

CHAPTER 4

ANALYSIS

4.1 The Mathematical Model

The open loop transfer function from equation 2.9 can be rewritten as

$$G_o(s) = K_{sf} \frac{K_A}{n} G_h(s) G_m(s) \quad (4.1)$$

Substitute for

$$\begin{aligned} K_{sf} &= 0.000146 \text{ sec/rad} \\ K_A &= 21739.0 \text{ volts/sec} \\ n &= 76.56 \\ K_m &= 35.5 \text{ rad/sec/volt} \\ T_m &= 0.0149 \text{ sec} \end{aligned}$$

$$G_h(s) = \frac{1 - e^{-sT}}{s}$$

$$G_m(s) = \frac{K_m}{s(T_m s + 1)}$$

Then equation (4.1) becomes

$$G_o(s) = 1.472 \cdot \frac{1 - e^{-sT}}{s^2(T_m s + 1)} \quad (4.2)$$

$$= 1.472 (1 - e^{-sT}) \left(\frac{1}{s^2} - \frac{T_m}{s} + \frac{T_m}{s+1/T_m} \right) \quad (4.3)$$

Then

$$G_o(z) = 1.472 (1 - z^{-1}) \left(\frac{zT}{(z-1)^2} - \frac{zT_m}{z-1} + \frac{zT_m}{z - e^{-T/T_m}} \right) \quad (4.4)$$

Let $T' = T/T_m$ (4.5)

$$G_o(z) = 0.02193 \frac{(T' + e^{-T'} - 1)z + (1 - T'e^{-T'} - e^{-T'})}{(z-1)(z - e^{-T'})} \quad (4.6)$$

4.2 The Critical Sampling Period

For dead-zone $d = 1\% \times 0.92 \times 10^{-3} = 0.92 \times 10^{-5}$,

then from equation (2.25), we have

$$E\left(\frac{1}{N(z)}\right)_{\min.} = \sqrt{2} \times 0.92 \times 10^{-5} = 1.3 \times 10^{-5} \text{ sec} \quad (4.7)$$

and from section (3.7) implies that

$$V = T_{em} = 0.92 \times 10^{-3} \text{ sec} \quad (4.8)$$

Then from equation (2.24), for $E=V$, we have

$$\begin{aligned} -\frac{1}{N(z)}_{\min} &= -\frac{\pi}{4} \times 2 \times \frac{d}{E} \\ &= -\frac{\pi}{4} \times 2 \times \frac{1}{100} \\ &= -1.57 \times 10^{-2} \text{ sec} \end{aligned} \quad (4.9)$$

From equation (4.6), we can calculate the critical sampling period to be used by equating

$$-\frac{1}{N(z)} = G_0(z) \quad (4.10)$$

then

$$-1.57 \times 10^{-2} = 0.02193 \frac{(T' + e^{-T'})z + (1 - T'e^{-T'} - e^{-T'})}{(z-1)(z-e^{-T'})} \quad (4.11)$$

by substitution, we have the approximate critical sampling period as

$$T_{cr} = 30 \text{ ms.}$$

4.3 The Nyquist Diagram

From equation (4.6), we make a Nyquist plot for $G_o(z)$ at various sampling period T .

For $T = 2$ ms

$$G_o(z) = \frac{0.0001864z + 0.0001821}{(z-1)(z-0.8743)} \quad (4.12)$$

For $T = 20$ ms

$$G_o(z) = \frac{0.01322z + 0.00852}{(z-1)(z-0.2611)} \quad (4.13)$$

For $T = 50$ ms

$$G_o(z) = \frac{0.0524z + 0.01859}{(z-1)(z-0.0349)} \quad (4.14)$$

The values of $G_o(z)$ at various sampling periods and angles are tabulated as follows :

<u>z</u>	<u>T = 2 ms</u>	<u>T = 20 ms</u>	<u>T = 50 ms</u>
<u>1/45°</u>	5.720x10 ⁻⁴ /167°	0.03150 /-142.6°	0.119/168.2°
<u>1/90°</u>	1.387x10 ⁻⁴ /139.5°	0.01070 /177.6°	0.0390/-154.1°
<u>1/135°</u>	0.439x10 ⁻⁴ /114.2°	0.00423/148.7°	0.0118/-160.7°
<u>1/180°</u>	1.147x10 ⁻⁶ /180°	0.00186/180°	0.0163/180°
<u>1/270°</u>	1.387x10 ⁻⁴ /-139.5°	0.01070/-177.6°	0.0390/154.1°
<u>1/360°</u>	∞	∞	∞

4.4. Summary

The Nyquist plots for the open loop system at various sampling periods are shown in Figure 4.1, 4.2 and 4.3. The system is found to be stable for 2 ms and 20 ms sampling intervals. For the sampling interval of 50 ms the system is not stable, since the $G_o(z)$ locus encircles the $-\frac{1}{N(z)}$ locus.

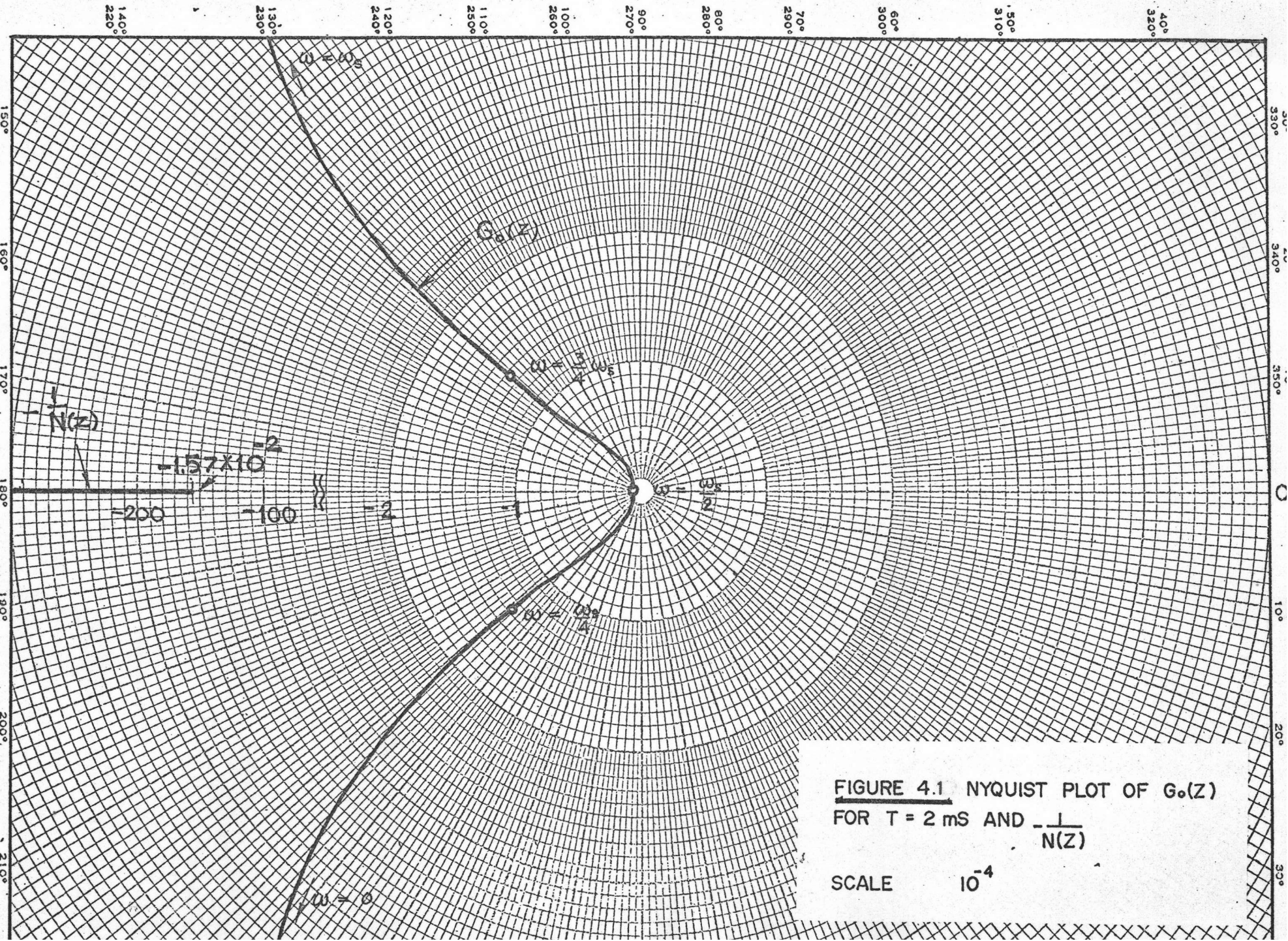


FIGURE 4.1 NYQUIST PLOT OF $G_o(z)$
 FOR $T = 2 \text{ ms}$ AND $\frac{1}{N(z)}$

SCALE 10^{-4}

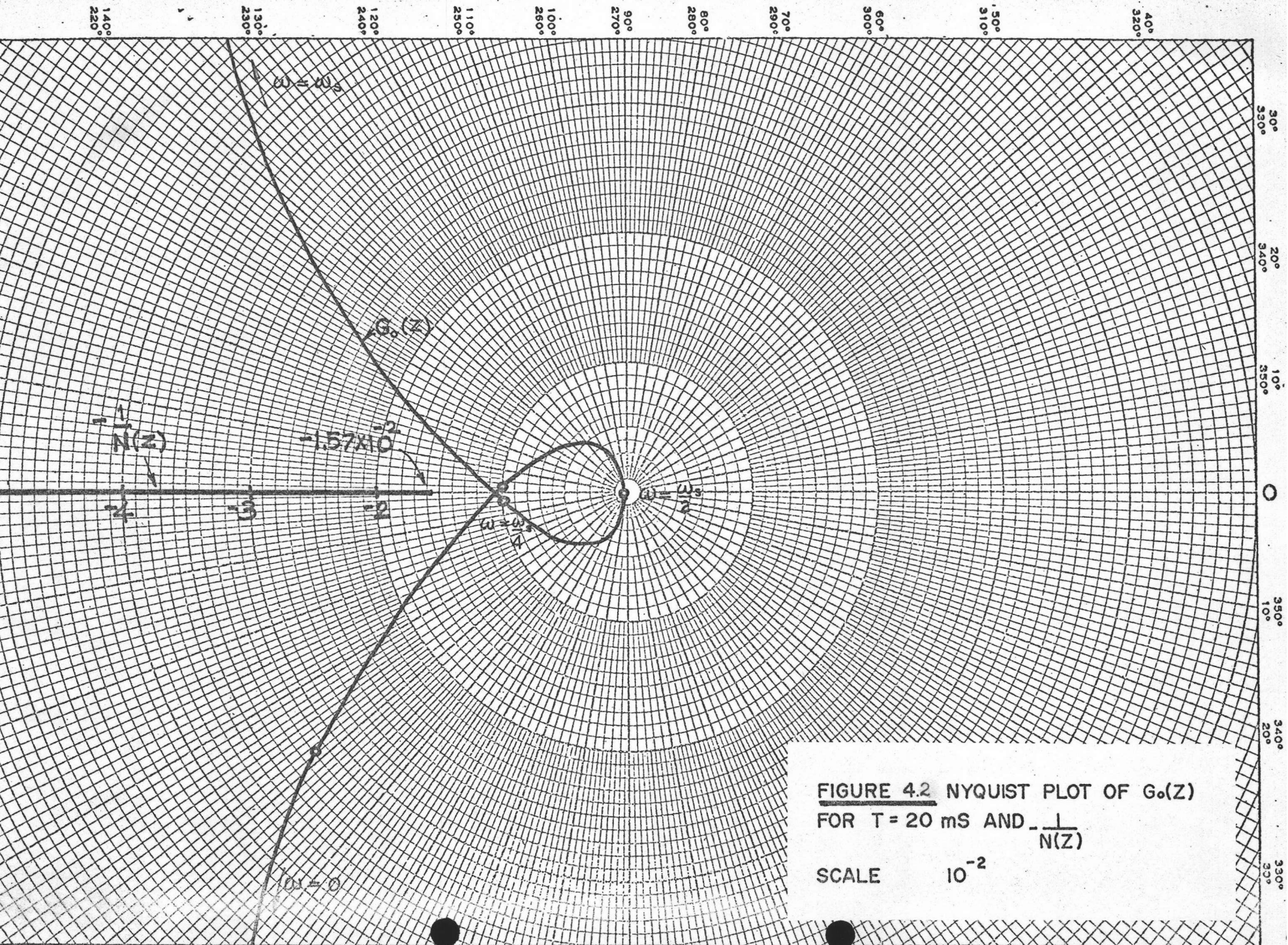


FIGURE 4.2 NYQUIST PLOT OF $G_o(z)$
 FOR $T = 20$ mS AND $\frac{1}{N(z)}$
 SCALE 10^{-2}

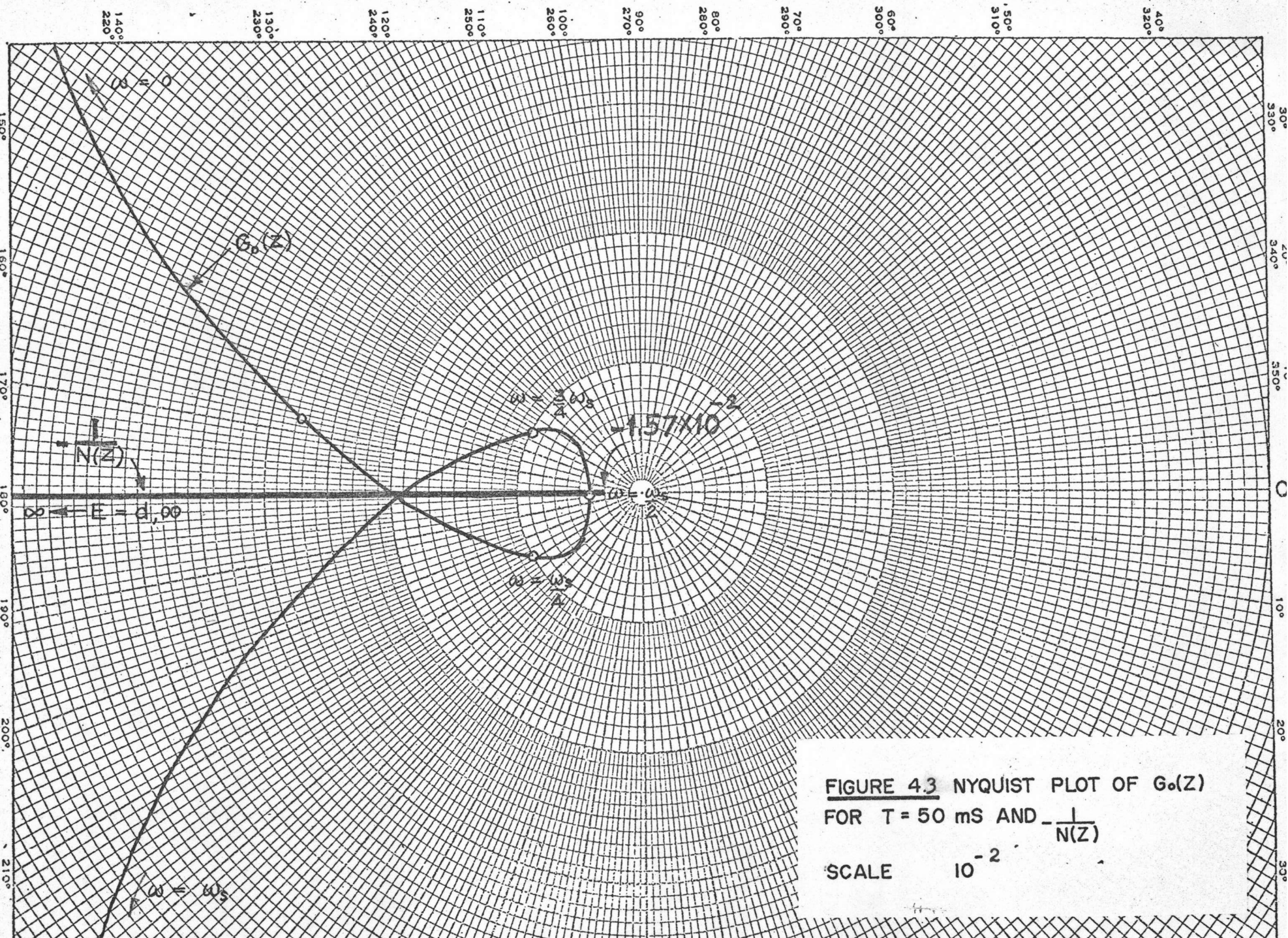


FIGURE 4.3 NYQUIST PLOT OF $G_o(z)$
 FOR $T = 50$ ms AND $-\frac{1}{N(z)}$
 SCALE 10^{-2}