CONTINUOUS REMOVAL OF THIOPHENIC SULFUR COMPOUNDS FROM TRANSPORTATION FUELS BY USING X ZEOLITE

Jittima Kaewboran

A Thesis Submitted in Partial Fulfilment of the Requirements
for the Degree of Master of Science

The Petroleum and Petrochemical College, Chulalongkorn University
in Academic Partnership with

The University of Michigan, The University of Oklahoma,
Case Western Reserve University and Institut Français du Pétrole
2006

ISBN 974-9937-42-2

Thesis Title:

Continuous Removal of Thiophenic Sulfur Compounds

from Transportation Fuels by Using X Zeolite

By:

Jittima Kaewboran

Program:

Petroleum Technology

Thesis Advisors:

Asst. Prof. Pomthong Malakul

Dr. Sophie Jullian

Dr. Rapeepong Suwanwarangkul

Accepted by the Petroleum and Petrochemical College, Chulalongkorn University, in partial fulfilment of the requirements for the Degree of Master of Science.

Nontage Sammet . College Director

(Assoc. Prof. Nantaya Yanumet)

Thesis Committee:

(Asst. Prof. Pomthong Malakul)

(Dr. Sophie Jullian)

(Dr. Rapeepong Suwanwarangkul)

(Asst. Prof. Apanee Luengnaruemitchai)

(Dr. Siriporn Jongpatiwut)

J Sint

ABSTRACT

4773004063: Petroleum Technology

Jittima Kaewboran: Continuous Removal of Thiophenic Sulfur

Compounds from Transp ortation Fuels by Using X Zeolite

Thesis Advisors: Asst. Prof. Pomthong Malakul, Dr. Sophie Jullian,

and Dr. Rapeepong Suwanwarangkul 94 pp. ISBN 974-9937-42-2

Keywords:

Adsorption/ Diesel/ Gasoline/ Sulfur Removal/ Zeolite

Recently, new laws and regulations concerning environmental impacts have driven an increase in the demand of ultra low sulfur fuels. Over the years, the adsorption process has proven to be an efficient process for removing a small amount of refractory sulfur compounds (ppm level), which is difficult to treat by the conventional hydrodesulfurization process (HDS). In this research, continuous liquid adsorption of three model sulfur compounds, i.e., 3-methylthiophene (3-MT), benzothiophene (BT) and dibenzothiophene (DBT), using NaX zeolites were studied in a packed column. Iso-octane and decane were used to represent gasoline and diesel, respectively. The effects of initial sulfur concentration and types of sulfur compounds on the adsorption breakthrough curve were examined. The result shows that at higher initial feed concentration, the slope of the breakthrough curve is steeper and the breakthrough time is shorter. Whereas, the breakthrough of the three types of sulfur compounds are found to arrange in the order of BT>3-MT>DBT. The mathematical model of sulfur adsorption on NaX zeolite was developed to predict breakthrough profiles. It considers diffusion along the column and inside the adsorbent particles. The breakthrough curve obtained from the model agrees well with the experimental data. In addition, the desorption of sulfur compounds was also studied by heating the column at 400°C. The desorptions of adsorbed 3-MT and BT were successfully achieved. NaX zeolite can be recovered almost all of the original capacity but it is not effective for DBT desorption.

บทค๊ดย่อ

จิตติมา แก้วโบราณ: การกำจัดสารประกอบกำมะถั่นออกจากน้ำมันเชื้อเพลิงโดยการคูด ซับบนโซเดียมเอ็กซ์ซีโอไลท์ในระบบแบบต่อเนื่อง (Continuous Removal of Thiophenic Sulfur Compounds from Transportation Fuels by Using X Zeolite) อ. ที่ปรึกษา: ผศ. คร. ปมทอง มาลากุล ณ อยุธยา, คร. โซฟิ จูเลียน และ คร. รพีพงศ์ สุวรรณวรางกูร 94 หน้า ISBN 974-9937-42-2

ปัจจุบันกฎระเบียบค้านสิ่งแวคล้อมที่เข้มงวคทำให้น้ำมันเชื้อเพลิงที่มีกำมะถันใน ปริมาณต่ำเป็นพิเศษเป็นที่ต้องการมากขึ้น ในช่วงที่ผ่านมากระบวนการคูคซับจึงได้รับความสนใจ ในการกำจัดสารประกอบกำมะถั่นประเภทที่กำจัดได้ยากซึ่งไม่สามารถกำจัดได้โดยวิธีไฮโดรดี ซัลเฟอร์ไรเซชั่น (Hydrodesulfurization) งานวิจัยนี้เป็นการศึกษาการคูคซับสารประกอบ กำมะถั่นประเภทไทโอฟีน 3 ชนิค คือ 3-เมทิลไทโอฟีน เบนโซไทโอฟีน และไคเบนโซไทโอฟีน ในระบบแบบต่อเนื่องโดยใช้ตัวคูดซับ คือ โซเดียมเอ็กส์ซีโอไลท์ (NaX zeolite) และใช้ดีเกน และ ไอโซออกเทน เป็นแบบจำลองของน้ำมันเชื้อเพลิงคีเซลและแก๊สโซลีนตามลำคับ โคยศึกษา ผลกระทบของความเข้มข้นตั้งต้นของสารประกอบกำมะถันและชนิดของสารประกอบกำมะถันที่ มีผลต่อกราฟการเบรคทรู ผลการทคลองแสคงให้เห็นว่าเมื่อความเข้มข้นตั้งต้นของสารประกอบ กำมะถันในสารละลายสูงขึ้น ความชั้นของกราฟการเบรคทรูมีแนวโน้มเพิ่มขึ้น แต่ระยะเวลาใน การเบรคทรูจะสั้นลง เมื่อเปรียบเทียบระยะเวลาในการเบรคทรูของสารประกอบกำมะถันทั้ง 3 ชนิดพบว่าลดลงตามลำดับดังนี้ เบนโซไทโอฟีน>3-เมทิลไทโอฟีน>ไดเบนโซไทโอฟีน สำหรับ การพัฒนาแบบจำลองทางคณิตศาสตร์เพื่อทำนายกราฟการเบรคทรูของการคูคซับของ สารประกอบกำมะถั่นบนโซเคียมเอ็กซ์ซีโอไลท์นั้นได้พิจารณาทั้งการแพร่ผ่านของสารประกอบ กำมะถันทั้งภายในหอดูคซับและภายในซีโอไลท์ ผลที่ได้จากแบบจำลองทางคณิตศาสตร์ สอคกล้องกับผลการทคลองภายใต้สภาวะต่างๆ นอกจากนี้ได้ทำการศึกษาการฟื้นฟูสภาพและการ นำตัวคูคซับกลับมาใช้ใหม่ที่อุณหภูมิ 400 องศาเซลเซียส ซึ่งพบว่าสามารถฟื้นฟูความสามาถใน การคูคซับของโซเคียมเอ็กซ์ซีโอไลท์ได้ดีในกรณีของ 3-เมทิลไทโอฟีน และเบนโซไทโอฟีน แต่ ยังไม่มีประสิทธิภาพดีพอสำหรับไดเบนโซไทโอฟีน

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ACKNOWLEDGEMENTS

This thesis can not be successful without the participation and support from the following individuals and organization. First of all, I would like to express my deepest appreciation to Asst. Prof. Pomthong Malakul, Dr. Rapeepong Suwanwarangkul, my thesis advisors, for their enlighten, suggestions, invaluable guidance, understanding and strong encouragement throughout the course of this research. This thesis would never have been completed without their consistent help. The others that could not be forgotten in this work is Dr. Sophie Jullian. I would like give special thanks to her for valuable suggestions and comments on this research.

I would also thank Asst. Prof. Apanee Luengnaruemitchai and Dr. Siriporn Jongpatiwut for kindly serving on my thesis commitee.

I would like to extend my sincere thank to all of my professors who guided me through their courses, establishing the knowledge needed for this thesis.

It is pleasure to acknowledge the Petroleum and Petrochemical College for their support in laboratory facilities and all of the staff of the college for their helpful assistance.

I am grateful for the partial scholarship and partial funding of the thesis work provided by Postgraduate Education and Research Programs in Petroleum and Petrochemical Technology (PPT Consortium).

I would like to express my special thank to the Environmental Engineering Association of Thailand (EEAT) for partial financial support.

Finally, I would like to take this opportunity to thank PPC Ph.D students and all my PPC friends. I had the most enjoyable time working with all of them. And also unforgettable thanks are forwarded to my family for their endless support, love and understanding.

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LIST OF SYMBOLS

SYMBOL

\boldsymbol{A}	cross sectional area of column (m2)
c_b	adsorbate concentration in mobile phase (mole m ⁻³)
c_p	adscrbate concentration in macropores of the pellet (mole m ⁻³)
C_i	total sulfur concentration in the feed (ppmw)
C(t)	effluent total sulfur concentration (ppmw) at any time
d_p	average pellet diameter (m)
D	combined diffusivity inside the macro-pores of the
	zeolites pellet (m ² s ⁻¹)
D_{AB}	molecular diffusivity (m ² s ⁻¹)
D_c	diffusivity of the adsorbate within the crystal (m ² s ⁻¹)
D_k	Knudsen diffusivity (m ² s ⁻¹)
D_L	axial dispersion coefficient (m ² s ⁻¹)
D_p	effective diffusivity inside the pores (m ² s ⁻¹)
\boldsymbol{k}	adsorption equilibrium constant (m ³ mole ⁻¹)
k_a	adsorption rate constant (s ⁻¹)
k_d	desorption rate constant (s ⁻¹)
K	equilibrium or partition coefficient between macro
	and micro-pores volume
K_m	average mass transfer coefficient (m s ⁻¹).
madsorbent	weight of adsorbent bed (g)
M_B	molecular weight of solvent (g mole-1)
MW_{sulfur}	molecular weight of sulfur (g mole-1)
N_R	molar diffusion flux in the radial direction of the pellet
	$(\text{mol m}^{-2} \text{ s}^{-1})$
n	Freundlich exponent
Pe_{Mp}	molecular mass Peclet numbe
q	amount of adsorbed (mole g ⁻¹ adsorbent)

SYMBOLS

q_c	concentration of the adsorbate inside the crystal (mol m ⁻³)
$\frac{1}{q_c}$	average concentration of the adsorbate inside
16	the crystal (mol m ⁻³)
2	maximum amount of adsorbed (mole g ⁻¹ adsorbent)
a_{max}	maximum amount of adsorbed (mole g adsorbent)
r	radial co-ordinate in the crystal (m)
R	radial co-ordinate in the particle (m)
R_c	crystal radius (m)
Re	Reynold number
R_p	pellet radius (m)
Sc	Schmidt number
Sh	Sherwood number
t	time (s)
T	temperature (°C)
Q	volumetric flow rate of feed stream (cm ³ min ⁻¹)
V_{bA}	molar volume of solute (cm ³ mole ⁻¹)
v_z	interstitial fluid velocity (m s ⁻¹)
X_{i}	total sulfur fraction (by weight) in the feed
z	distance measure from column inlet (m)

GREEK LETTERS

ϵ_b	voidage of adsorbent bed
ϵ_b	voidage of pellet
$\mu_{ m B}$	viscosity of solvent (centipoise)
ρ_{fuel}	fuel density at room temperature (g cm ⁻³)
Ø	association parameter
τ	tortuosity factor