to produce the surface species. Fig. 7 depicts the relevant traces of outlet gases obtained on TPD step after dosing each gas mixture on Pt/Al₂O₃. The main outlet gases for C₃H₆+NO+O₂ system were carbon dioxide and nitrogen, while only carbon dioxide was released when there was no NO in the adsorbed gas mixture. 461

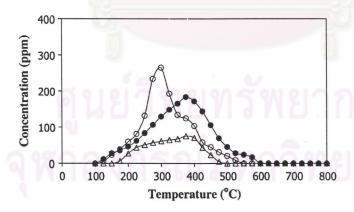


Fig. 7. The TPD profiles of Pt/Al₂O₃ after dosing 1000 ppm C₃H₆ + 5% O₂ at 100 °C: (●) carbon dioxide; 1000 ppm C₃H₆ + 1000 ppm NO + 5% O_2 at 100 °C: (O) carbon dioxide, (\triangle) nitrogen.

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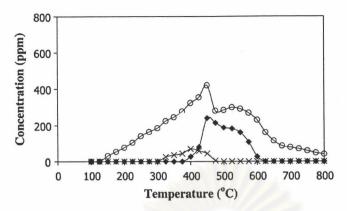


Fig. 8. The TPD profiles of Pt/Al₂O₃ after dosing 1000 ppm C₃H₆ + 5% O₂ at 150 °C: (O) carbon dioxide, (×) methane, (◆) carbon monoxide.

It was significantly noticed that no species was detected during TPO step. For C₃H₆+O₂ system, a sharp peak of carbon dioxide appeared at 375 °C whereas for C₃H₆ + NO + O₂ system, it was shifted to lower temperature (at approximately 300 °C) with a shoulder at ca. 375 °C. It was noted that the amount of carbon dioxide released from both systems was equivalent. Taking close consideration, it was seen that there were two peaks in C₃H₆+NO+O₂ system after deconvolution, i.e. at 300 and 375 °C. In addition, the deconvolution of nitrogen profile obtained from C₃H₆+NO+O₂ system showed a peak at 375 °C and a broad peak at low temperature range (200-350 °C). From these results, it was inclined that the presence of NO in the adsorbed gas mixture induced N-containing surface species at 300 °C. According to the report of Xin et al. [51], nitro and nitrito organic compounds were absolutely detected by DRIFTS after addition of a mixture of $C_3H_6 + NO + O_2$ onto Pt-ZSM-5 at 100 °C. The coincident position of carbon dioxide peak at 375 °C in both systems and the appearance of nitrogen peak at the same temperature for $C_3H_6 + NO + O_2$ system may imply two aspects. First, these carbon dioxide peaks at 375 °C represented to the same type of surface species whereas nitrogen peak was occurred due to the decomposition of adsorbed NO. Second, types of surface species for two systems were different but their partial structures may be similar.

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However, the nature of surface species could be certainly changed under the reaction condition. Okuhara

et al. [27] found that for the reaction of C₃H₆ + $NO_2 + O_2$ on Pt/SiO₂, the organic nitro and nitrite compounds appeared at low temperature whereas the organic carbonyl species and isocyanate species occurred at higher temperature. Therefore, the surface species over Pt/Al₂O₃ were also observed after dosing the gas mixture of $C_3H_6 + O_2$ and $C_3H_6 + NO + O_2$ at each reaction temperature of 150 and 225 °C, respectively. At a given temperature, propene conversion of each system was equally ca. 20%. Figs. 8 and 9 illustrate the traces of outlet gases during TPD step containing carbon dioxide, methane, and carbon monoxide for C₃H₆ + O₂ system and the additional nitrogen and nitrous oxide for C₃H₆ + NO + O₂ system. It was significantly remarked that most of surface species were released during TPD step whereas the amount of outlet gases by TPO step was extremely small. This suggested that the surface species could easily decompose themselves on Pt/Al₂O₃, unlike Co-ZSM-5, and the formation and removal of surface species were therefore clearly not the controlling steps for the selective catalytic reduction of NO by propene on this catalyst.

In case of $C_3H_6 + O_2$ system, as seen in Fig. 8, the carbon dioxide profile showed two main peaks at 450 and 525 °C. There was a little amount of methane at a temperature range 300–475 °C. It was interesting that for the carbon monoxide trace, its peak and shoulder were located to be coincident with the carbon dioxide peak at 450 and 525 °C, respectively. In case of

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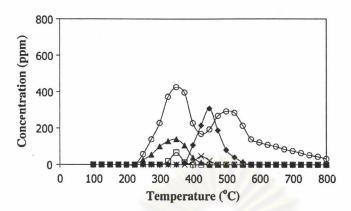


Fig. 9. The TPD profiles of Pt/Al₂O₃ after dosing 1000 ppm C_3H_6+1000 ppm NO +5% O₂ at 225 °C: (O) carbon dioxide, (×) methane, (\spadesuit) carbon monoxide, (\spadesuit) nitrogen, (\square) nitrous oxide.

 $C_3H_6 + NO + O_2$ system as shown in Fig. 9, there were two carbon dioxide peaks in TPD profile, while the other gases gave only one peak. Nitrogen and nitrous oxide peaks existed at low temperature whereas methane and carbon monoxide peaks were located at higher temperature. The deconvolution of these TPD profiles indicated that there were at least three types of surface species occurred on the catalyst surface. They were addressed as $C_x H_y O_z N_w$, $(C_i H_i O_k)_{LT}$, and $(C_lH_mO_n)_{HT}$ species decomposing themselves at low temperature region (200-400 °C), at moderate one (350-550 °C) and at high one (400-800 °C), respectively. The existence of these surface species was in agreement with the observation by IR technique in several references [31,52-54]. For example, Captain and Amiridis [31] noticed cyanide, isocyanate, acetate, and formate species on Pt/Al2O3 in $C_3H_6 + NO + O_2$ system by the use of in situ Fourier transform infrared spectroscopy and also found that only isocyanate species disappeared by flushing with helium at 250 °C. In addition, only isocyanate and acetate species were observed when increasing the reaction temperature at 350 °C and again only the intensity of isocyanate peak was essentially affected after the reactor was flushed with helium.

Considering the feature of surface species obtained by dosing the gas mixture of $C_3H_6 + O_2$ at 150 °C, the position of both carbon dioxide peaks was definitely coincident with that of two TPD peaks assigned as $(C_iH_jO_k)_{LT}$, and $(C_lH_mO_n)_{HT}$ species in $C_3H_6+NO+O_2$ system. From this result, it was believed that NO assisted the production of the particular surface species assigned as $C_xH_yO_zN_w$ species whereas two types of partially oxidized hydrocarbons, $(C_iH_jO_k)_{LT}$, and $(C_lH_mO_n)_{HT}$ species, were certainly generated in both $C_3H_6+O_2$ and $C_3H_6+NO+O_2$ systems.

3.2.3. The reactivity of surface species

In fact, the obtained surface species may possibly play a role to be either the intermediate species or the spectator species depending on the reaction condition as reported in some literatures. Tanaka et al. [52] proposed that nitro, nitrite and carbonyl surface species were key reaction intermediates for the selective catalytic reduction of NO by propene on Pt/SiO₂ at 120 °C. While Xin et al. [53] suggested that nitro, nitrito and isocyanate species were not the catalytic active intermediates for the selective catalytic reaction of NO by propene on Pt-ZSM-5 at 250 °C. On the other hand, Captain and Amiridis [31] concluded that carboxylates, nitrates and cyanide species were probably the spectator byproducts of the selective catalytic reduction of NO by propene on Pt/Al2O3 at 250 °C, whereas the surface isocyanate species could be a potential reaction intermediate in such reaction. With the above-mentioned reason, the reactivity of $C_x H_y O_z N_w$, $(C_i H_j O_k)_{LT}$, and $(C_l H_m O_n)_{HT}$ species with the oxidizing reactant gas in the reaction temperature range was studied. The reactivity test was con-

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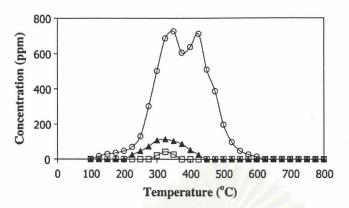


Fig. 10. The TPO profiles of Pt/Al_2O_3 by using 1% O_2 as the oxidizing gas after dosing 1000 ppm $C_3H_6 + 1000$ ppm NO + 5% O_2 at 225 °C: (O) carbon dioxide, (\blacktriangle) nitrogen, (\square) nitrous oxide.

ducted by using TPO technique after the production of surface species through dosing a gas mixture of $C_3H_6+NO+O_2$ on Pt/Al_2O_3 at 225 °C. The oxidizing gases were varied as 1000 ppm NO, 1% O_2 and the gas mixture of 1000 ppm NO and 1% O_2 . It was noted that the TPD step was negligible in this reactivity test.

Figs. 10–12 illustrate the concentrations of carbon dioxide, nitrogen and nitrous oxide during TPO experiment by using NO, O_2 and $NO + O_2$ as the oxidizing gas, respectively. It was noted that neither methane nor carbon monoxide was detected when each oxidizing gas was used for removing the surface species. It was also found that the position of carbon dioxide peak addressed as $C_x H_y O_z N_w$ species was unaffected with

changing oxidizing gas (NO, O_2 or $NO + O_2$). Furthermore, the nitrous oxide peak was not shifted under either O_2 or $NO + O_2$ atmosphere. The observation of nitrogen peak at 350 °C was rather difficult under NO or $NO + O_2$ atmosphere because nitrogen atoms in the oxidizing gas could possibly interact with other surface species to produce nitrogen. However, the introduction of only O_2 during TPO experiment did not influence the position of nitrogen peak. These results revealed that $C_xH_yO_zN_w$ species could decompose themselves under the oxidizing gas at the same temperature at which they decomposed under helium flow. Therefore, it was pronounced that neither NO nor O_2 was involved in the decomposition of $C_xH_yO_zN_w$ species at

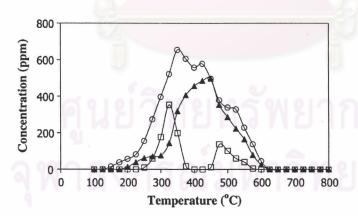


Fig. 11. The TPO profiles of Pt/Al_2O_3 by using 1000 ppm NO as the oxidizing gas after dosing 1000 ppm C_3H_6+1000 ppm NO + 5% O_2 at 225 °C: (\bigcirc) carbon dioxide, (\triangle) nitrogen, (\square) nitrous oxide.

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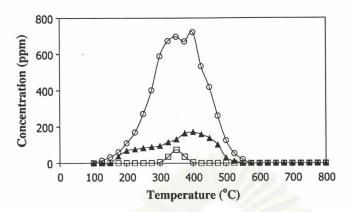


Fig. 12. The TPO profiles of Pt/Al_2O_3 by using 1000 ppm NO + 1% O_2 as the oxidizing gas after dosing 1000 ppm C_3H_6 + 1000 ppm NO + 5% O_2 at 225 °C: (O) carbon dioxide, (\triangle) nitrogen, (\square) nitrous oxide.

any temperature. This was also in agreement with the work by Captain and Amiridis [31] who reported that the surface cyanide on Pt/Al₂O₃ was not reacting in NO, NO₂, O₂ and NO + O₂ environments at 250 °C.

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A larger amount of carbon dioxide released at low temperature and the disappearance of the carbon dioxide peak at high temperature (525 °C) in the presence of O_2 or $NO + O_2$ as the oxidizing gas indicated that the surface species decomposing at high temperature, $(C_l H_m O_n)_{HT}$ species, were easily removed by these oxidizing gases. However, the existence of carbon dioxide peak at 525 °C in case that only NO was used as the oxidizing gas showed that O₂ was a more potential oxidizing gas than NO to be reactive with $(C_l H_m O_n)_{HT}$ species. This corresponds with the work by Tanaka et al. [52] who suggested that on Pt/SiO₂ the carbonyl species reacted rapidly with NO2 and O2 at 120 °C, while these species were inactive to NO. Considering the reactivity of $(C_iH_jO_k)_{LT}$ species to the different oxidizing gas, the relatively small shift to lower temperature of the peak of $(C_iH_iO_k)_{LT}$ species for all oxidizing gases manifested that these species were slightly reactive with NO, O₂ and NO + O₂. The reactivity of $(C_l H_m O_n)_{HT}$ species to either O_2 or $NO + O_2$ and the shift to lower temperature of a $(C_iH_iO_k)_{LT}$ species peak were also observed in C₃H₆ + O₂ system but they were not seen here. These results supported the above suggestion that $(C_i H_i O_k)_{LT}$ and $(C_l H_m O_n)_{HT}$ species were not only produced in $C_3H_6 + NO + O_2$ system but also generated in $C_3H_6 + O_2$ system.

3.3. The role of surface species on the reaction mechanism for the selective catalytic reduction of NO by propene on Co-ZSM-5 and Pt/Al₂O₃ catalysts

For Co-ZSM-5 catalyst, many literatures concluded that the reaction mechanism involved the adsorbed nitrogen dioxide reacting with hydrocarbon to produce the intermediate species on Co ion [35,36,38-43,55]. These intermediate species were subsequently oxidized by nitrogen dioxide to form nitrogen product. From the results described in Section 3.1.2, it was suggested that the coexistence of three reactants (C₃H₆+ $NO + O_2$) enhanced the formation of deposits. It was also believed that these deposits obtained during TPO step became the intermediate species for the selective catalytic reduction of NO by propene on Co-ZSM-5. Goryashenko et al. [41] mentioned that the gas phase nitrogen dioxide was not involved directly in the selective catalytic reduction of NO. The formation of nitrogen dioxide adsorbed on cobalt cations was also observed by Sun et al. [39]. Hence, it was possible that the intermediate species was formed through the interaction of propene and the adsorbed NO_v complex species, which were originated form the adsorbed nitrogen dioxide.

The nitrogen production should depend on the removal of intermediate species discussed in Section 3.1.3. The removal of intermediate species favorably occurred in the presence of oxygen; nevertheless, it was extremely enhanced by the coexistence of NO and oxygen. The nitrogen product was produced by nitro-

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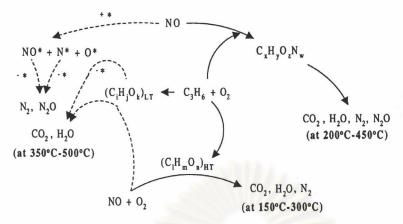


Fig. 13. A proposed reaction mechanism scheme for the selective catalytic reduction of NO by propene under lean-burn condition over Pt/Al₂O₃ ((*) is given as the vacancy Pt sites).

gen atom from both intermediate species and NO re-670 actant feed. It was concluded that the coexistence of 671 NO and oxygen was necessary for the removal of in-672 termediate species, which was corresponding with the 673 literatures [35,36,38-43,55]. Hence, the mechanism 674 for the selective catalytic reduction of NO by propene 675 under oxygen excess on Co-ZSM-5 was proposed as 676 follows: 677

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$$NO + O_2 \rightarrow NO_{\gamma}(ads)$$

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NO_y(ads) + C₃H₆
$$\rightarrow$$
 C_aH_bO_cN_d

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$$C_a H_b O_c N_d + NO + O_2 \rightarrow N_2 + CO_2 + H_2 O$$

For Pt/Al₂O₃ catalyst, although there were two different mechanisms, most researchers proposed that the selective catalytic reduction of NO by propene occurred only on Pt sites for both mechanisms [56-58]. From the results described in Section 3.2, the observation of three types of surface species indicated the complication in formation of surface species. Each surface species played an independently different role on the overall reaction mechanism. However, the weak adsorption of surface species resulted in the formation and removal of surface species being not the controlling steps for such reaction. It was postulated that there were at least three pathways in the overall reaction mechanism depending on the reaction temperature range. At low temperature range (150-300 °C), the NO reduction mechanism was mainly observed. $(C_l H_m O_n)_{HT}$ species on the catalyst surface easily reacted with either nitrogen dioxide or oxygen to produce nitrogen and carbon dioxide. The decomposition of $C_xH_yO_zN_w$ species occurred at moderate temperature range (200-450 °C). It was significantly remarked that the decomposition of $C_x H_y O_z N_w$ species was an only mechanism pathway attributed to produce nitrous oxide product. At high temperature range (350-500°C), nitrogen dioxide and oxygen slightly assisted to remove (CiHjOk)LT species. However, the nitrogen production was still unclear. Two aspects should presumably explain this behavior. In the first case, NO could adsorb and decompose to nitrogen on vacant sites, which were occurred by the removal of $(C_iH_iO_k)_{LT}$ species. In the second case, nitrogen product was generated by the reaction between nitrogen dioxide and (CiHiOk)LT species. Hence, the mechanism for the selective catalytic reduction of NO by propene under oxygen excess on Pt/Al₂O₃ was proposed as shown in Fig. 13.

4. Conclusions

The different nature of surface species on Co-ZSM-5 718 and Pt/Al₂O₃ catalyst may possibly play an important role on the reaction mechanism pathway for the selective catalytic reduction of NO by propene under 121 lean-burn condition. The strong adsorption of surface species on Co-ZSM-5 shows that these surface 723

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27	species become the intermediate species and their for
725	mation and removal directly relate to the controlling
726	step in the reaction mechanism. On the other hand
727	the weak adsorption of surface species on Pt/Al ₂ O ₃
728	indicates the complication of the reaction mechanism
729	pathway. The reaction should possibly via several co-
730	operative mechanisms at the same reaction condition
731	Hence, it is difficult to control the required reaction
732	mechanism over this catalyst. These are dependen
733	on various parameters, e.g. the reaction temperature
734	type of reductant, the reactant concentration, etc.

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पुरस्तितिमा पुरस्ति। श्रीकारीमा वार्षिकार्यः

COMPARATIVE STUDY OF COKE DEPOSITION ON CATALYSTS IN REACTIONS WITH AND WITHOUT OXYGEN

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Abstract-Two types of catalysts, i.e. Pt/y Al,O, and Cu/Na-ZSM-5, were used to investigate the catalyst activity and amount of coke formation on the spent catalysts. The reactions of particular interest were the hydrocarbon oxidation and the SCR of NO with and without O2. Propane and propene were used as the hydrocarbon sources. The reaction conditions were as follows: reaction temperature = 170-500°C, GHSV = 4,000 hr1, TOS = 2 hr, feed composition depending on each reaction, but the composition of gases were fixed as HC = 3,000 ppm, NO = 1,000 ppm and O₂ = 2.5%, using Hc balance. It was found that both the case of Pt/y Al₂O₃ and the case of Cu/Na-ZSM-5, propene provided higher conversion and coke deposition than propane in the presence or the absence of O₂ and/or NO. For Pt/Y Al2O3 catalyst, in case of the absence of oxygen reactions, the propene conversion dropped more rapidly than the propane conversion. Finally the reaction of propene gave a lower percent of hydrocarbon conversion than the reaction of propane. Additionally, propene had a higher percent selectivity of coke formation for the reaction with the absence of oxygen, but propane had a higher percent selectivity of coke formation for the reaction with the presence of oxygen. For Cu/Na-ZSM-5, in the system with absence and presence of oxygen, the addition of oxygen caused a significant change in % coke selectivity. With the presence of NOx, the percent conversion of both propane and propene decreased and that the % coke selectivity of propane decreased, whereas that of in propene increased.

INTRODUCTION

Coke deposition is an important deactivation mode in the hydrocarbon conversion process In general, most researchers [1-5] have emphasized only coke formation in reducing atmospheres e.g. dehydrogenation, cracking, reforming etc. Nevertheless, in oxidizing atmospheres, coke deposition can also take place on the catalyst surface. Therefore, in the present work, it is set up to compare the amount of coke formed on Pt/Al₂O₃ and Cu/Na-ZSM-5 catalysts for reactions with the absence and presence of oxygen. The catalytic activity and the amount of coke on the spent Pt/Al₂O₃ and Cu/Na-ZSM-5 catalysts were investigated for reactions with oxygen, *i.e.* hydrocarbon combustion and reduction of NO_x, and without oxygen, *i.e.* dehydrogenation or aromatization and reduction of NO_x. Propane and propene were used as the hydrocarbon sources for all four reactions.

EXPERIMENTAL

Pt/Al₂O₃ (0.3 wt.% Pt) catalyst in this study was prepared by a dry impregnation method using H2PtCl6 as the salt precursor. The parent Na-ZSM-5 zeolite with Si/AI ratio of 50 was hydrothermally synthesized from gel and decant solution in an autoclave. The structure of ZSM-5 was confirmed by X-ray diffraction (XRD). Cu/Na-ZSM-5 zeolite was prepared by exchanging Cu²⁺ into Na-ZSM-5 sample in the aqueous solution. The catalytic reactions were carried out at atmospheric pressure in a fixed bed reactor. A 0.5 g of catalyst was packed in a quartz tube reactor. In the case of Cu/Na-ZSM-5, before the reaction, the catalyst was heated under He flow from room temperature to 500°C in 1 hr., and held for 1 hr. before being cooled down. In the case of Pt/Al₂O₃, the catalyst was reduced to 500°C for 1 hr using hydrogen as the reductant gas. The 50 cc./min. of mixed gas feed consisting of 100 ppm NO, 3000 ppm hydrocarbon, 2.5% vol. oxygen and He was introduced to the reactor at a space velocity of 4000 hr⁻¹. The temperatures of the reaction with and without oxygen were 170°C and 350°C (in the case of Pt/Al₂O₃) or 500 °C (in the case of Cu/Na-ZSM-5) respectively. The outlet gases were analyzed by SHIMADZU GC-8APT gas chromatograph with MS-5A column for nitrogen, oxygen and carbon monoxide and with SHIMADZU GC-8AIT porapak QS column for carbon dioxide, propane and propene. Coke deposited on the catalysts was characterized by temperature programmed oxidation (TPO). Before starting the TPO, 0.5 g of the spent catalysts was heated to 130°C at 10°C/min. under He atmosphere and held for 3 hr. The heat treatment removed any air and water that was adsorbed on the catalyst. Then the pretreated sample was heated from 50°C to 700°C with a heating rate of 5°C/min. then in a 30 cc./min. stream of 1% O, in helium gas. The carbon dioxide formed was determined by SHIMADZU GC-8AIT gas chromatograph using a thermal conductivity detector with parapak QS column. The percentage of carbon in coke can be calculated from TPO curves. CO, area is divided by a internal time in which CO2 flows through the sampling loop (1 cc.). The rate of CO₂ formation is, hence, obtained. The area under the curve of CO₃ formation rate versus time gives the value of total CO₂ formation. Finally, this value is converted to milligram carbon or percentage of carbon by using a calibration curve.

RESULTS AND DISCUSSION

For the Case of Pt/Al₂O₃

The experimental results were shown in Table 1, Figure 1 and Figure 2. In all four reactions, it was observed that the reactions with propene as a reactant gave a larger percent of hydrocarbon conversion in the initial interval of time on stream and also

Table 1
Hydrocarbon conversion, amount of coke and coke selectivity of 0.3% Pt/Al₂O₃.

Reaction	Reactant	Temperature (°C)	% HC conversion (at 5 min.)	% Carbon in coke	% Selectivity of coke formation
HC	Propane	350	59.36	0.17	0.22
	Propene	350	98.88	0.32	0.27
HC+NO	Propane	350	46.17	0.13	0.19
	Propene	350	66.14	0.16	0.34
HC+O ₂	Propane	170	11.71	0.13	1.13
	Propene	170	100.00	0.48	0.29
HC+NO+O ₂	Propane	170	5.59	0.12	1.07
	Propene	170	40.12	0.33	0.54

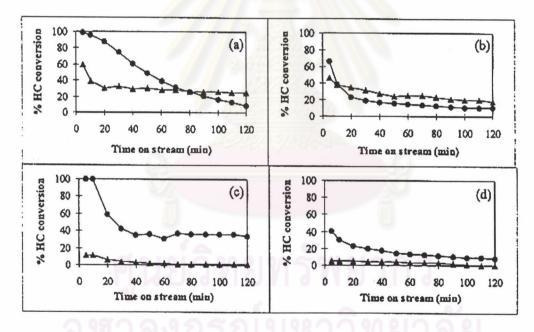


Figure 1. Relationship between % HC conversion versus time on stream. (a) Feed: 3000 ppm HC + He balance, Temperature = 350° C. (b) Feed: 3000 ppm HC + 1000 ppm NO + He balance, Temperature = 350° C. (c) Feed: 3000 ppm HC + 2.5 vol.% O_2 + He balance, Temperature = 170° C. (d) Feed: 3000 ppm HC + 1000 ppm NO + 2.5 vol.% O_2 + He balance, Temperature = 170° C.: (\blacklozenge) Propane, (\spadesuit) Propene.

had a larger amount of coke than the reactions with propane as a reactant. However, in the dehydrogenation reaction and NO_x reduction under the absence of oxygen condition, the propene conversion dropped more rapidly than the propane

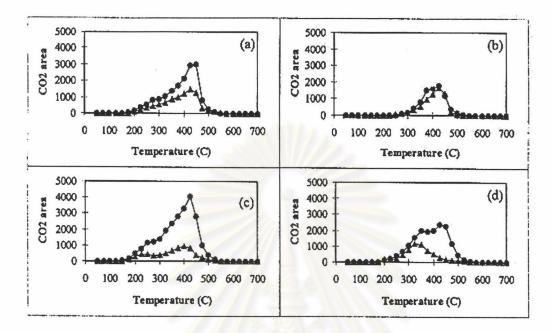


Figure 2. TPO profiles of 0.3 g coked catalyst from reaction. (a) Dehydrogenation, Temperature = 350°C. (b) Reduction of NO_x under absence of oxygen condition, Temperature = 350°C. (c) Combustion, Temperature = 170°C. (d) Reduction of NO_x under absence of oxygen condition, Temperature = 170°C.: (\spadesuit) Propane, (\spadesuit) Propene.

conversion. Finally the reaction of propene gave a lower percent of hydrocarbon conversion than the reaction of propane. It meant that propene is more active than propane [6]. Since propene reacted more, there was more opportunity to convert to coke precursor. Additionally, it was clarified that the product of propene from the reaction with the absence of oxygen, propadiene which is converted irreversibly to ethylidyne leading to coke deposition [7,8], was more reactive than propene [6]. Thus the catalysts in the reaction using propene as a reactant were rapidly covered by carbonaceous deposits. The TPO profiles of 0.3% Pt/Al₂O₃ catalysts are indicated in Figure 2. Each sample showed a TPO peak around 425°C except the TPO profiles of spent catalyst from reduction of NO_X in the presence of oxygen condition. This TPO profiles showed a TPO peak at a temperature of around 325°C for the reaction with propane as a reactant and two peaks at the temperature around 325°C and 425°C for that with propene as a reactant. Barbier et al. [3] suggested that the first peak is the coke on metal and the second peak is the coke on the support. In this paper, we define the selectivity of coke formation as the ratio of carbon atom in coke to carbon atom of feed hydrocarbon converted. It was found that propene had a higher percent of selectivity of coke formation for the reaction with the absence of oxygen, but propane had a higher percent of selectivity of coke

formation for the reaction with the presence of oxygen. Under the presence of oxygen, it suggested that coke is formed in parallel with carbon dioxide formation. Propene or coke precursor is more effectively reacted with oxygen to carbon dioxide [9]. Additionally, for the reaction with the presence of oxygen using propane as a reactant, it was observed that the reaction with the absence of NO gave a higher percent of selectivity of coke formation than the reaction with the presence of NO. On the other hand, in the case of propene, the reactant with the presence of NO gave higher percent selectivity of coke formation. It suggests that propane or propene is first reacted with adsorbed oxygen to be converted to intermediates [10,11]. In the case of propane [10,11], these intermediates are preferably reacted with NO which result in, when NO was added in feed, propane producing less selectively of coke formation. However, in the case of propene [12], NO hardly reacted with the intermediates but it preferred to dissociate into dinitrogen. Thus, since the dissociation of NO hinders the reaction of carbon dioxide formation, the intermediates prefer produce coke rather than carbon dioxide for the case of the presence of NO reaction.

For the Case of Cu/Na-ZSM-5

The experimental results were summarized in Figure 3. It was found that the propene conversion was higher than that of propane. This is particularly obvious for the reaction with the presence of oxygen and absence of NOx as shown in Figure 3(b). Propane conversion was only 10 %, whereas propene conversion is about 100 %. Figure 3(c),(d) (reduction of NO_x with and without O₂) exhibited the effect of NO_x on the reaction. It was found that the % of propene conversion decreased when NO, was added, however the % of propene conversion was still higher than that of propane. It means that propene is more active than propane [6]. The temperature program oxidation (TPO) results were shown in Figure 4. It was found that the amount of coke from the four reactions of propene was greater than propane over Cu/Na-ZSM-5 zeolite. The results in Table 2 can suggest that in aromatization, the percentage of propene conversion was greater than that of propane; however, on the other hand, the % coke selectivity of propene was less than that of propane, because propene was converted to product more than to coke while propane formed product less than coke. In the system with absence and presence of oxygen it was found that the addition of oxygen caused a significant change in % of coke selectivity [13-15]. With the presence of NO_x, it was found that the percent conversion of both propane and propene decrease and that the % of coke selectivity of propane decreased whereas that of in propene increased. From this result in the case of propene, we can propose that NOx was adsorbed on the surface of the catalyst to form an intermediate which is strongly adsorbed and, hence, the desorption rate is slow [16-21]. As a result, the intermediate can not selectively form the product but can be further

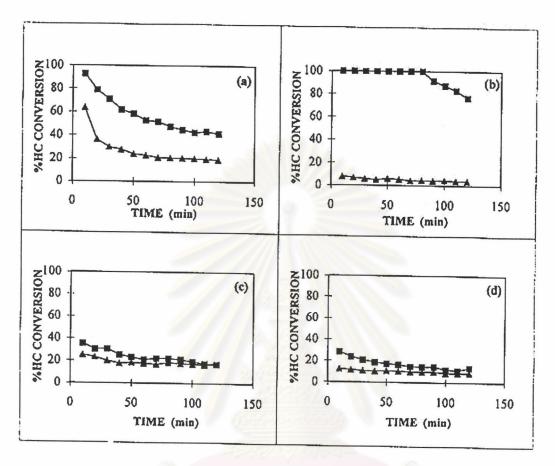


Figure 3. Relationship between % HC conversion versus time over 1.58% Cu/Na-ZSM-5; (a) Feed: 3000 ppm HC + He balance, Temperature = 500° C. (b) Feed: 3000 ppm HC + 2.5 vol.% O_2 + He balance, Temperature = 170° C. (c) Feed: 3000 ppm HC + 1000 ppm NO + He balance, Temperature = 500° C. (d) Feed: 3000 ppm HC + 1000 ppm NO + 2.5 vol.% O_2 + He balance, Temperature = 170° C: (\triangle) C_3H_8 , (\blacksquare) C_3H_6

converted to coke.

CONCLUSION

Both in the case of Pt/γ Al_2O_3 and in the case of Cu/Na-ZSM-5, propene provided both higher conversion and coke deposition than propane in the presence or the absence of O_2 and/or NO. For Pt/γ Al_2O_3 catalyst, in the case of the absence of oxygen reactions, the propene conversion dropped more rapidly than the propane conversion. Finally, the reaction of propene gave a lower percentage of hydrocarbon conversion than the reaction of propane. Additionally, propene had a higher

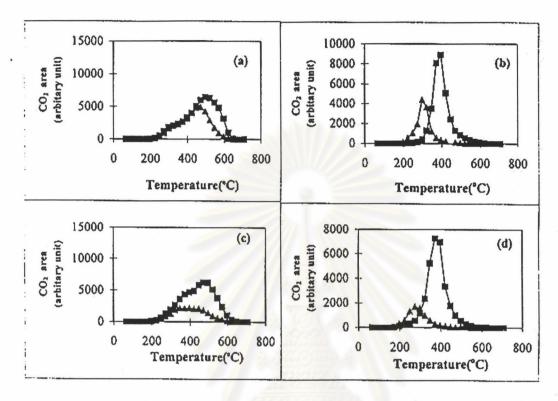


Figure 4. TPO curve of 1.58% Cu/Na-ZSM-5 after the reaction; (a) HC at 500 °C, (b) HC+O₂ at 170 °C, (c) HC+NO at 500 °C, (d) HC+NO+O₂ at 170 °C; (\blacktriangle) C₃H₈, (\blacksquare) C₃H₆; In the case of propene (b,d), amount of coked catalyst for TPO is five times than that of propane.

Table 2
Percentage HC conversion and selectivity of coke over 1.58%Cu/Na-ZSM-5

Reaction	Reactant	Temperature (°C)	% HC conversion (at 5 min.)	% Carbon in coke	% Selectivity of coke formation
HC	propane	500	75	0.45	0.74
	propene	500	98	0.68	0.51
HC+O ₂	propane	170	9	0.17	1.43
	propene	170	100	2.03	0.86
HC+NO _s	propane	500	26	0.25	0.45
	propene	500	38	0.67	1.51
HC+NO,+O,	propane	170	15	0.10	0.39
	propene	170	38	1.82	2.80

percentage of selectivity of coke formation for the reaction with the absence of oxygen but propane had higher percent selectivity of coke formation for the reaction with the presence of oxygen. For Cu/Na-ZSM-5, in the system with absence and presence of oxygen, the addition of oxygen caused a significant change in the % of coke selectivity. With the presence of NO_x, the percent conversion of both propane and propene decreased and that of the % coke selectivity of propane decreased, whereas that in propene increased.

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ROLE OF NO ON PROPENE AND NO CONVERSION OVER Pt/Al₂O₃ CATALYST UNDER LEAN-BURN CONDITION AT LOW TEMPERATURE

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Summary: The catalytic activity and the amount of coke on the spent Pt/Al₂O₃ catalysts were investigated for the C₃H₆/O₂ reaction with and without the presence of NO at 150 °C. The addition NO with the concentrations of 212 ppm or 520 ppm decrease percent propene conversion and the amount of coke, but the selectivity of coke formation becomes higher.

Introduction

From the recent literature [1-2], there are still arguments on the reaction mechanisms of NO reduction by hydrocarbon under excess oxygen condition over Pt catalyst. Since coke deposition can also take place on catalyst surface in oxidizing atmosphere, the investigation of coke formation for NO reduction by hydrocarbon may illustrate some aspects that may be useful for the prediction of reaction mechanism.

Results and Discussion

For the reaction without NO (with a feed containing 3000 ppm C₃H₆, 2.5%O₂ and He balance at a GHSV of 4000 for 2 hrs at 150°C), 100% and 37.5% of propene were converted to CO at 5 mins and 2 hrs, respectively. When 212 ppm or 520 ppm NO was added, percent propene conversion decreased. In the case of NO at 212 ppm, 17.6% and 2.4% of propene were converted to CO₂ at 5 mins and 2 hrs, respectively. In case of 520 ppm, a percent of propene conversion was 24.2% and 1% at 5 mins and 2 hrs, respectively. Additionally, 10% and 21.5% of NO were approximately converted to N₂ in case of 212 ppm and 520 ppm NO, respectively. After the reaction, the coked catalyst was analyzed by temperature programmed oxidation technique (TPO) performed by burning it in 1 vol.% O₂ in He. It was found that the amount of carbon in coked catalysts were as follows: 0.48% (no NO), 0.27% (212 ppm NO) and 0.34% (520 ppm NO). The TPO profile of the spent catalyst from the reaction without NO showed two TPO peaks at the temperature around 225°C and 425°C. Similarly, the TPO

Role of NO on Propene and NO Conversion Over Pt/Al₂ O₃ Catalyst Under Lean-Burn Condition at Low Temperature

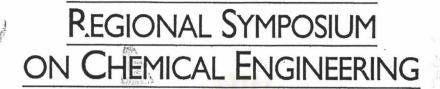
profiles of the coked catalyst from the reaction with NO (both 212 ppm NO and 500 ppm NO) demonstrated two peaks, but the first peak was shifted to a higher temperature (325 °C). Barbier et al [3] suggested that the first peak is the coke on metal and the second peak is the coke on the support. Additionally, it was found that propene conversion decreased with the increase of the amount of coke but NO conversion to N2 was nearly constant. It was possible that propene reacts with O2 on the sites on which coke was formed. In this paper, we define the selectivity of coke formation as the ratio of carbon atoms in coke to carbon atoms of feed hydrocarbon converted. It was found that the reaction with NO had higher percent selectivity of coke formation than the reaction without NO (0.86% for 212 ppm NO, 1.70% for 520 ppm NO and 0.26% for no NO). From the results, it suggested that NO would compete with C3H6 and O to adsorb on metal active sites [1,2] leading to the decrease of percent propene conversion and the amount of coke and to react with adsorbed O2 to NO2 [2] leading to the decrease of propene combustion or the increase of percent selectivity of coke formation. Since the advorbed O2 which prevents the deposition of carbonaceous deposits [4] decrease, the peak of the coke on metal shifted to a higher temperature. It does not believe that an active carbonaceous material, which is formed from the propene, was responsible for the formation of N₂ [5] because the percent propene conversion decreased whereas the percent NO conversion to N₂ were almost constant as time on stream increased.

Conclusions

It was concluded that the reaction between propene and oxygen carried out on the sites rely on coke formation and that the reaction between propene and NO₂ proceed on the sites do not relate to coke formation.

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THE EFFECT OF NO ON COKE FORMATION OVER Pt CATALYST IN NO REDUCTION BY PROPENE UNDER LEAN-BURN CONDITION.

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ABSTRACT

The catalytic activity and the amount of coke on the spent Pt/Al₂O₃ catalysts were investigated for the C₃H₆/O₂ reaction with and without the presence of NO at 170 °C. The addition of NO with the concentration of 1000 ppm decreased percent propene conversion and the amount of coke, but the selectivity of coke formation became higher. Additionally, the peak of the coke on metal and support shifted to a higher temperature in even of the presence of NO. It was also found that organic NO₂ groups was the main species detected after the reaction with NO thus it was suggested to be the intermediates.

INTRODUCTION

The emission of NO_x from stationary and automotive sources has serious environmental implications and therefore, various catalysts have been developed for NOx control. Ammonia has used as a reducing agent to remove NOx under net-oxidizing conditions but this technology can only be conveniently used on stationary sources. The three-way automotive catalyst has been highly successful in controlling exhaust emissions from conventional petrol engines which operate close to stoichiometric conditions. However, this catalyst is no longer effective for NO_x control in oxygen-rich exhaust gases such as the exhaust from diesel and lean-burn gasoline engines. To reduce NOx under these conditions alternative catalytic systems must be developed. Various zeolites [1,2], metal oxide [3], and noble metals [4] have been reported to have catalytic activity for the selective reduction of nitrogen monoxide with hydrocarbon in the presence of excess oxygen. The platinum group metals supported on metal oxide are among the most important catalysts. Although the supported platinum catalyst does not have as high activity as Cu-ZSM-5 catalyst at high temperature, Cu-ZSM-5 catalyst has poorer thermal and hydrothermal stability. It has been emphasized that the activities of the Pt catalysts were little diminished by the introduction of SO₂ [5,6] or water [6]. From the recent literature [7-12], there are still arguments on the reaction mechanisms of NO reduction by hydrocarbon under excess oxygen condition over Pt/A2O3 catalyst. In general, many mechanisms have been proposed for NO reduction in the presence of oxygen, for example:

1. The hydrocarbon may remove the surface oxygen poisoning the active site, while nitrogen is formed through NO decomposition [7].

2. The hydrocarbon may react with oxygen to partially oxidized hydrocarbon

which then reacts with NO (or NO₂) to form nitrogen [8].

3. The hydrocarbon may react with NO₂ [4] formed by NO oxidation to intermediates such as isocyanate [9] and organic nitro compound [10] leading to the formation of nitrogen.

4. The hydrocarbon may be converted to an active carbonaceous material [11] and then it is rely on the formation of nitrogen, while oxygen may prevent the deposition of carbonaceous deposits which would cover the active sites [12].

In general, most researches have emphasized only on coke formation in reducing atmosphere e.g. dehydrogenation [13], cracking [14], reforming [15] etc. Nevertheless under these net-oxidizing condition it appears that coke deposition can take place on catalyst surface. The investigation of coke formation for NO reduction by hydrocarbons may illustrate some aspects that may be useful for the prediction of reaction of reaction mechanism. Therefore, in the present work, coke formation on Pt/Al₂O₃ catalyst for propene combustion (without NO) and NO reduction by propene under lean-burn condition (with NO) were studied.

EXPERIMENT

The 0.3 % Pt/Al₂O₃ catalyst used in this study was prepared by dry impregnation method using hexchloroplatinic acid as the salt precursor. The sample was calcined at 500 °C for 3 hr. in air. Catalytic testing was carried out using a quartz tubular downflow microreactor (i.d. 6 mm). The sample (0.5g) was held between plugs of quartz wool. Prior to the reactor, the catalyst was reduced with a flow of H2 at 500 °C for 1 hr. Then it was cooled down from 500°C to reaction temperature, 170.°C. Both reactions, propene combustion and NO reduction by propene under lean-burn condition, were performed at the pressure close to the atmospheric pressure. A feed gas mixture was fed at the volumetric flow rate of 60 cm³/min or with gas hourly space velocity (GHSV) of 4000 hr⁻¹. The feed gas consists of propene (3000 ppm) and oxygen (2.5 %vol) with He balance for propene combustion. NO (1000 ppm) was added in feed stream for selective catalytic reduction of NO with propene in the presence of excess oxygen. The time on stream of both reactions was varied at 1, 2, and 4 hr. The products were analyzed using a SHIMADZU GC-8ATP gas chromatograph equipped with molecular sieve 5A for the separation of O2, N2 and CO and a SHIMADZU GC-8AIT gas chromatograph equipped with Porapak QS for the separation of CO2, N2O and C3H6.

The coke catalysts from both reactions were characterized by temperature programmed oxidation technique (TPO) performed by burning it in 1 vol% oxygen in helium. Before starting the TPO, 0.3 g of spent catalyst was pretreated at 120°C for 3 hr under helium atmosphere. During testing the TPO, the temperature was raised from 50 °C to 700 °C and the effluent stream was sampled by an on-line gas sampling valve every 5 minutes. Carbon dioxide produced was measured by a thermal conductivity detector (TCD) gas chromatography (GC 8AIT, SHIMADZU) with Porapak QS column. The percentage of carbon in coke can be calculated from TPO curves. CO₂ area is divided by a internal time in which CO₂ formation is, hence, obtained. The area under the curve of CO₂ formation rate versus time gives the value of total CO₂ formation. Finally, this value is converted to milligram carbon or percentage of carbon by using a calibration curve.

Infrared spectra of the adsorbed species on the spent catalysts from both reactions were recorded on an FT-IR spectrometer (The Micolet model Impact 400) equipped with a deuterated triglycine sulfate (DTGS) detector. About 50 mg of the spent catalyst was set in the IR cell. The resolution of 4 cm⁻¹ with 500 scans was employed for every experiment.

RESULTS AND DISCUSSIONS

The effect of time on stream on the $C_3H_6 + O_2$ and $C_3H_6 + O_2 + NO$ reactions over 0.3 %Pt/Al₂O₃ at 170 °C is shown in Figure 1. It was observed that the reaction without NO gave significantly higher percent hydrocarbon conversion than the reaction with NO.

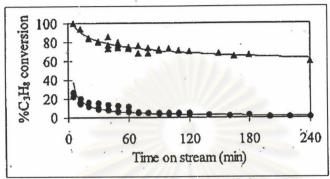


FIGURE 1 Relationship between %C₃H₆ conversion and time on stream on Pt/Al₂O₃. Given: (**A**) The reaction without NO (C₃H₆+O₂),

() The reaction with NO (C₃H₆+O₂+NO)

After the reaction, the spent catalysts were characterized by temperature programmed oxidation technique (TPO) and then percentage of carbon in catalyst was calculated as shown in Table 1. It was noticed that the $C_3H_6 + O_2$ reaction provided higher amount of coke than the $C_3H_6 + O_2 + NO$ reaction (at the same time on stream). Additionally, the amount of coke increase with time on stream in both reactions. In this paper, we define the selectivity of coke formation as the ratio of carbon atom in coke to carbon atom of hydrocarbon feed converted. From Table 1, it was found that the reaction with NO had higher percent selectivity of coke formation than the reaction without NO. For the $C_3H_6 + O_2$ reaction, the percent selectivity of coke formation decreased with time on stream. When NO was added, it appeared that the percent selectivity of coke formation was not related simply to time on stream.

TABLE 1 t of coke and selectivity of coke formation of Pt/Al₂O₃.

Reaction	Time on stream (hr)	% C ₃ H ₆ conversion	% Coke	% Selectivity of coke formation
C ₃ H ₆ +O ₂	1	74.08	0.45	0.31
	2	70.34	0.67	0.23
	4	59.76	0.98	0.19
C ₃ H ₆ +O ₂ +NO	1	10.97	0.28	0.80
	2	3.18	0.41	1.27
	4	0.51	0.47	1.08

The TPO profiles of 0.3 %Pt/Al₂O₃ catalysts are indicated in Figure 2. The spent catalyst from the reaction without NO showed a shoulder at 250 °C and a TPO peak around 425 °C, while the TPO profiles of spent catalysts from the reaction with NO demonstrated two TPO peak at the temperature around 325 °C and 450 °C. Barbier et al. [16] suggested that the first peak is the coke on metal and the second peak is the coke on the support. It was noticed that the reaction without NO provided higher amount of coke on support than the reaction with NO but coke on support for $C_3H_6 + O_2$ reaction was burnt harder than coke on support for $C_3H_6 + O_2 + NO$ reaction. It was also found that the peak of the coke on metal shifted to a higher temperature in even of the presence of NO; besides, for $C_3H_6 + O_2 + NO$ reaction the amount of coke on metal is higher than the amount of coke on support.

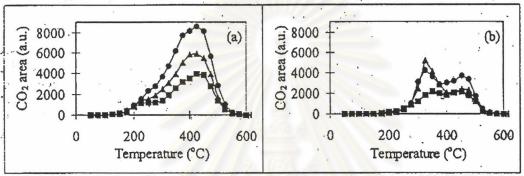


FIGURE 2 (a) TPO profiles of coked catalyst from the reaction without NO (C₃H₆+O₂).

(b) TPO profiles of coked catalyst from the reaction with NO (C₃H₆+O₂+ NO).

Given: (■) Time on stream = 1 hr., (▲) Time on stream = 2 hr.,

() Time on stream = 4 hr.

Figure 3 shows IR spectra of the surface species after $C_3H_6 + O_2$ and $C_3H_6 + O_2 + O_3$ NO reactions at 170 °C. It was observed that three main peaks appeared at 1460, 1570 and 1630 cm⁻¹ for both reactions. Besides, it was noticed that two board peaks also appeared approximately at 1350 and 1410 cm⁻¹ for the presence of NO.

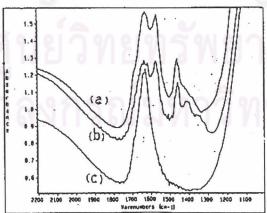


FIGURE 3 IR spectra of the surface species, (a) Spent catalyst C₃H₆+O₂ reaction, (b) Spent catalyst C₃H₆+O₂+ NO reaction, (c) Fresh catalyst.

For all the catalyst, both fresh and spent catalysts, the band at 1630 cm⁻¹ disappeared after pretreatment under vacuum at 150 °C. It believed that this band can be assigned to OH deformation (adsorbed water on catalyst surface) [17]. Two bands at 1460 and 1570 cm⁻¹ can be assigned to carbonaceous deposits because these bands appeared on spent catalyst from the reactions with the presence of NO and the absence of NO. Normally, the band in the region of 1500-1600 cm⁻¹ are very specific to stretching mode of aromatic systems [18]. The in-phase blending vibration of the carbon-hydrogen bands of methyl or methylene groups occur in the regions of 1340-1470 cm⁻¹ [18]. Thus, two bands at 1460 and 1570 cm⁻¹ can be assigned to methyl or methylene groups and aromatic ring, respectively. As report previously, it was speculated that two bands at 1350 and 1410 cm⁻¹ can be assigned to organic NO₂ groups (stretching mode) [10].

From literature, on account of the fact that Al₂O₃ is not active to hydrocarbon combustion at this temperature [19], propene should react with oxygen on the metal sites. Furthermore, NO oxidation also take place on the metal sites [20]. Therefore, it is possible that both NO and propene may compete to adsorb and react with oxygen on metal active sites. R.Burch et al. [20] found that NO conversion to NO2 was independent of contact time for NO oxidation over Pt/Al₂O₃ catalyst They believed that conversion of NO to NO₂ was faster than the other reactions, e.g. hydrocarbon combustion, NO conversion to N2 etc., occurring on the Pt/ Al₂O₃ catalyst. From the results above, it was suggested that oxygen would preferably react with NO leading to the decrease of percent propene conversion. Since propene from C₃H₆ + O₂ reaction was more reacted than that from C₃H₆ + O₂ + NO reaction, there are more opportunities to be converted to coke precursor. Because the catalysts in the C₃H₆ + O₂ reaction were rapidly covered by carbonaceous deposits, they gave higher amount of coke than the catalysts in the C₃H₆ + O₂ + NO reaction. From the previous [21] work, it was concluded that the higher production rate of coke precursor appeared in the gas product, the lower coke deposited on the catalyst surfaces is. On the other hand, if the deactivation is found significantly, product of coke precursor would be found in amount of trace. This is consistent with the results above which it was found that the C₃H₆ + O₂ + NO reaction had higher percent selectivity of coke formation than that of C₃H₆ + O₂ reaction. From TPO results of both reactions, it is speculated that shifting and decreasing of coke on support after the addition NO may have three reasons as follows: 4, :

- 1. NO₂ spill over [20] will suppress the drain off effect.
- 2. The coke on support will be burnt by oxygen [12].

[11].

3. The active carbonaceous material on support will react with the other species

It is expected that the first reason are more possible than the other reasons. Because the coke on the support is a complex structure coke, there are opportunities to be burnt or reacted hardly. On the other hand, the peak of the coke on metal shifted to a higher temperature since the adsorbed O₂ which prevents the deposition of carbonaceous deposits decrease. Finally, it is suggested that adsorbed NO on metal active sites reacted with oxygen to NO₂ and then it may be transferred from metal active sites to support. Indeed, it hindered the drain off effect and related to the formation of intermediates to nitrogen production which it will correspond to the formation of organic nitro species.

CONCLUSION

It was concluded that the addition NO affect to coke formation as follow;

- 1. NO would complete with C₃H₆ to adsorb and react rapidly with O₂ on metal active sites leading to the decrease of present propene conversion and the amount of coke.
- 2. and would suppress C₃H₆ combustion leading to the increase of present selectivity of coke formation.
 - 3. NO would difficultly lead to burn coke on metal and support.
 - 4. NO would correspond to the formation of organic nitro species.

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Abstracts Book Résumés



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COMPARATIVE STUDY OF COKE DEPOSITION ON Pt CATALYSTS IN REACTIONS WITH AND WITHOUT OXYGEN.

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ABSTRACT

Coke deposition is an important deactivation mode in hydrocarbon conversion process. In general, most researchers (1-5) have emphasized only on coke formation in reducing atmosphere e.g. dehydrogenation, cracking, reforming etc. Nevertheless, in oxidizing atmosphere, coke deposition can also take place on catalyst surface. Therefore, in the present work, it is set up to compare the amount of coke formed on Pt/Al₂O₃ catalysts for reactions with the absence and presence of oxygen. The catalytic activity and the amount of coke on the spent Pt/Al₂O₃ catalysts were investigated for reactions with oxygen, i.e. hydrocarbon combustion and reduction of NOx, and without oxygen, i.e. dehydrogenation and reduction of NO_X. Propane and propene were used as the hydrocarbon sources for all four reactions. Pt/Al₂O₃ (0.3 wt.% Pt) catalyst in this study was prepared by dry impregnation method using H₂PtCl₆ as the salt precursor. The catalytic test is carried out in a 0.6 I.D. quartz microreactor where a 0.5 g of the catalyst was packed. The reactor was heated from room temperature to 500°C at the heating rate of 5 °C/min. Then, the catalyst was reduced at 500°C for 1 hr using hydrogen as the reductant gas. The reactor was cooled down from 500°C to reaction temperature as 350°C and 170°C for the case of the presence and absence of oxygen reaction, respectively. All four reactions were performed at the pressure close to the atmospheric pressure. A feed gas mixture was fed at the volumetric flow rate of 50 cm³/min or with gas hourly space velocity (GHSV) of 4000 hr⁻¹. Its hydrocarbon (propane or propene) composition was fixed at 3000 ppm. The time on stream was fixed at 2 hr. The coked catalyst from each reaction was analyzed by temperature program oxidation technique (TPO) performed by burning it in 1 vol.% oxygen in helium. The temperature was raised to 700°C at the heating rate of 5°C/min. When temperature was 50°C, the effluent stream was sampled every 5 minutes by an on-line gas sampling valve. Carbon dioxide produced was measured by a thermal conductivity detector (TCD) gas chromatography (GC 8AIT, Shimadzu) with Parapak-QS column.

The experimental results were shown in Table 1, Figure 1 and Figure 2. In all four reactions, it was observed that the reactions with propene as a reactant gave more percent hydrocarbon conversion in the initial interval of time on stream and also had more amount of coke than the reactions with propane as a reactant. However, in the dehydrogenation reaction and NO_X reduction under the absence of oxygen condition, the propene conversion was dropped more rapidly than the propane conversion. Finally the reaction of propene gave less percent hydrocarbon conversion than the reaction of propane. It meant that propene is more active than propane (6). Since propene was more reacted, there is more opportunity to be converted to coke precursor. Additionally, it was clarified that the product of propene form the reaction with the absence of oxygen, propadiene which is converted irreversibly to ethylidyne leading to coke deposition (7,8), was more reactive than propene (6). Thus the catalysts in the reaction using propene as a reactant were rapidly covered by carbonaceous deposits. The TPO profiles of 0.3% Pt/Al₂O₃ catalysts are indicated in Figure 2. Each sample

showed a TPO peak around 425° C except the TPO profile of spent catalyst from reduction of NO_X in the presence of oxygen condition. This TPO profiles showed a TPO peak at the temperature around 325°C for the reaction with propane as a reactant and two peaks at the temperature around 325 °C and 425 °C for that with propene as a reactant. Barbier et al. (3) suggested that the first peak is the coke on metal and the second peak is the coke on the support. In this paper, we define the selectivity of coke formation as the ratio of carbon atom in coke to carbon atom of feed hydrocarbon converted. It was found that propene had higher percent selectivity of coke formation for the reaction with the absence of oxygen but propane had higher percent selectivity of coke formation for the reaction with the presence of oxygen. Under the presence of oxygen, it suggested that coke is formed in parallel with carbon dioxide formation. Propene or coke precursor is more effectively reacted with oxygen to carbon dioxide (9). Additionally, for the reaction with the presence of oxygen using propane as reactant, it was observed that the reaction with the absence of NO gave higher percent selectivity of coke formation than the reaction with the presence of NO. On the other hand, for the case of propene, the reactant with the presence of NO gave higher percent selectivity of coke formation. It suggested that propane or propene is first reacted with adsorbed oxygen to be converted to intermediates (10,11). For the case of propane (10,11), these intermediates are preferably reacted with NO which result in, when NO was added in feed, propane less selectively produce coke. However, for the case of propene (12), NO is hardly reacted with the intermediates but it prefer dissociate into dinitrogen. Thus, since the dissociation of NO hinders the reaction of carbon dioxide formation, the intermediates prefer produce coke rather than carbon dioxide for the case of the presence of NO reaction.

Table 1: Hydrocarbon conversion, amount of coke and coke selectivity of 0.3% Pt/Al₂O₃

Reaction	Reactant	Temperature (°C)	% HC conversion (at 5 min.)	% Coke	% Selectivity of coke formation
HC	Propane	350	59.36	0.1759	0.223
	Propene	350	98.88	0.3236	0.269
HC+NO	Propane	350	46.17	0.1336	0.192
	Propene	350	66.14	0.1633	0.338
HC+O ₂	Propane	170	11.71	0.1319	1.131
	Propene	170	100.00	0.4795	0.294
HC+NO+O ₂	Propane	170	5.59	0.1213	1.069
	Propene	170	40.12	0.3289	0.542

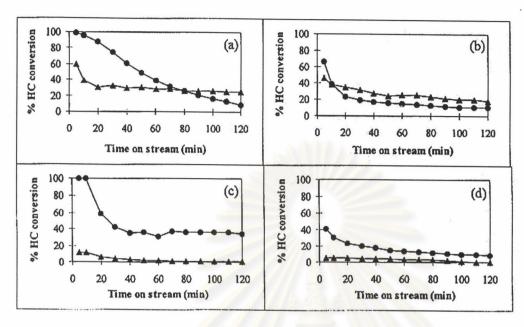


Figure 1: Relationship between % HC conversion versus time on stream (a) Feed: 3000 ppm HC + He balance, Temperature = 350 °C (b) Feed: 3000 ppm HC + 1000 ppm NO + He balance, Temperature = 350 °C (c) Feed: 3000 ppm HC + 2.5 vol.% O₂ + He balance, Temperature = 170 °C (d) Feed: 3000 ppm HC + 1000 ppm NO + 2.5 vol.% O₂ + He balance, Temperature = 170 °C: (A) Propane, (D) Propane

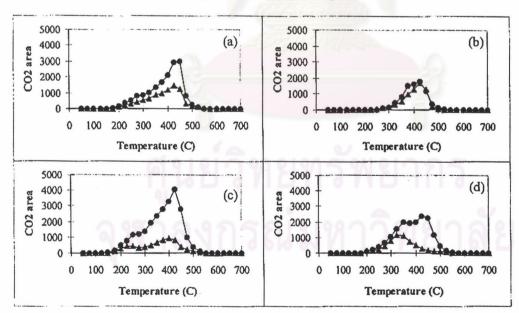


Figure 2: TPO profiles of coked catalyst from reaction (a) Dehydrogenation, Temperature = 350 °C (b) Reduction of NO_x under absence of oxygen condition, Temperature = 350 °C (c) Combustion, Temperature = 170 °C (d) Reduction of NO_x under absence of oxygen condition, Temperature = 170 °C : (\triangle) Propane , (\bigcirc) Propene

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