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APPENDICES

APPENDIX A

A.1 The Matrices $\mathbf{R}(\xi, z, s)$ and $\mathbf{S}(\xi, z, s)$

The matrices \mathbf{R} and \mathbf{S} in eqns (2.15) and (2.16), respectively, are given by (Senjuntichai and Rajapakse, 1995)

$$\mathbf{R} = [\mathbf{R}_1 : \mathbf{R}_2] \quad (\text{A1})$$

$$\mathbf{S} = [\mathbf{S}_1 : \mathbf{S}_2] \quad (\text{A2})$$

where

$$\mathbf{R}_1 = \begin{bmatrix} -2\mu\alpha_3\eta\delta_2e^{\gamma z} & -2\mu\alpha_3\eta\delta_2e^{-\gamma z} & a_1ze^{\xi z} & -a_1ze^{-\xi z} \\ 0 & 0 & 0 & 0 \\ 2\mu\alpha_3\eta\delta_1e^{\gamma z} & -2\mu\alpha_3\eta\delta_1e^{-\gamma z} & -(a_1z - \frac{a_2}{\xi})e^{\xi z} & -(a_1z + \frac{a_2}{\xi})e^{-\xi z} \\ 2\mu\alpha_3\eta e^{\gamma z} & 2\mu\alpha_3\eta e^{-\gamma z} & -2\mu\alpha_4\eta e^{\xi z} & -2\mu\alpha_4\eta e^{-\xi z} \end{bmatrix} \quad (\text{A3})$$

$$\mathbf{R}_2 = \frac{1}{2} \begin{bmatrix} e^{\xi z} & e^{-\xi z} & -e^{\xi z} & -e^{-\xi z} \\ e^{\xi z} & e^{-\xi z} & e^{\xi z} & e^{-\xi z} \\ -e^{\xi z} & e^{-\xi z} & e^{\xi z} & -e^{-\xi z} \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (\text{A4})$$

$$\mathbf{S}_1 = \mu \begin{bmatrix} -4\mu\alpha_3\xi\eta\delta_1e^{\gamma z} & 4\mu\alpha_3\xi\eta\delta_1e^{-\gamma z} & (2a_1\xi z - 1)e^{\xi z} & (2a_1\xi z + 1)e^{-\xi z} \\ 0 & 0 & 0 & 0 \\ 4\mu\alpha_3\xi\eta\delta_2e^{\gamma z} & 4\mu\alpha_3\xi\eta\delta_2e^{-\gamma z} & -2(a_1\xi z - a_4)e^{\xi z} & 2(a_1\xi z + a_4)e^{-\xi z} \\ -2a_3\delta_1e^{\gamma z} & 2a_3\delta_1e^{-\gamma z} & 2a_4\delta_2e^{\xi z} & -2a_4\delta_2e^{-\xi z} \end{bmatrix}$$

(A5)

$$S_2 = \frac{\mu}{2} \begin{bmatrix} 2\xi e^{\xi z} & -2\xi e^{-\xi z} & -2\xi e^{\xi z} & 2\xi e^{-\xi z} \\ \xi e^{\xi z} & -\xi e^{-\xi z} & \xi e^{\xi z} & -\xi e^{-\xi z} \\ -2\xi e^{\xi z} & -2\xi e^{-\xi z} & 2\xi e^{\xi z} & 2\xi e^{-\xi z} \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (A6)$$

and

$$a_1 = \frac{1}{2(1-2\nu_u)} \quad (A7)$$

$$a_2 = \frac{(3-4\nu_u)}{2(1-2\nu_u)} \quad (A8)$$

$$a_3 = \frac{B(1+\nu_u)(1-\nu)}{3(\nu_u-\nu)} \quad (A9)$$

$$a_4 = \frac{(1-\nu_u)}{(1-2\nu_u)} \quad (A10)$$

$$c = 2\mu a_3 \kappa \eta \quad (A11)$$

$$\eta = \frac{B(1+\nu_u)}{3(1-\nu_u)} \quad (A12)$$

$$\delta_1 = \frac{\kappa \gamma \eta}{s} \quad (A13)$$

$$\delta_2 = \frac{\kappa \xi \eta}{s} \quad (A14)$$

APPENDIX B

B.1 Formulation of Bending Moment and Shear Force of Axisymmetric Circular Plate

The bending moment of the plate per unit length (Timoshenko and Woinowsky-Krieger, 1959)

$$M_r = -D \left(\frac{d^2 w}{dr^2} + \frac{\nu_p}{r} \frac{dw}{dr} \right) \quad (\text{B1})$$

$$Q = -D \left(\frac{d^3 w}{dr^3} + \frac{1}{r} \frac{d^2 w}{dr^2} - \frac{1}{r^2} \frac{dw}{dr} \right) \quad (\text{B2})$$

From eqn(2.43) ; $w(r,t) = a_0(t)r^2 \ln r + \alpha_0 + \sum_{n=1}^N \alpha_n(t)r^{2n}$, $0 \leq r \leq 1$

$$\frac{dw}{dr} = a_0(r + 2r \ln r) + \sum_{n=1}^N 2n \alpha_n r^{2n-1} \quad (\text{B3})$$

$$\frac{d^2 w}{dr^2} = a_0(3 + 2 \ln r) + \sum_{n=1}^N 2n(2n-1) \alpha_n r^{2n-2} \quad (\text{B4})$$

$$\frac{d^3 w}{dr^3} = a_0 \left(3 + \frac{2}{r} \right) + \sum_{n=2}^N 2n(2n-1)(2n-2) \alpha_n r^{2n-3} \quad (\text{B5})$$

Substitute eqns(B3) - (B5) into eqns(B1) and (B2) we have

$$M_r(r,t) = -D \left\{ a_0(3 + 2 \ln r + \nu_p + 2 \nu_p \ln r) + \sum_{n=1}^N \alpha_n [2n(2n-1) + 2n\nu_p] r^{2n-2} \right\} \quad (\text{B6})$$

$$Q(r,t) = -D \left[\frac{4a_0}{r} + \sum_{n=2}^N 4n^2(2n-2)\alpha_n r^{2n-3} \right] \quad (\text{B7})$$

B.2 Formulation of Strain Energy of Plate

$$\text{From} \quad U_p = \int_0^1 \pi D \left[\left(\frac{d^2 w}{dr^2} + \frac{1}{r} \frac{dw}{dr} \right)^2 - \frac{2(1-\nu_p)}{r} \frac{dw}{dr} \frac{d^2 w}{dr^2} \right] r dr \quad (\text{B8})$$

$$\text{and from} \quad \frac{1}{r} \frac{dw}{dr} = a_0(1 + 2 \ln r) + \sum_{n=1}^N 2n\alpha_n r^{2n-2} \quad (\text{B9})$$

$$\frac{d^2 w}{dr^2} + \frac{1}{r} \frac{dw}{dr} = a_0(4 + 4 \ln r) + \sum_{n=1}^N 4n^2 \alpha_n r^{2n-2} \quad (\text{B10})$$

$$\begin{aligned} \left(\frac{d^2 w}{dr^2} + \frac{1}{r} \frac{dw}{dr} \right)^2 &= a_0^2(4 + 4 \ln r)^2 + 2a_0(4 + 4 \ln r) \cdot \sum_{n=1}^N 4n^2 \alpha_n r^{2n-2} \\ &\quad + \sum_{n=1}^N 4n^2 \alpha_n r^{2n-2} \cdot \sum_{n=1}^N 4n^2 \alpha_n r^{2n-2} \end{aligned} \quad (\text{B11})$$

$$\frac{dw}{dr} \frac{d^2 w}{dr^2} = \left[a_0(r + 2r \ln r) + \sum_{n=1}^N 2n\alpha_n r^{2n-1} \right] \left[a_0(3 + 2 \ln r) + \sum_{n=1}^N 2n(2n-1)\alpha_n r^{2n-2} \right] \quad (\text{B12})$$

$$\begin{aligned}
&= \alpha_0^2(3r + 6r \ln r + 2r \ln r + 4r(\ln r)^2) + \sum_{n=1}^N 2\alpha_0(3 + 2 \ln r)n\alpha_n r^{2n-1} \\
&+ \sum_{n=1}^N \alpha_0(r + 2r \ln r)2n(2n-1)\alpha_n r^{2n-2} + \sum_{n=1}^N 2n\alpha_n r^{2n-1} \cdot \sum_{n=1}^N 2n(2n-1)\alpha_n r^{2n-2}
\end{aligned} \tag{B13}$$

Substitute (B11) and (B13) into (B8) we have

$$U_p = \int_0^1 \pi D \left\{ \begin{aligned} &\left[\alpha_0^2 r(4 + 4 \ln r)^2 + 2\alpha_0(4 + 4 \ln r) \sum_{n=1}^N 4n^2 \alpha_n r^{2n-1} \right. \\ &\left. + \sum_{n=1}^N 4n^2 \alpha_n r^{2n-1} \sum_{n=1}^N 4n^2 \alpha_n r^{2n-1} \right] \\ &- 2(1 - \nu_p) \left[\alpha_0^2(3r + 8r \ln r + 4r(\ln r)^2) + \sum_{n=1}^N 2\alpha_0 n \alpha_n r^{2n-1} (2 + 2n + 4n \ln r) + \right. \\ &\left. \sum_{n=1}^N 2n \alpha_n r^{2n-1} \sum_{n=1}^N 2n(2n-1)\alpha_n r^{2n-2} \right] \end{aligned} \right\} dr \tag{B14}$$

After Integration and rewritten eqn.(B14) in term of i, j where $i, j = 2$ to $N+1$

$$\begin{aligned}
U_p &= \pi D \left[4\alpha_0^2 - 2(1 - \nu_p) \frac{\alpha_0^2}{2} \right] + \pi D \left[\{8\alpha_0(2i-3)\}^T \{\alpha\} - 2(1 - \nu_p) \{2\alpha_0(i-1)\}^T \{\alpha\} \right] \\
&+ \pi D \left[\{\alpha\}^T \left\{ \frac{4(i-1)^2 4(j-1)^2}{2i+2j-6} \right\} \{\alpha\} - 2(1 - \nu_p) \{\alpha\}^T \left\{ \frac{4(i-1)(j-1)(2j-3)}{2i+2j-6} \right\} \{\alpha\} \right]
\end{aligned} \tag{B15}$$

$$\begin{aligned}
U_p &= \pi D \left[(3 + \nu_p) \alpha_0^2 \right] + \{\alpha\}^T \left[\frac{4(i-1)(j-1)\pi D}{2i+2j-6} \right] \left[4(i-1)(j-1) - 2(1 - \nu_p)(2i-3) \right] \{\alpha\} \\
&+ \pi D 4\alpha_0 \left[(3 + \nu_p)i - \nu_p - 5 \right] \{\alpha\} \quad , \quad 2 \leq i, j \leq N+1
\end{aligned} \tag{B16}$$

The strain energy of the plate corresponding to the assumed displacement function can be expressed in the Laplace domain as

$$U_p = \pi D(3 + \nu_p)\bar{\alpha}_0^2 + \langle Q^p \rangle \{\bar{\alpha}\} + \{\bar{\alpha}\}^T [K^p] \{\bar{\alpha}\} \quad (\text{B17})$$

where

$$Q_1^p = 0 \quad (\text{B18})$$

$$Q_i^p = \pi D \left[4\bar{\alpha}_0 (4(i-1) - (1-\nu_p)i) - 4\bar{\alpha}_0(1+\nu_p) \right] ; 2 \leq i \leq (N+1) \quad (\text{B19})$$

$$K_{ij}^p = K_{ji}^p = 0 \quad (\text{B20})$$

$$K_{ij}^p = \frac{4(i-1)(j-1)\pi D}{(2i+2j-6)} \left[4(i-1)(j-1) - 2(1-\nu_p)(2i-3) \right] ; 2 \leq i, j \leq (N+1) \quad (\text{B21})$$

B.3 Formulation of Strain Energy of Half-Space

$$U_h = \frac{1}{2} \int_V \sigma_{ij} \varepsilon_{ij} dV \quad (B22)$$

$$U_h = \frac{1}{2} \int_0^h [2\pi r \bar{T}_z(r, H, s) \bar{w}(r, s)] dr \quad (B23)$$

where

$$\bar{T}_z(r, s) = \sum_{n=0}^N \bar{\alpha}_n(s) \tilde{T}_{nz}(r) + \bar{a}_0(s) T_z^*(r) \quad (B24)$$

So

$$U_h = \int_0^h \pi r \left[\sum_{n=0}^N \bar{\alpha}_n \tilde{T}_{nz}(r) + \bar{a}_0 T_z^*(r) \right] \bar{w}(r, s) dr \quad (B25)$$

where

$$\bar{w}(r, s) = \bar{a}_0(s) r^2 \ln r + \sum_{n=0}^N \bar{\alpha}_n(s) r^{2n}, \quad 0 \leq r \leq 1 \quad (B26)$$

$$U_h = \int_0^h \left[\begin{aligned} &\pi r \sum_{n=0}^N \bar{\alpha}_n \tilde{T}_{nz}(r) \cdot \bar{a}_0 r^2 \ln r + \pi r \bar{a}_0^2 T_z^*(r) \cdot r^2 \ln r + \pi r \sum_{n=0}^N \bar{\alpha}_n \tilde{T}_{nz}(r) \cdot \sum_{n=0}^N \bar{\alpha}_n r^{2n} \\ &+ \pi r \bar{a}_0 T_z^*(r) \cdot \sum_{n=0}^N \bar{\alpha}_n r^{2n} \end{aligned} \right] dr \quad (B27)$$

From the discretization of circular surface into M ring elements. So the above expression can be expressed in form of summation of M terms.

$$\begin{aligned} U_h = & \sum_{i=1}^M \left(\pi r_i \cdot \sum_{n=0}^N \bar{\alpha}_n \tilde{T}_{nz}(r_i) \cdot \bar{a}_0 r_i^2 \ln r_i \cdot \Delta r_i \right) + \sum_{i=1}^M \left(\pi r_i \bar{a}_0^2 \cdot T_z^*(r_i) \cdot r_i^2 \ln r_i \cdot \Delta r_i \right) \\ & + \sum_{i=1}^M \left(\pi r_i \cdot \sum_{n=0}^N \bar{\alpha}_n \tilde{T}_{nz}(r_i) \cdot \sum_{n=0}^N \bar{\alpha}_n r_i^{2n} \cdot \Delta r_i \right) + \sum_{i=1}^M \left(\pi r_i \bar{a}_0 \cdot T_z^*(r_i) \cdot \sum_{n=0}^N \bar{\alpha}_n r_i^{2n} \cdot \Delta r_i \right) \end{aligned}$$

$$\begin{aligned}
&= \sum_{l=1}^M \langle \pi r_l^3 \bar{a}_0 \tilde{T}_{z(i-1)}(r_l) \ln r_l \cdot \Delta r_l \rangle \langle \bar{\alpha} \rangle + \sum_{l=1}^M \langle \pi r_l^3 \bar{a}_0^2 T_z^*(r_l) \ln r_l \cdot \Delta r_l \rangle \\
&+ \sum_{l=1}^M \langle \bar{\alpha} \rangle^T \langle \pi r_l^{2j-1} \cdot \tilde{T}_{z(i-1)}(r_l) \rangle \langle \bar{\alpha} \rangle + \sum_{l=1}^M \langle \pi r_l^{2i-1} \bar{a}_0 T_z^*(r_l) \cdot \Delta r_l \rangle \langle \bar{\alpha} \rangle
\end{aligned}$$

$$U_h = \{\bar{\alpha}\}^T [K^h] \{\bar{\alpha}\} + \langle Q^h \rangle \{\bar{\alpha}\} + \sum_{j=1}^M \pi r_j T_j^* \bar{a}_0^2 r_j^2 \ln r_j \Delta r_j \quad (\text{B28})$$

where

$$K_{ij}^h = \sum_{l=1}^M \tilde{T}_{z(i-1)}(r_l) \cdot \pi r_l^{2j-1} \Delta r_l \quad , \quad 1 \leq i, j \leq (N+1) \quad (\text{B29})$$

$$Q_i^h = \sum_{j=1}^M \left[\pi r_j^{2i-1} T_j^* \Delta r_j + \pi r_j^3 \ln r_j \cdot \tilde{T}_{z(i-1)}(r_j) \cdot \Delta r_j \right] \bar{a}_0 \quad , \quad 1 \leq i \leq (N+1) \quad (\text{B30})$$



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BIOGRAPHY

Mr. Sukkasem Lalitkulthorn was born in Bangkok 1971. He graduated from Faculty of Engineering , Kasetsart University in 1992. He continued his study for Master Degree in Civil Engineering at Chulalongkorn University in 1994.