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## APPENDICES

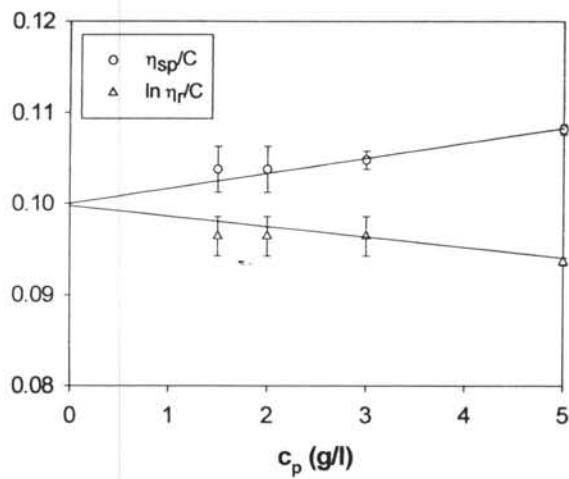
### Appendix A Viscosity Data for Aqueous PEO, HTAC, PEO-HTAC, PEO-HTAC-NaSal solutions at 30°C

#### A1 Viscosity data for aqueous PEO solutions at 30°C

##### *A1.1 PEO (quoted $M_w = 1.0 \times 10^5$ g/mol)*

$c_p$ (g/l)	$\eta_{sp}/c$ (l/g)						[ $\eta$ ] l/g	$K_H$
	Run 1	Run 2	Run 3	Run 4	Run 5	Std.deviation ( $\pm$ )		
1.5	0.1006	0.0989	0.0995	0.1104	0.1094	0.0056		
2.0	0.1077	0.1032	0.1020	0.1055	0.1055	0.0022	0.100	0.27
3.0	0.1080	0.1073	0.1067	0.1094	0.1095	0.0012		
5.0	0.1149	0.1145	0.1144	0.1168	0.1162	0.0011		

$c_p$ (g/l)	$\ln \eta_r/c$ (l/g)						[ $\eta$ ] l/g	$K_H$
	Run 1	Run 2	Run 3	Run 4	Run 5	Std.deviation ( $\pm$ )		
1.5	0.0937	0.0922	0.0928	0.1022	0.1013	0.0049		
2.0	0.0976	0.0938	0.0928	0.0957	0.0958	0.0019	0.100	0.27
3.0	0.0936	0.0930	0.0925	0.0946	0.0947	0.0010		
5.0	0.0908	0.0906	0.0905	0.0920	0.0916	0.0007		

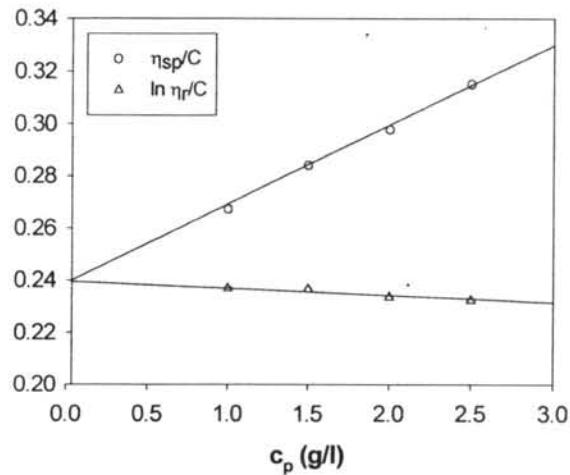


**Figure 1.1**  $\eta_{sp}/c$  and  $\ln \eta_r/c$  as a function of PEO concentration,  $c_p$  for PEO ( $M_w = 1.0 \times 10^5$  g/mol) at 30°C.

*A1.2 PEO (quoted  $M_w = 3.0 \times 10^5$  g/mol)*

$c_p$ (g/l)	$\eta_{sp}/c$ (l/g)				[ $\eta$ ] l/g	$K_H$
	Run 1	Run 2	Run 3	Std.deviation ( $\pm$ )		
1.0	0.2657	0.2680	0.2679	0.0013		
1.5	0.2850	0.2841	0.2830	0.0010	0.240	0.28
2.0	0.2989	0.2968	0.2975	0.0011		
2.5	0.3161	0.3149	0.3142	0.0010		

$c_p$ (g/l)	$\ln \eta_r/c$ (l/g)				[ $\eta$ ] l/g	$K_H$
	Run 1	Run 2	Run 3	Std.deviation ( $\pm$ )		
1.5	0.2356	0.2375	0.2374	0.0011		
2.0	0.2373	0.2367	0.2359	0.0007	0.240	0.28
3.0	0.2343	0.2330	0.2335	0.0007		
5.0	0.2330	0.2323	0.2319	0.0006		

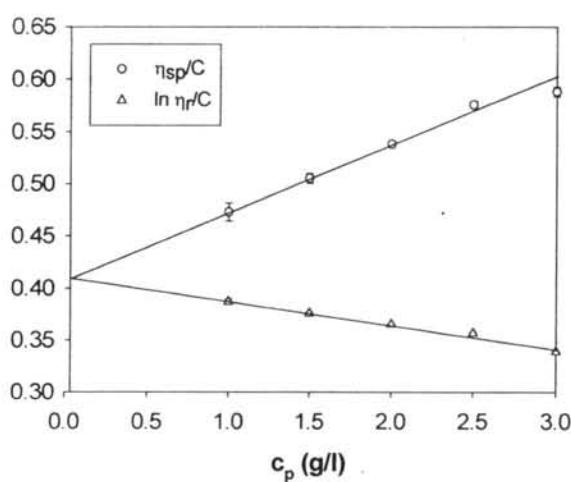


**Figure 1.2**  $\eta_{sp}/c$  and  $\ln \eta_r/c$  as a function of PEO concentration,  $c_p$  for PEO ( $M_w = 3.0 \times 10^5$  g/mol) at 30°C.

*A1.3 PEO (quoted  $M_w = 6.0 \times 10^5$  g/mol)*

$c_p$ (g/l)	$\eta_{sp}/c$ (l/g)						[ $\eta$ ] l/g	$K_H$
	Run 1	Run 2	Run 3	Run 4	Run 5	Std.deviation ( $\pm$ )		
1.0	0.4875	0.4706	0.4650	0.4717	0.4687	0.0087		
1.5	0.5059	0.5035	0.5133	0.5026	0.5009	0.0049		
2.0	0.5413	0.5379	0.5347	0.5402	0.5373	0.0026	0.412	0.37
2.5	0.5730	0.5800	0.5762	0.5722	0.5776	0.0032		
3.0	0.5876	0.5957	0.5879	0.5861	0.5836	0.0045		

$c_p$ (g/l)	$\ln \eta_r/c$ (l/g)						[ $\eta$ ] l/g	$K_H$
	Run 1	Run 2	Run 3	Run 4	Run 5	Std.deviation ( $\pm$ )		
1.0	0.3971	0.3857	0.3819	0.3864	0.3844	0.0058		
1.5	0.3764	0.3751	0.3806	0.3746	0.3736	0.0027		
2.0	0.3668	0.3652	0.3636	0.3663	0.3649	0.0013	0.412	0.37
2.5	0.3556	0.3584	0.3569	0.3552	0.3575	0.0013		
3.0	0.3387	0.3417	0.3389	0.3382	0.3373	0.0017		

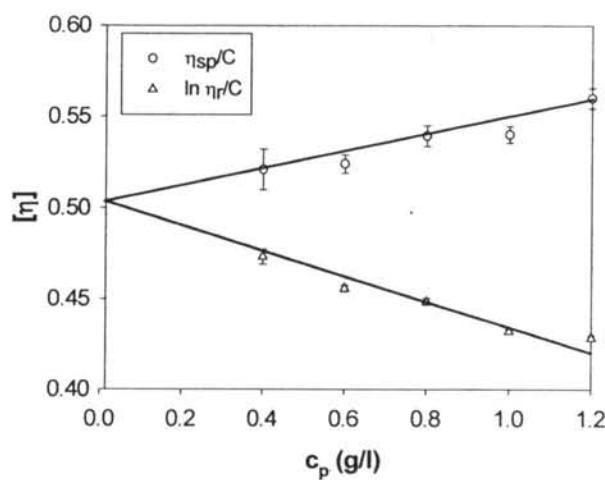


**Figure 1.3**  $\eta_{sp}/c$  and  $\ln \eta_r/c$  as a function of PEO concentration,  $c_p$  for PEO ( $M_w = 6.0 \times 10^5$  g/mol) at 30°C.

*A1.4 PEO (quoted  $M_w = 9.0 \times 10^5$  g/mol)*

$c_p$ (g/l)	$\eta_{sp}/c$ (l/g)						$[\eta]$ l/g	$K_H$
	Run 1	Run 2	Run 3	Run 4	Run 5	Std.deviation ( $\pm$ )		
0.4	0.5317	0.5231	0.5023	0.5215	0.5256	0.0111		
0.6	0.5236	0.5232	0.5170	0.5312	0.5249	0.0051		
0.8	0.5468	0.5407	0.5322	0.5354	0.5417	0.0057	0.503	0.26
1.0	0.5427	0.5400	0.5320	0.5430	0.5425	0.0047		
1.2	0.5636	0.5634	0.5507	0.5629	0.5589	0.0055		

$c_p$ (g/l)	$\ln \eta_r/c$ (l/g)						$[\eta]$ l/g	$K_H$
	Run 1	Run 2	Run 3	Run 4	Run 5	Std.deviation ( $\pm$ )		
0.4	0.4821	0.4750	0.4578	0.4737	0.4771	0.0092		
0.6	0.4553	0.4551	0.4503	0.4611	0.4563	0.0038		
0.8	0.4536	0.4493	0.4433	0.4456	0.4501	0.0040	0.503	0.26
1.0	0.4336	0.4318	0.4266	0.4338	0.4334	0.0030		
1.2	0.4305	0.4304	0.4228	0.4301	0.4277	0.0033		

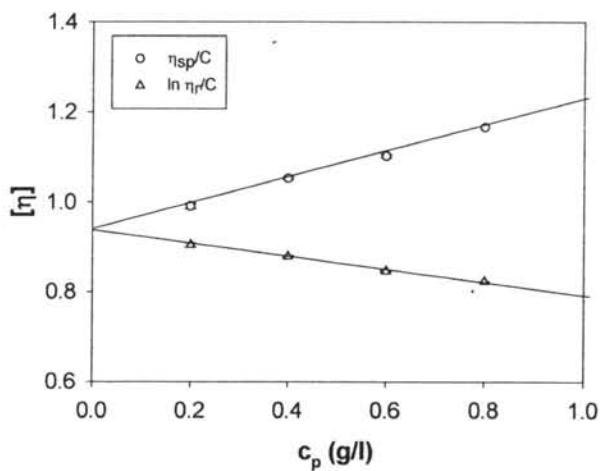


**Figure 1.4**  $\eta_{sp}/c$  and  $\ln \eta_r/c$  as a function of PEO concentration,  $c_p$  for PEO ( $M_w = 9.0 \times 10^5$  g/mol) at 30°C.

*A1.5 PEO (quoted  $M_w = 4.0 \times 10^6$  g/mol)*

$c_p$ (g/l)	$\eta_{sp}/c$ (l/g)				$[\eta]$ l/g	$K_H$
	Run 1	Run 2	Run 3	Std.deviation ( $\pm$ )		
0.2	0.9904	0.9808	1.0015	0.0104		
0.4	1.0472	1.0570	1.0541	0.0050	0.9500	0.31
0.6	1.1093	1.1006	1.0977	0.0060		
0.8	1.1664	1.1664	1.1664	0.0000		

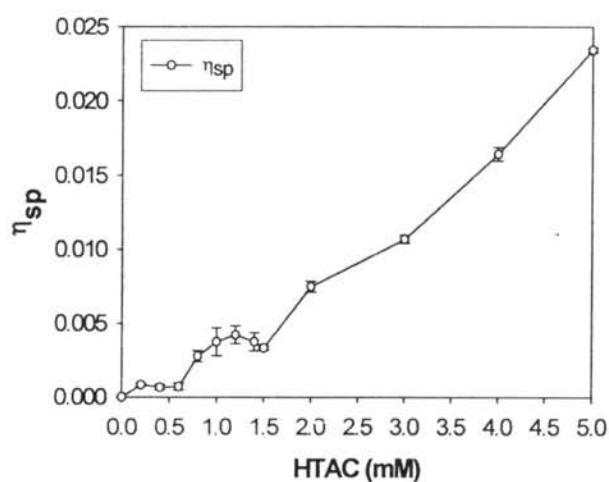
$c_p$ (g/l)	$\ln \eta_r/c$ (l/g)				$[\eta]$ l/g	$K_H$
	Run 1	Run 2	Run 3	Std.deviation ( $\pm$ )		
0.2	0.9036	0.8956	0.9128	0.0086		
0.4	0.8747	0.8816	0.8795	0.0035	0.9500	0.31
0.6	0.8503	0.8450	0.8433	0.0037		
0.8	0.8239	0.8239	0.8239	0.0000		



**Figure 1.5**  $\eta_{sp}/c$  and  $\ln \eta_r/c$  as a function of PEO concentration,  $c_p$  for PEO ( $M_w = 40.0 \times 10^5$  g/mol) at 30°C.

**A2 Viscosity data for aqueous HTAC solutions at 30°C**

HTAC (mM)	$\eta_{sp}$			
	Run 1	Run 2	Run 3	Std. deviation ( $\pm$ )
0.00	0.0000	0.0000	0.0000	0.0000
0.20	0.0011	0.0007	0.0008	0.0002
0.40	0.0009	0.0003	0.0007	0.0003
0.60	0.0011	0.0008	0.0002	0.0005
0.80	0.0027	0.0035	0.0022	0.0007
1.00	0.0038	0.0021	0.0053	0.0016
1.20	0.0040	0.0033	0.0053	0.0010
1.40	0.0050	0.0031	0.0031	0.0011
1.50	0.0035	0.0034	0.0031	0.0002
2.00	0.0000	0.0078	0.0068	0.0042
3.00	0.0102	0.0111	0.0108	0.0005
4.00	0.0171	0.0155	0.0167	0.0008
5.00	0.0232	0.0234	0.0238	0.0003

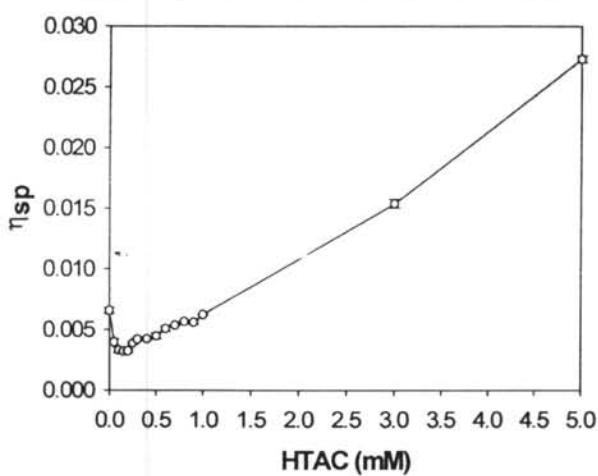


**Figure 2.1**  $\eta_{sp}$  as a function of HTAC concentration in aqueous solutions at 30°C.

### A3 Viscosity data for aqueous PEO-HTAC solutions at 30°C

*A3.1 Viscosity data for aqueous PEO1\_40 ppm - HTAC solutions at 30°C  
(PEO1 = PEO  $M_w$   $0.91 \times 10^5$  g/mol)*

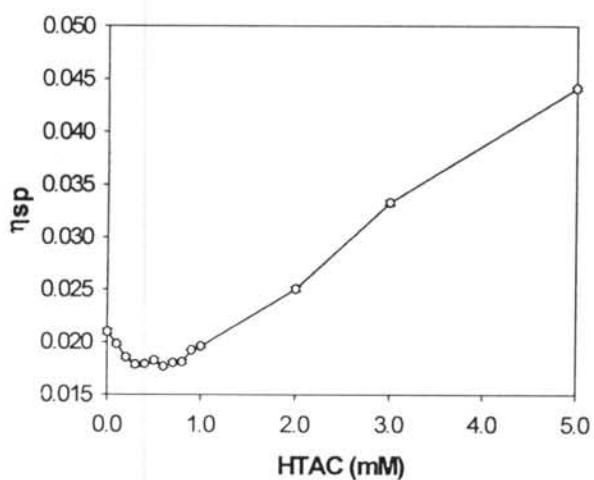
HTAC (mM)	$\eta_{sp}$			
	Run 1	Run 2	Run 3	Std. deviation ( $\pm$ )
0.000	0.0062	0.0070	0.0065	0.0004
0.05	0.0037	0.0037	0.0045	0.0005
0.10	0.0033	0.0037	0.0030	0.0004
0.15	0.0032	0.0034	0.0031	0.0002
0.20	0.0035	0.0032	0.0031	0.0002
0.25	0.0040	0.0040	0.0037	0.0002
0.30	0.0042	0.0041	0.0044	0.0002
0.40	0.0042	0.0041	0.0045	0.0002
0.50	0.0049	0.0041	0.0045	0.0004
0.60	0.0054	0.0047	0.0052	0.0004
0.70	0.0054	0.0054	0.0053	0.0001
0.80	0.0057	0.0058	0.0056	0.0001
0.90	0.0059	0.0053	0.0057	0.0003
1.00	0.0063	0.0063	0.0062	0.0001
3.00	0.0149	0.0152	0.0161	0.0006
5.00	0.0268	0.0278	0.0272	0.0005



**Figure 3.1**  $\eta_{sp}$  as a function of PEO1\_40 ppm + HTAC in aqueous solutions at 30°C.

*A3.2 Viscosity data for aqueous PEO1\_200 ppm - HTAC solutions at 30°C  
(PEO1 = PEO  $M_w$   $0.91 \times 10^5$  g/mol)*

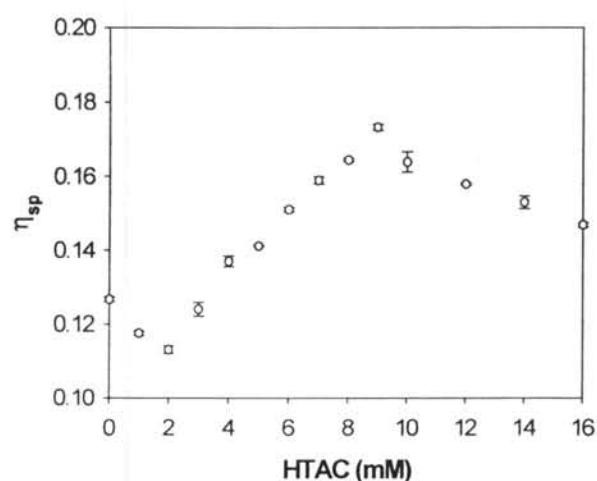
HTAC (mM)	$\eta_{sp}$			
	Run 1	Run 2	Run 3	Std. deviation ( $\pm$ )
0.00	0.0211	0.0213	0.0205	0.0004
0.10	0.0195	0.0198	0.0201	0.0003
0.20	0.0183	0.0186	0.0188	0.0003
0.30	0.0176	0.0176	0.0183	0.0004
0.40	0.0179	0.0180	0.0179	0.0001
0.50	0.0186	0.0182	0.0180	0.0003
0.60	0.0175	0.0179	0.0177	0.0002
0.70	0.0179	0.0184	0.0178	0.0003
0.80	0.0184	0.0181	0.0178	0.0003
0.90	0.0193	0.0192	0.0192	0.0001
1.00	0.0199	0.0195	0.0194	0.0003
2.00	0.0255	0.0250	0.0247	0.0004
3.00	0.0329	0.0334	0.0337	0.0004
5.00	0.0439	0.0442	0.0443	0.0002



**Figure 3.2**  $\eta_{sp}$  as a function of PEO1\_200 ppm + HTAC in aqueous solutions at 30°C.

*A3.3 Viscosity data for aqueous PEO1\_1000 ppm - HTAC solutions at 30°C*  
*(PEO1 = PEO  $M_w$  0.91 x 10<sup>5</sup> g/mol)*

HTAC (mM)	$\eta_{sp}$			
	Run 1	Run 2	Run 3	Std. deviation ( $\pm$ )
0.00	0.1275	0.1271	0.1254	0.0011
1.00	0.1183	0.1180	0.1163	0.0011
2.00	0.1151	0.1123	0.1118	0.0018
3.00	0.1274	0.1209	0.1239	0.0033
4.00	0.1399	0.1354	0.1357	0.0025
5.00	0.1410	0.1413	0.1410	0.0002
6.00	0.1500	0.1513	0.1518	0.0009
7.00	0.1582	0.1578	0.1609	0.0017
8.00	0.1652	0.1640	0.1641	0.0007
9.00	0.1745	0.1716	0.1736	0.0015
10.00	0.1608	0.1615	0.1693	0.0047
12.00	0.1578	0.1573	0.1585	0.0006
14.00	0.1562	0.1524	0.1503	0.0030
16.00	0.1479	0.1467	0.1457	0.0011

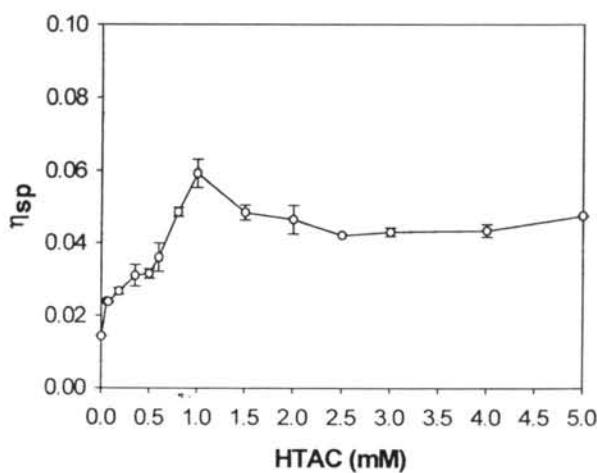


**Figure 3.3**  $\eta_{sp}$  as a function of PEO1\_1000 ppm + HTAC in aqueous solutions at 30°C.

*A3.4 Viscosity data for aqueous PEO6\_40 ppm - HTAC solutions at 30°C*

(PEO6 = PEO  $M_w$   $6.06 \times 10^5$  g/mol)

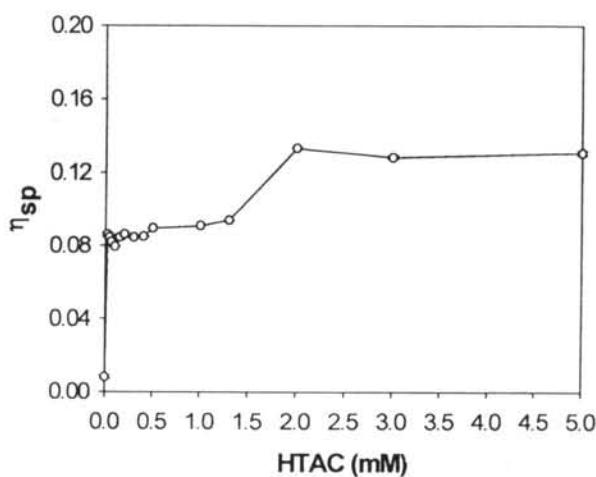
HTAC (mM)	$\eta_{sp}$				
	Run 1	Run 2	Run 3	Run 4	Std. deviation ( $\pm$ )
0.00	0.0143	0.0143	0.0143	-	0.0000
0.06	0.0236	0.0238	0.0241	-	0.0003
0.07	0.0238	0.0241	0.0233	-	0.0004
0.18	0.0280	0.0250	0.0269	-	0.0015
0.35	0.0277	0.0271	0.0399	0.0291	0.0060
0.50	0.0348	0.0318	0.0287	0.0307	0.0025
0.60	0.0306	0.0318	0.0340	0.0476	0.0079
0.80	0.0485	0.0507	0.0463	-	0.0022
1.00	0.0697	0.0602	0.0517	0.0552	0.0078
1.50	0.0428	0.0488	0.0488	0.0532	0.0043
2.00	0.0360	0.0536	0.0448	0.0515	0.0079
2.50	0.0421	-	-	-	0.0000
3.00	0.0422	0.0414	0.0454	-	0.0021
4.00	0.0427	0.0475	0.0390	0.0443	0.0035
5.00	0.0474	0.0474	0.0476	-	0.0001



**Figure 3.4**  $\eta_{sp}$  as a function of PEO6\_40 ppm + HTAC in aqueous solutions at 30°C.

*A3.5 Viscosity data for aqueous PEO6\_200 ppm - HTAC solutions at 30°C  
(PEO6 = PEO  $M_w$   $6.06 \times 10^5$  g/mol)*

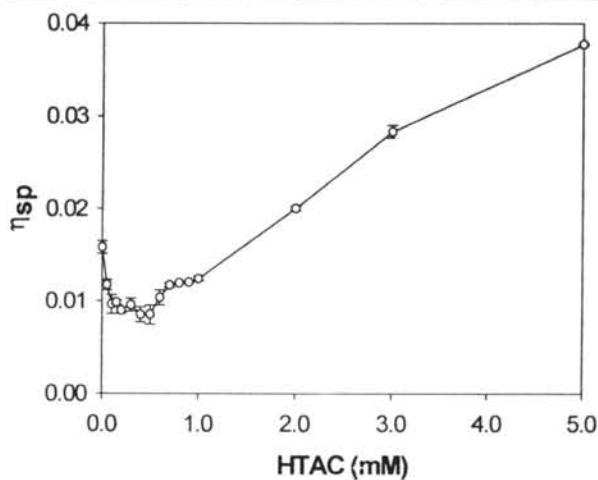
HTAC (mM)	$\eta_{sp}$			
	Run 1	Run 2	Run 3	Std. deviation ( $\pm$ )
0.00	0.0097	0.0072	0.0074	0.0014
0.02	0.0844	0.0877	0.0863	0.0017
0.04	0.0859	0.0846	0.0833	0.0013
0.06	0.0814	0.0830	0.0819	0.0008
0.10	0.0801	0.0795	0.0789	0.0006
0.15	0.0862	0.0817	0.0859	0.0025
0.20	0.0849	0.0868	0.0872	0.0012
0.30	0.0850	0.0843	0.0842	0.0004
0.40	0.0854	0.0845	0.0851	0.0005
0.50	0.0896	0.0896	0.0896	0.0000
1.00	0.0910	-	-	0.0000
1.30	0.0940	-	0.0939	0.0001
2.00	0.1336	0.1331	0.1335	0.0003
3.00	0.1267	0.1298	0.1286	0.0016
5.00	0.1331	0.1295	0.1299	0.0020



**Figure 3.5**  $\eta_{sp}$  as a function of PEO6\_200 ppm + HTAC in aqueous solutions at 30°C.

*A3.6 Viscosity data for aqueous PEO20\_15 ppm - HTAC solutions at 30°C  
(PEO20 = PEO  $M_w$   $17.90 \times 10^5$  g/mol)*

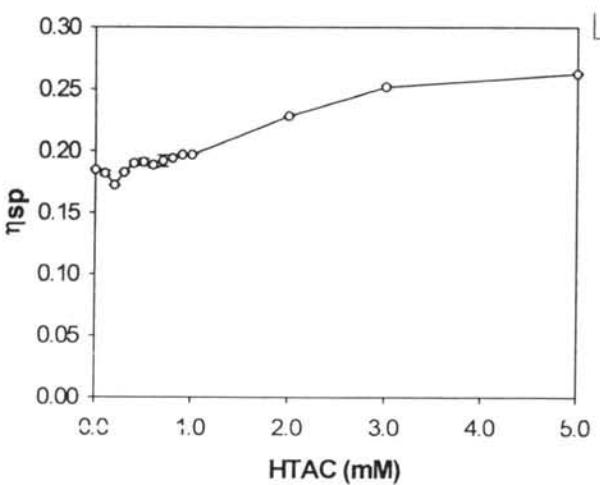
HTAC (mM)	$\eta_{sp}$			
	Run 1	Run 2	Run 3	Std. deviation ( $\pm$ )
0.00	0.0165	0.0165	0.0145	0.0012
0.05	0.0129	0.0110	0.0114	0.0010
0.10	0.0117	0.0087	0.0085	0.0018
0.15	0.0098	0.0103	0.0095	0.0004
0.20	0.0093	0.0094	0.0083	0.0006
0.30	0.0081	0.0104	0.0102	0.0013
0.40	0.0077	0.0093	-	0.0011
0.50	0.0070	0.0105	0.0082	0.0018
0.60	0.0111	0.0113	0.0088	0.0014
0.70	0.0122	0.0113	0.0117	0.0005
0.80	0.0120	0.0119	0.0120	0.0001
0.90	0.0121	0.0120	0.0119	0.0001
1.00	0.0122	0.0129	0.0121	0.0004
2.00	0.0196	0.0205	0.0200	0.0005
3.00	0.0297	0.0278	0.0275	0.0012
5.00	0.0377	0.0379	0.0376	0.0002



**Figure 3.6**  $\eta_{sp}$  as a function of PEO20\_15 ppm + HTAC in aqueous solutions at 30°C.

*A3.7 Viscosity data for aqueous PEO20\_200 ppm - HTAC solutions at 30°C  
(PEO20 = PEO  $M_w$   $17.90 \times 10^5$  g/mol)*

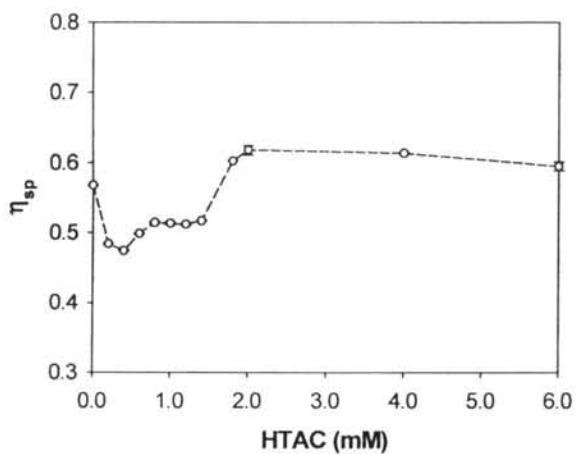
HTAC (mM)	$\eta_{sp}$				
	Run 1	Run 2	Run 3	Run 4	Std. deviation ( $\pm$ )
0.00	0.1831	0.1853	0.1856	-	0.0014
0.10	0.1876	0.1803	0.1800	0.1793	0.0039
0.20	0.1720	0.1727	0.1716	-	0.0006
0.30	0.1827	0.1816	0.1839	0.1819	0.0010
0.40	0.1922	0.1855	0.1912	0.1908	0.0030
0.50	0.1882	0.1894	0.1865	0.1992	0.0057
0.60	0.1869	0.1862	0.1854	0.1958	0.0049
0.70	0.1876	0.1874	0.1865	0.2061	0.0095
0.80	0.1940	0.1941	0.1941	-	0.0001
0.90	0.1978	0.1975	0.1949	-	0.0016
1.00	0.1969	0.1968	-	-	0.0001
2.00	0.2281	0.2279	0.2284	-	0.0003
3.00	0.2548	0.2501	0.2506	-	0.0026
5.00	0.2615	0.2621	0.2641	-	0.0014



**Figure 3.7**  $\eta_{sp}$  as a function of PEO20\_200 ppm + HTAC in aqueous solutions at 30°C.

*A3.8 Viscosity data for aqueous PEO20\_500 ppm - HTAC solutions at 30°C  
(PEO20 = PEO  $M_w$   $17.90 \times 10^5$  g/mol)*

HTAC (mM)	$\eta_{sp}$			
	Run 1	Run 2	Run 3	Std. deviation ( $\pm$ )
0.00	0.5672	0.5666	0.5695	0.0015
0.20	0.4845	0.4836	0.4835	0.0006
0.40	0.4742	0.4727	0.4763	0.0018
0.60	0.4979	0.4973	0.5008	0.0019
0.80	0.5128	0.5131	0.5172	0.0025
1.00	0.5152	0.5145	0.5100	0.0028
1.20	0.5132	0.5128	0.5098	0.0019
1.40	0.5164	0.5178	0.5169	0.0007
1.80	0.6017	0.6033	0.6024	0.0008
2.00	0.6058	0.6189	0.6294	0.0118
4.00	0.6158	0.6146	0.6120	0.0019
6.00	0.5825	0.6010	0.6016	0.0109

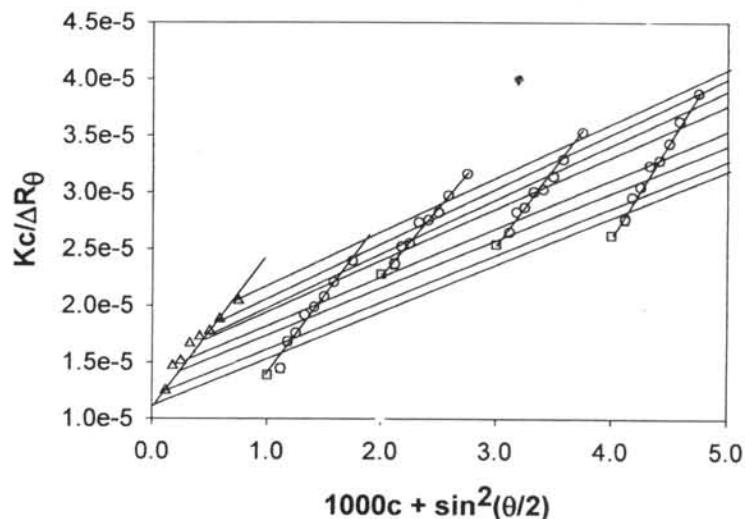


**Figure 3.8**  $\eta_{sp}$  as a function of PEO20\_500 ppm + HTAC in aqueous solutions at 30°C.

**Appendix B Static and Dynamic Light Scattering Data for Aqueous PEO, HTAC, PEO-HTAC and PEO-HTAC-NaSal solutions at 30°C**

**B1 Static light scattering data for aqueous PEO solutions at 30°C**

**B1.1 PEO1 (quoted  $M_w = 1.0 \times 10^5$  g/mol)**



**Figure 1.1** Zimm plot for PEO ( $M_w = 0.91 \times 10^5$  g/mol) in aqueous solution at 30°C.

(i) PEO = 1.0 g/l

Angle	1000c <sub>1</sub> + sin <sup>2</sup> (θ/2)	Kc/ΔR <sub>θ</sub> × 10 <sup>5</sup>		
		Run 1	Run 2	Run 3
40	1.1170	1.39	1.52	1.43
50	1.1786	1.74	1.61	1.70
60	1.2500	1.77	1.72	1.79
70	1.3290	1.94	1.91	1.90
80	1.4132	2.04	1.96	1.96
90	1.5000	2.08	2.07	2.09
100	1.5868	2.24	2.20	2.18
120	1.7500	2.44	2.37	2.38

(ii) PEO = 2.0 g/l

Angle	$1000c_2 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^5$		
		Run 1	Run 2	Run 3
40	2.1170	2.28	2.40	2.43
50	2.1786	2.51	2.51	2.55
60	2.2500	2.55	2.54	2.57
70	2.3290	2.73	2.76	2.72
80	2.4132	2.75	2.78	2.74
90	2.5000	2.84	2.83	2.80
100	2.5868	2.97	2.97	2.98
120	2.7500	3.19	3.16	3.15

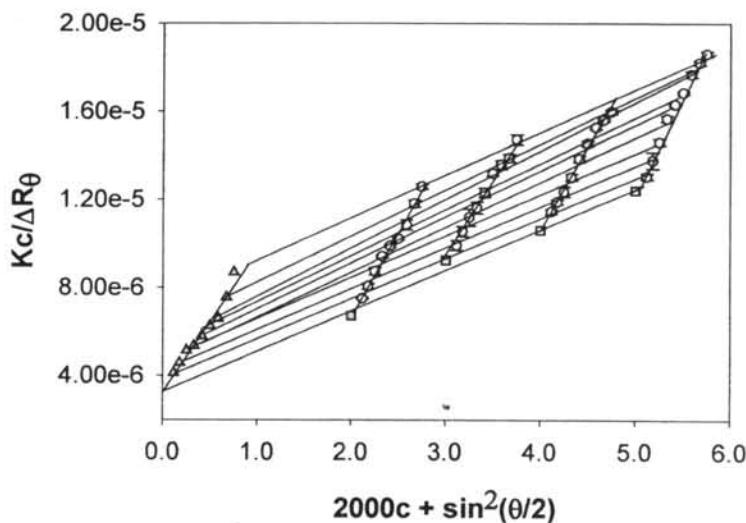
(iii) PEO = 3.0 g/l

Angle	$1000c_3 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^5$		
		Run 1	Run 2	Run 3
40	3.1170	2.69	2.65	2.61
50	3.1786	2.85	2.81	2.83
60	3.2500	2.85	2.87	2.89
70	3.3290	2.94	3.04	3.04
80	3.4132	2.99	3.04	3.05
90	3.5000	3.16	3.14	3.13
100	3.5868	3.33	3.30	3.25
120	3.7500	3.55	3.54	3.50

(iv) PEO = 4.0 g/l

Angle	$1000c_4 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^5$		
		Run 1	Run 2	Run 3
40	4.1170	2.70	2.84	2.75
50	4.1786	2.93	2.96	2.98
60	4.2500	3.03	3.02	3.10
70	4.3290	3.26	3.19	3.27
80	4.4132	3.31	3.22	3.32
90	4.5000	3.46	3.43	3.42
100	4.5868	3.65	3.64	3.60
120	4.7500	3.89	3.89	3.85

B1.2 PEO3 (quoted  $M_w = 3.0 \times 10^5$  g/mol)



**Figure 1.2** Zimm plot for PEO ( $M_w = 3.04 \times 10^5$  g/mol) in aqueous solution at 30°C.

(i) PEO = 1.0 g/l

Angle	2000c <sub>1</sub> + sin <sup>2</sup> (θ/2)	Kc/ΔR <sub>θ</sub> × 10 <sup>5</sup>		
		Run 1	Run 2	Run 3
40	2.1170	0.74	0.76	0.75
50	2.1786	0.79	0.80	0.83
60	2.2500	0.86	0.91	0.86
70	2.3290	0.93	0.94	0.95
80	2.4132	0.98	0.98	1.00
90	2.5000	1.02	1.03	1.01
100	2.5868	1.06	1.06	1.13
110	2.6710	1.21	1.16	1.17
120	2.7500	1.25	1.28	1.24

(ii) PEO = 1.5 g/l

Angle	$2000c_2 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^5$		
		Run 1	Run 2	Run 3
40	3.1170	0.95	1.03	0.99
50	3.1786	1.03	1.03	1.10
60	3.2500	1.15	1.16	1.04
70	3.3290	1.20	1.17	1.11
80	3.4132	1.26	1.24	1.19
90	3.5000	1.30	1.31	1.34
100	3.5868	1.39	1.36	1.32
110	3.6710	1.42	1.36	1.38
120	3.7500	1.51	1.47	1.43

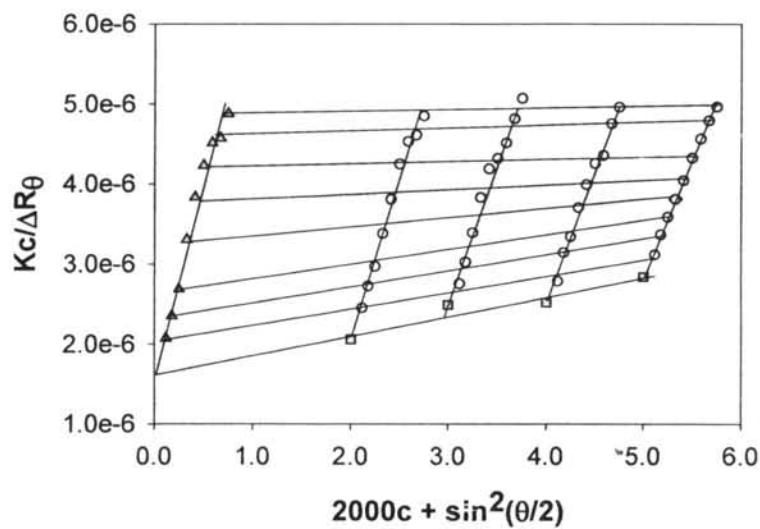
(iii) PEO = 2.0 g/l

Angle	$2000c_3 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^5$		
		Run 1	Run 2	Run 3
40	4.1170	1.12	1.15	1.16
50	4.1786	1.21	1.18	1.17
60	4.2500	1.28	1.21	1.21
70	4.3290	1.33	1.28	1.29
80	4.4132	1.41	1.38	1.36
90	4.5000	1.48	1.44	1.44
100	4.5868	1.53	1.54	1.51
110	4.6710	1.57	1.56	1.55
120	4.7500	1.60	1.58	1.61

(iv) PEO = 2.5 g/l

Angle	$2000c_4 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^5$		
		Run 1	Run 2	Run 3
40	5.1170	1.28	1.30	1.33
50	5.1786	1.36	1.32	1.45
60	5.2500	1.49	1.45	1.44
70	5.3290	1.54	1.58	1.58
80	5.4132	1.63	1.62	1.64
90	5.5000	1.69	1.67	1.69
100	5.5868	1.74	1.79	1.77
110	5.6710	1.81	1.84	1.81
120	5.7500	1.86	1.88	1.84

B1.3 PEO6 (quoted  $M_w = 6.0 \times 10^5$  g/mol)



**Figure 1.3** Zimm plot for PEO ( $M_w = 6.06 \times 10^5$  g/mol) in aqueous solution at  $30^\circ\text{C}$ .

(i) PEO = 0.5 g/l

Angle	$2000c_1 + \sin^2(\theta/2)$	$K_c/\Delta R_\theta \times 10^6$
40	2.1170	2.45
50	2.1786	2.73
60	2.2500	2.97
70	2.3290	3.38
80	2.4132	3.81
90	2.5000	4.25
100	2.5868	4.53
110	2.6710	4.61
120	2.7500	4.85

(ii) PEO = 1.0 g/l

Angle	$2000c_2 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^6$
40	3.1170	2.75
50	3.1786	3.02
60	3.2500	3.39
70	3.3290	3.83
80	3.4132	4.19
90	3.5000	4.32
100	3.5868	4.52
110	3.6710	4.82
120	3.7500	5.07

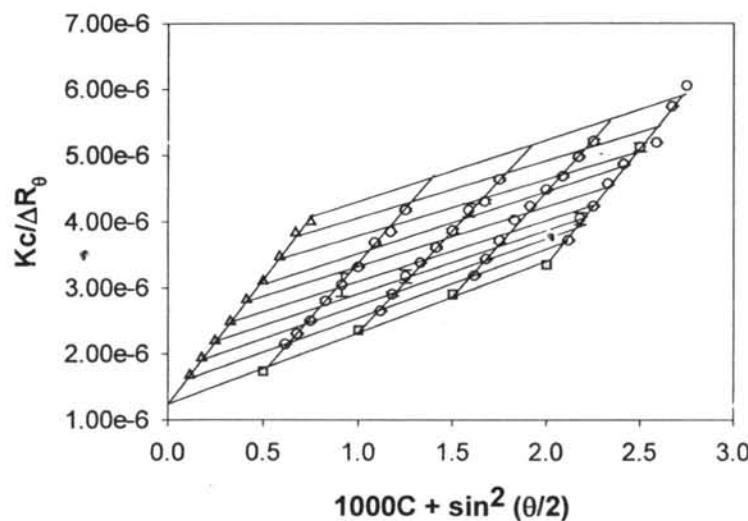
(iii) PEO = 1.5 g/l

Angle	$2000c_3 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^6$
40	4.1170	2.78
50	4.1786	3.14
60	4.2500	3.34
70	4.3290	3.70
80	4.4132	3.99
90	4.5000	4.26
100	4.5868	4.35
110	4.6710	4.75
120	4.7500	4.96

(iv) PEO = 2.0 g/l

Angle	$2000c_4 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^6$
40	5.1170	3.11
50	5.1786	3.36
60	5.2500	3.58
70	5.3290	3.80
80	5.4132	4.04
90	5.5000	4.32
100	5.5868	4.56
110	5.6710	4.79
120	5.7500	4.96

B1.4 PEO9 (quoted  $M_w = 9.0 \times 10^5$  g/mol)



**Figure 1.4** Zimm plot for PEO ( $M_w = 8.03 \times 10^5$  g/mol) in aqueous solution at 30°C.

(i) PEO = 0.5 g/l

Angle	5000c <sub>1</sub> + sin <sup>2</sup> (θ/2)	Kc/ΔR <sub>θ</sub> × 10 <sup>6</sup>		
		Run 1	Run 2	Run 3
40	0.6170	2.15	2.14	2.16
50	0.6786	2.32	2.30	-
60	0.7500	2.52	2.50	2.48
70	0.8290	2.80	2.75	2.85
80	0.9132	3.35	3.05	2.75
90	1.0000	3.31	3.33	-
100	1.0868	3.70	3.66	-
110	1.1710	3.86	3.84	-
120	1.2500	4.20	4.16	-

(ii) PEO = 1.0 g/l

Angle	$5000c_2 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^6$		
		Run 1	Run 2	Run 3
40	1.1170	2.65	2.67	2.63
50	1.1786	2.90	2.95	2.85
60	1.2500	3.07	3.27	-
70	1.3290	3.37	3.39	-
80	1.4132	3.59	3.63	-
90	1.5000	3.89	3.83	-
100	1.5868	4.07	4.27	-
110	1.6710	4.33	4.27	-
120	1.7500	4.66	4.62	-

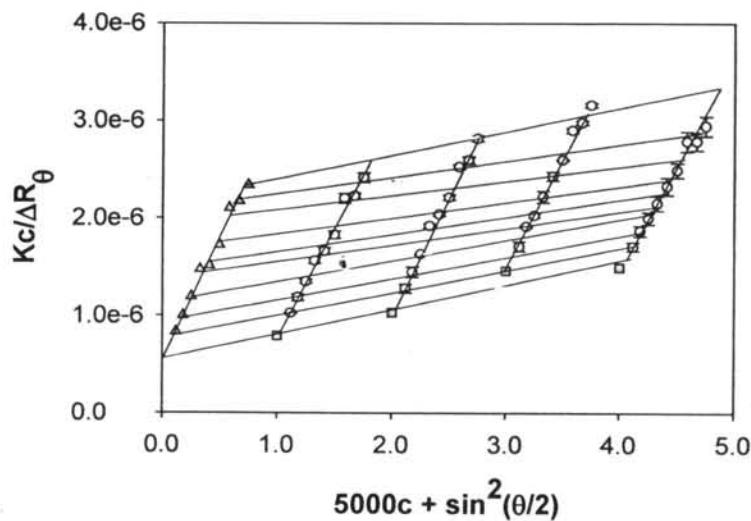
(iii) PEO = 1.5 g/l

Angle	$5000c_3 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^6$		
		Run 1	Run 2	Run 3
40	1.6170	3.20	3.16	3.18
50	1.6786	3.45	3.41	3.43
60	1.7500	3.76	3.66	3.71
70	1.8290	4.04	4.00	4.02
80	1.9132	4.24	4.23	4.25
90	2.0000	4.48	4.50	-
100	2.0868	4.67	4.71	-
110	2.1710	5.00	4.96	-
120	2.2500	5.25	5.19	-

(iv) PEO = 2.0 g/l

Angle	5000c <sub>3</sub> + sin <sup>2</sup> (θ/2)	Kc/ΔR <sub>θ</sub> × 10 <sup>6</sup>	
		Run 1	Run 2
40	2.1170	3.71	3.73
50	2.1786	3.96	4.14
60	2.2500	4.24	4.22
70	2.3290	4.59	4.55
80	2.4132	4.85	4.89
90	2.5000	5.19	5.06
100	2.5868	5.20	5.20
110	2.6710	5.73	5.75
120	2.7500	6.06	6.06

B1.5 PEO20 (quoted  $M_w = 40.0 \times 10^5$  g/mol)



**Figure 1.5** Zimm plot for PEO ( $M_w = 17.9 \times 10^5$  g/mol) in aqueous solution at 30°C.

(i) PEO = 0.2 g/l

Angle	5000c <sub>1</sub> + sin <sup>2</sup> (θ/2)	Kc/ΔR <sub>θ</sub> × 10 <sup>6</sup>		
		Run 1	Run 2	Run 3
40	1.1170	1.02	1.02	1.03
50	1.1786	1.19	1.24	1.12
60	1.2500	1.38	1.32	1.34
70	1.3290	1.62	1.52	1.54
80	1.4132	1.69	1.59	1.70
90	1.5000	1.83	1.89	1.76
100	1.5868	2.29	2.20	2.12
110	1.6710	2.27	2.18	2.23
120	1.7500	2.45	2.48	2.32

(ii) PEO = 0.4 g/l

Angle	$5000c_2 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^6$		
		Run 1	Run 2	Run 3
40	2.1170	1.19	1.34	1.31
50	2.1786	1.34	1.51	1.49
60	2.2500	1.62	1.64	1.63
70	2.3290	1.94	1.94	1.88
80	2.4132	2.03	2.07	2.02
90	2.5000	2.19	2.18	2.27
100	2.5868	2.52	2.49	2.57
110	2.6710	2.59	2.54	2.66
120	2.7500	2.83	2.76	2.86

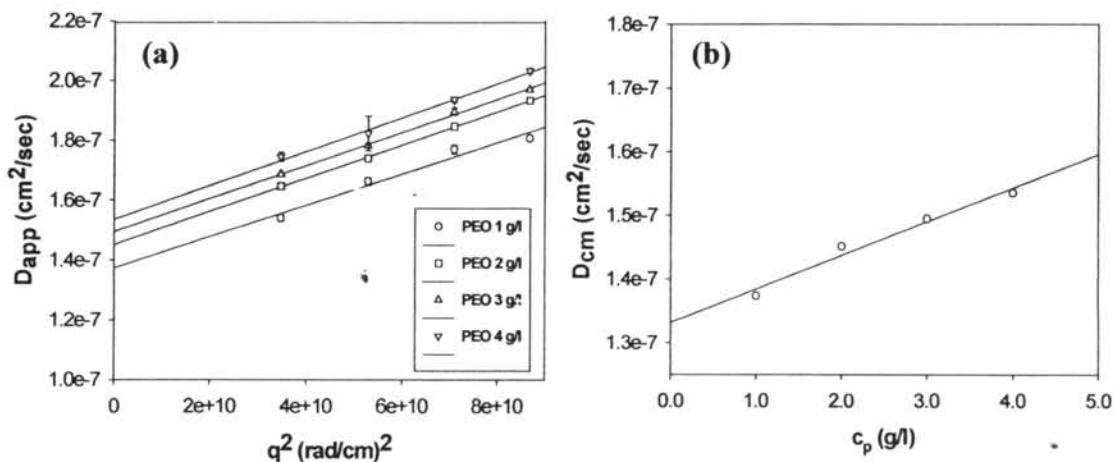
(iii) PEO = 0.6 g/l

Angle	$5000c_3 + \sin^2(\theta/2)$	$Kc/\Delta R_\theta \times 10^6$		
		Run 1	Run 2	Run 3
40	3.1170	1.77	1.61	1.74
50	3.1786	1.89	1.93	1.92
60	3.2500	2.06	1.99	2.03
70	3.3290	2.30	2.10	2.26
80	3.4132	2.49	2.34	2.46
90	3.5000	2.59	2.61	2.59
100	3.5868	2.94	2.85	2.91
110	3.6710	3.00	3.00	2.94
120	3.7500	3.18	3.18	3.12

(iv) PEO = 0.8 g/l

Angle	5000c <sub>4</sub> + sin <sup>2</sup> (θ/2)	Kc/ΔR <sub>θ</sub> × 10 <sup>6</sup>			
		Run 1	Run 2	Run 3	Run 4
40	4.1170	1.73	1.70	1.64	1.60
50	4.1786	1.97	1.84	1.75	1.76
60	4.2500	2.10	2.04	1.86	1.84
70	4.3290	2.28	2.19	1.96	1.99
80	4.4132	2.49	2.36	2.10	2.14
90	4.5000	2.63	2.53	2.42	2.24
100	4.5868	2.95	2.82	2.63	2.49
110	4.6710	2.95	2.80	2.66	2.52
120	4.7500	3.06	2.97	2.84	2.63

### B2 Dynamic light scattering data for aqueous PEO solutions at 30°C



**Figure 2.1** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different PEO concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of PEO concentration for PEO  $M_w$   $0.91 \times 10^5$  g/mol at 30°C.

#### B2.1 PEO1 (quoted $M_w = 1.0 \times 10^5$ g/mol)

(i) PEO = 1.0 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ ( $\text{cm}^2/\text{s}$ )			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
			1.80	1.82	1.80	0.550	0.491	0.476
130	2.9459	8.6784	1.80	1.75	1.76	0.513	0.514	0.513
110	2.6628	7.0903	1.80	1.75	1.76	0.486	0.476	0.503
90	2.2987	5.2838	1.65	1.69	1.65	0.533	0.521	0.503
70	1.8646	3.4769	1.54	1.56	1.52			

(ii) PEO = 2.0 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
			1.94	1.94	1.92	0.496	0.461	0.433
130	2.9459	8.6784	1.85	1.83	1.86	0.457	0.424	0.467
110	2.6628	7.0903	1.76	1.73	1.73	0.476	0.488	0.478
90	2.2987	5.2838	1.65	1.63	1.66	0.508	0.497	0.515
70	1.8646	3.4769						

(iii) PEO = 3.0 g/l

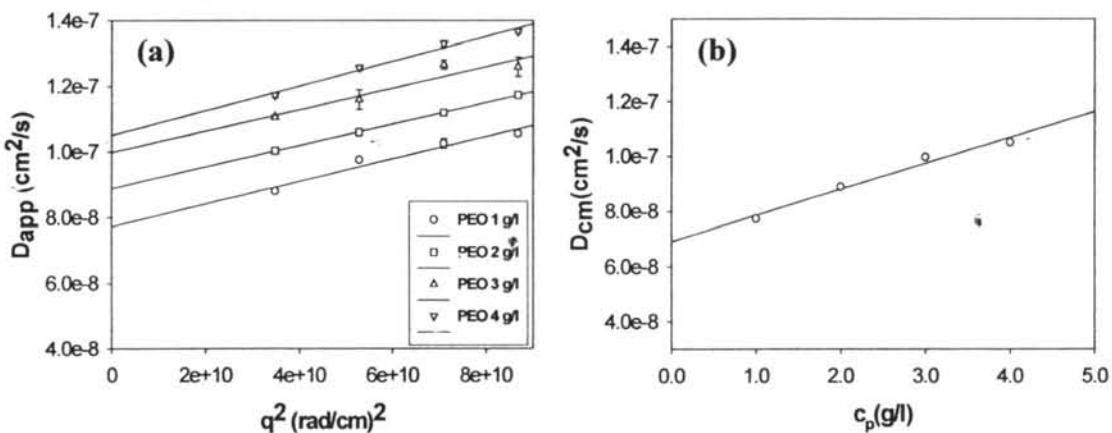
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
			1.98	1.96	1.97	0.620	0.593	0.585
130	2.9459	8.6784	1.92	1.89	1.88	0.608	0.607	0.594
110	2.6628	7.0903	1.77	1.79	1.79	0.641	0.705	0.632
90	2.2987	5.2838	1.69	1.68	1.69	0.691	0.661	0.662
70	1.8646	3.4769						

(iv) PEO = 4.0 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
			2.05	2.02	2.03	0.618	0.627	0.628
130	2.9459	8.6784	1.92	1.95	1.94	0.639	0.654	0.619
110	2.6628	7.0903	1.86	1.71	1.90	0.667	0.665	0.654
90	2.2987	5.2838	1.73	-	1.76	0.698	0.704	0.698
70	1.8646	3.4769						

PEO (g/l)	$D_{cm} \times 10^7$ (cm <sup>2</sup> /s)	$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
1.0	1.37			
2.0	1.45			
3.0	1.49	13.3	16.69	0.50
4.0	1.54			

B2.2 PEO3 (quoted  $M_w = 3.0 \times 10^5$  g/mol)



**Figure 2.2** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different PEO concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of PEO concentration for PEO  $M_w 3.04 \times 10^5$  g/mol at  $30^\circ\text{C}$ .

(i) PEO = 1.0 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ ( $\text{cm}^2/\text{s}$ )			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
			-	-	-	0.404	0.410	0.416
130	2.9459	8.6784	-	1.06	1.05	0.404	0.410	0.416
110	2.6628	7.0903	1.01	-	1.04	0.415	0.428	0.422
90	2.2987	5.2838	0.97	0.98	-	0.454	0.450	0.460
70	1.8646	3.4769	0.87	0.89	0.88	0.477	0.486	0.488

(ii) PEO = 2.0 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ ( $\text{cm}^2/\text{s}$ )			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
			1.18	1.18	1.16	0.406	0.401	0.400
130	2.9459	8.6784	1.18	1.18	1.16	0.406	0.401	0.400
110	2.6628	7.0903	1.12	1.13	1.11	0.410	0.410	0.414
90	2.2987	5.2838	1.08	1.06	1.04	0.418	0.422	0.423
70	1.8646	3.4769	1.00	1.01	1.00	0.441	0.451	0.437

(iii) PEO = 3.0 g/l

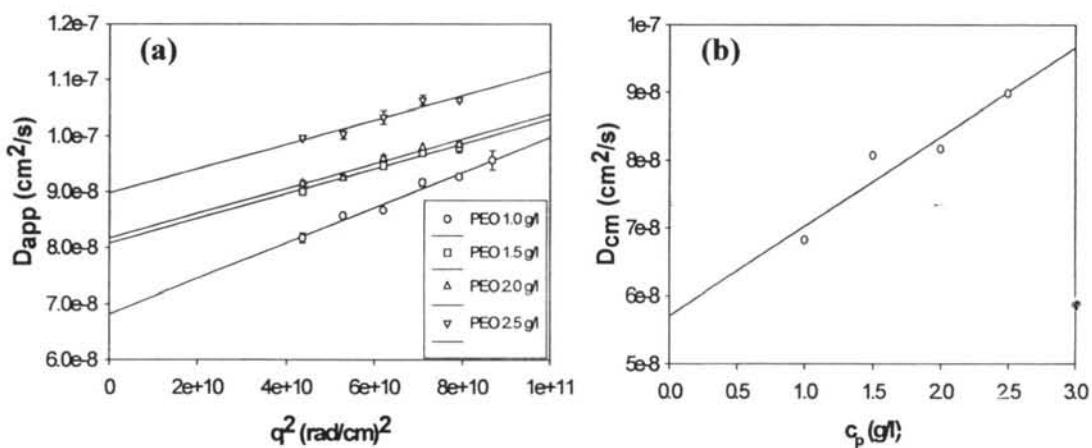
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
130	2.9459	8.6784	1.23	1.23	1.32	0.430	0.430	0.435
110	2.6628	7.0903	1.29	1.24	1.27	0.442	0.443	0.446
90	2.2987	5.2838	1.10	1.18	1.20	0.450	0.457	0.450
70	1.8646	3.4769	1.10	1.10	1.127	0.527	0.540	0.472

(iv) PEO = 4.0 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
130	2.9459	8.6784	1.38	1.36	1.36	0.447	0.446	0.444
110	2.6628	7.0903	1.32	1.35	1.32	0.498	0.449	0.444
90	2.2987	5.2838	1.27	1.26	1.24	0.461	0.458	0.442
70	1.8646	3.4769	1.18	1.18	1.16	0.469	0.461	0.479

PEO (g/l)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
1.0	7.73			
2.0	8.88			
3.0	9.97	7.00	31.71	0.49
4.0	10.51			

B2.3 PEO6 (quoted  $M_w = 6.0 \times 10^5$  g/mol)



**Figure 2.3** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different PEO concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of PEO concentration for PEO  $M_w 6.06 \times 10^5$  g/mol at  $30^\circ\text{C}$ .

(i) PEO = 1.0 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) $^2$	$D_{app} \times 10^8$ ( $\text{cm}^2/\text{s}$ )			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
130	2.9459	8.6784	9.90	9.50	9.30	0.394	0.394	0.395
120	2.8151	7.9245	9.30	9.20	9.30	0.392	0.381	0.389
110	2.6628	7.0903	9.30	9.10	9.10	0.382	0.383	0.387
100	2.4902	6.2011	8.70	8.70	8.60	0.381	0.380	0.380
90	2.2987	5.2838	8.50	8.60	8.60	0.395	0.390	0.387
80	2.0896	4.3664	8.20	8.00	8.30	0.394	0.399	0.382

(ii) PEO = 1.5 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) $^2$	$D_{app} \times 10^8$ ( $\text{cm}^2/\text{s}$ )			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
120	2.8151	7.9245	9.60	9.90	9.90	0.421	0.403	0.402
110	2.6628	7.0903	9.70	9.70	9.70	0.400	0.395	0.398
100	2.4902	6.2011	9.40	9.50	9.50	0.397	0.397	0.392
80	2.0896	4.3664	-	-	9.00	0.416	0.381	0.390

(iii) PEO = 2.0 g/l

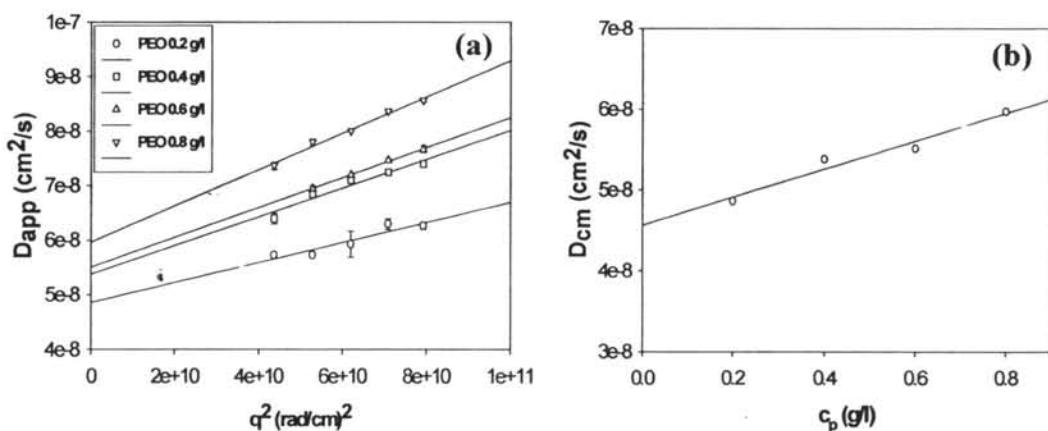
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
120	2.8151	7.9245	-	9.80	9.90	0.428	0.422	0.421
110	2.6628	7.0903	9.80	9.80	9.80	0.422	0.418	0.422
100	2.4902	6.2011	9.60	9.70	9.50	0.422	0.408	0.429
90	2.2987	5.2838	-	9.30	9.20	0.435	0.423	0.424
80	2.0896	4.3664	-	9.20	9.10	0.434	0.414	0.418

(iv) PEO = 2.5 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
120	2.8151	7.9245	1.06	1.07	1.06	0.413	0.415	0.417
110	2.6628	7.0903	1.08	1.06	1.05	0.403	0.419	0.413
100	2.4902	6.2011	1.04	1.01	1.05	0.424	0.427	0.420
90	2.2987	5.2838	1.02	0.99	1.00	0.418	0.420	0.422
80	2.0896	4.3664	0.99	1.00	1.00	0.418	0.417	0.417

PEO (g/l)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
1.0	6.82			
1.5	8.07			
2.0	8.17	5.70	38.87	0.39
2.5	8.98			

*B2.4 PEO9 (quoted  $M_w = 9.0 \times 10^5$  g/mol)*



**Figure 2.4** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different PEO concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of PEO concentration for PEO  $M_w 8.03 \times 10^5$  g/mol at  $30^\circ\text{C}$ .

(i) PEO = 0.2 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
120	2.8151	7.9245	6.20	6.20	6.40	0.448	0.445	0.439
110	2.6628	7.0903	6.20	6.50	6.200	0.426	0.40	0.434
100	2.4902	6.2011	6.40	5.80	5.60	0.401	0.455	0.424
90	2.2987	5.2838	5.70	5.80	5.70	0.424	0.429	0.438
80	2.0896	4.3664	5.40	5.20	5.20	0.427	0.437	0.449

(ii) PEO = 0.4 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
120	2.8151	7.9245	7.40	7.50	7.30	0.419	0.416	0.417
110	2.6628	7.0903	7.20	7.30	-	0.422	0.414	0.397
100	2.4902	6.2011	7.10	7.10	7.10	0.407	0.409	0.419
90	2.2987	5.2838	-	6.90	6.80	0.391	0.399	0.405
80	2.0896	4.3664	6.30	6.50	-	0.400	0.398	0.380

(iii) PEO = 0.6 g/l

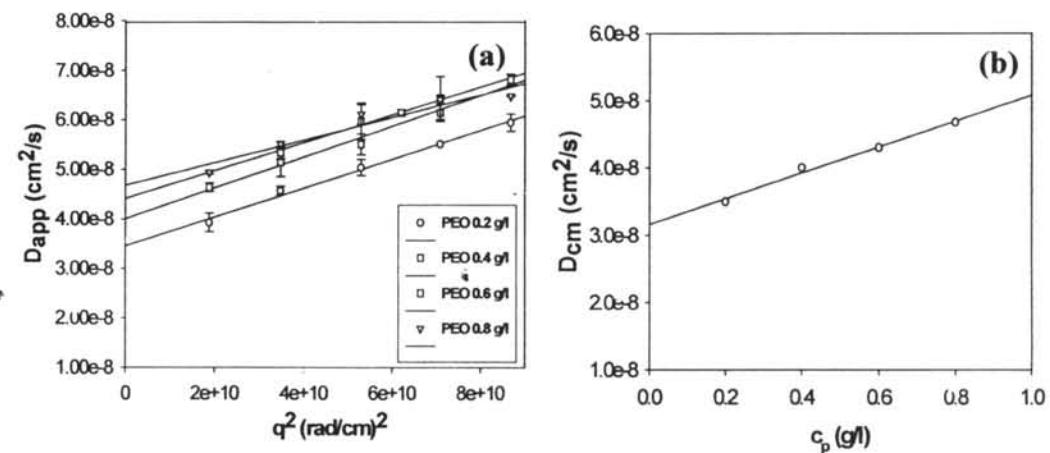
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
120	2.8151	7.9245	7.60	7.80	7.60	0.425	0.410	0.419
110	2.6628	7.0903	7.50	7.40	7.50	0.408	0.420	0.420
100	2.4902	6.2011	7.20	-	7.20	0.412	0.421	0.416
90	2.2987	5.2838	6.90	-	7.00	0.412	0.424	0.414
80	2.0896	4.3664	-	-	-	0.430	0.422	0.427

(iv) PEO = 0.8 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
120	2.8151	7.9245	8.60	8.50	8.60	0.407	0.413	0.407
110	2.6628	7.0903	8.40	8.40	8.30	0.390	0.412	0.406
100	2.4902	6.2011	8.00	8.00	8.00	0.396	0.410	0.401
90	2.2987	5.2838	7.80	7.70	7.90	0.393	0.402	0.397
80	2.0896	4.3664	7.50	7.30	7.30	0.401	0.407	0.412

PEO (g/l)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	$D_o \times 10^{12}$ (m <sup>2</sup> /s)	R <sub>h</sub> (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
0.2	4.86			
0.4	5.38			
0.6	5.51	4.60	48.56	0.37
0.8	5.97			

B2.5 PEO20 (quoted  $M_w = 40.0 \times 10^5$  g/mol)



**Figure 2.5** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different PEO concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of PEO concentration for PEO  $M_w 17.9 \times 10^5$  g/mol at  $30^\circ\text{C}$ .

(i) PEO = 0.2 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) $^2$	$D_{app} \times 10^8$ ( $\text{cm}^2/\text{s}$ )				$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 4	Run 1	Run 2	Run 3
130	2.8946	8.6784	5.6	6.20	6.00	-	0.987	0.912	0.922
110	2.6628	7.0903	-	5.50	5.50	-	0.827	0.813	0.834
90	2.2987	5.2838	-	4.70	5.20	5.20	0.839	0.801	0.796
70	1.8647	3.4769	4.40	4.60	4.70	-	0.654	0.665	0.671
50	1.3739	1.8877	3.90	4.40	3.50	3.90	0.667	0.660	0.604

(ii) PEO = 0.4 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) $^2$	$D_{app} \times 10^8$ ( $\text{cm}^2/\text{s}$ )			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
130	2.8946	8.6784	6.60	6.90	6.90	0.865	0.863	0.870
110	2.6628	7.0903	5.80	6.40	6.20	0.846	0.840	0.836
90	2.2987	5.2838	5.20	5.90	5.40	0.675	0.671	0.660
70	1.8647	3.4769	4.90	5.70	4.80	0.567	0.507	0.501
50	1.3739	1.8877	4.60	4.50	4.80	0.646	0.660	0.634

(iii) PEO = 0.6 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
130	2.8946	8.6784	6.60	6.80	7.00	0.691	0.673	0.697
110	2.6628	7.0903	7.20	6.40	5.70	0.691	0.674	0.659
90	2.2987	5.2838	6.00	6.20	6.20	0.613	0.620	0.615
70	1.8647	3.4769	6.70	5.60	5.60	0.675	0.669	0.680
50	1.3739	1.8877	5.40	5.50	5.10	0.625	0.626	0.628

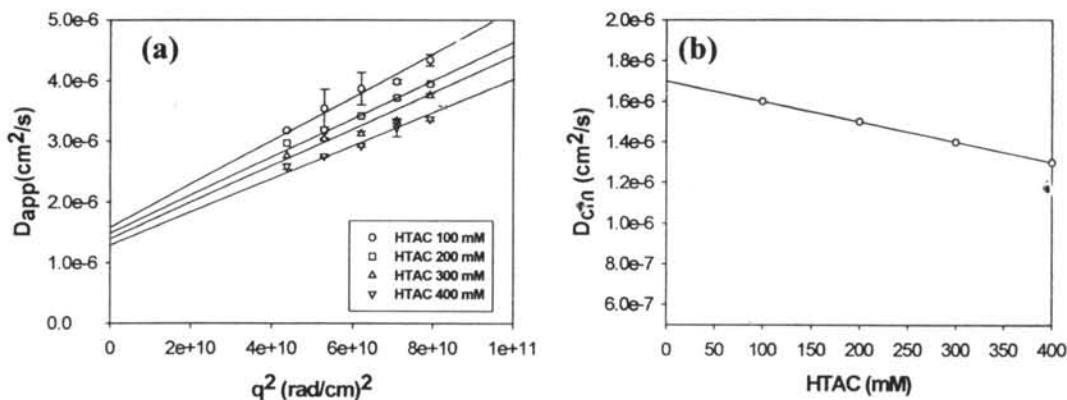
(iv) PEO = 0.8 g/l

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8$ (cm <sup>2</sup> /s)			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
130	2.8946	8.6784	6.47	6.49	6.44	0.781	0.780	0.773
110	2.6628	7.0903	6.40	6.20	6.40	0.770	0.762	0.713
90	2.2987	5.2838	5.70	6.30	6.30	0.703	0.740	0.739
70	1.8647	3.4769	5.50	5.60	5.40	0.756	0.734	0.735
50	1.3739	1.8877	4.90	5.00	4.90	0.722	0.740	0.738

$c_p$ (g/l)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\Gamma^2}$
0.2	3.50			
0.4	4.00			
0.6	4.30	3.20	70.24	0.32
0.8	4.68			

### B3 Dynamic light scattering data for aqueous HTAC solutions at 30°C

#### B3.1 HTAC in aqueous solution



**Figure 3.1** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of HTAC at 30°C.

(i)  $c_{\text{HTAC}} = 100 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^6 (\text{cm}^2/\text{s})$						$\frac{\mu_2}{\Gamma^2}$		
			1	2	3	4	5	6	1	2	3
80	2.0896	4.3664	3.86	3.23	4.41	3.16	3.20	2.84	0.188	0.154	--
90	2.2987	5.2838	4.51	4.33	3.99	3.54	3.62	3.96	0.155	--	--
100	2.4902	6.2011	4.12	4.02	-	3.90	3.93	4.18	0.125	0.081	0.070
110	2.6628	7.0903	-	-	-	4.34	4.51	-	0.170	0.195	0.227

(ii)  $c_{\text{HTAC}} = 200 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^6 (\text{cm}^2/\text{s})$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.97	2.97	2.97	0.226	--	--
90	2.2987	5.2838	3.19	3.19	3.18	0.243	--	--
100	2.4902	6.2011	3.43	3.42	3.42	0.254	0.277	0.289
110	2.6628	7.0903	3.67	3.77	3.73	0.233	0.269	--
120	2.8151	7.9245	3.92	3.98	3.95	0.234	--	--

(iii)  $c_{HTAC} = 300 \text{ mM}$ 

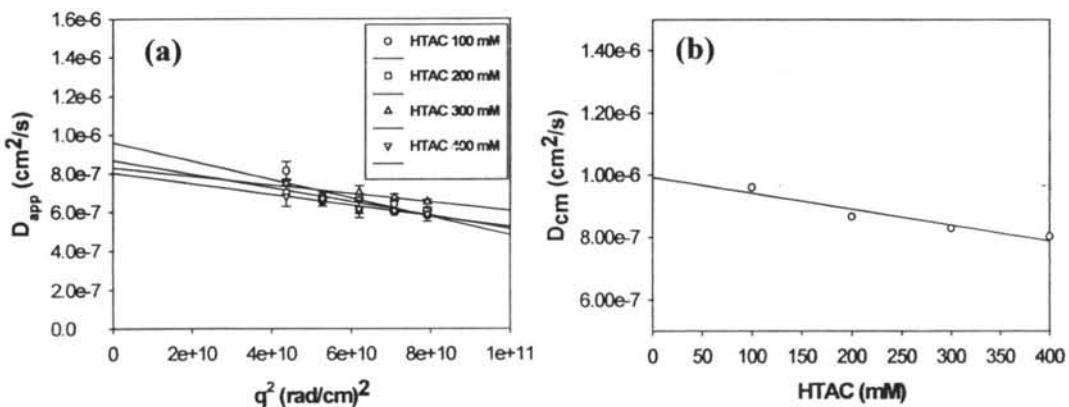
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^6 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.76	--	--	0.129	0.158	--
90	2.2987	5.2838	3.04	3.07	3.03	0.203	0.162	0.186
100	2.4902	6.2011	3.08	3.10	3.21	0.288	0.283	0.233
110	2.6628	7.0903	3.39	3.32	3.30	0.182	0.232	0.230
120	2.8151	7.9245	3.81	3.78	3.69	0.022	0.031	0.155

(iv)  $c_{HTAC} = 400 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^6 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.617	2.640	2.495	0.238	0.234	0.245
90	2.2987	5.2838	2.733	2.785	2.755	0.215	0.205	0.242
100	2.4902	6.2011	2.912	2.902	2.980	0.241	0.210	0.206
110	2.6628	7.0903	3.507	3.005	3.166	0.088	0.212	0.088
120	2.8151	7.9245	3.400	3.403	3.305	--	--	--

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	HTAC 1.3 mM		
		$D_o \times 10^{12}$ (m <sup>2</sup> /s)	R <sub>h</sub> (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
100	1.60			
200	1.50	170.00	1.31	0.16
300	1.40			
400	1.30			

*B3.2 HTAC+ [NaSal]/[HTAC] = 1 in aqueous solution*



**Figure 3.2** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of HTAC + [NaSal]/[HTAC] = 1 at 30°C.

(i)  $c_{HTAC} = 100 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	8.96	8.16	7.31	0.426	0.516	0.728
90	2.2987	5.2838	6.11	6.99	6.55	1.000	0.800	0.655
100	2.4902	6.2011	5.90	6.38	5.96	1.000	0.935	1.000
110	2.6628	7.0903	7.09	6.03	6.14	0.809	1.000	1.000
120	2.8151	7.9245	6.15	6.08	6.06	1.000	1.000	1.000

(ii)  $c_{HTAC} = 200 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	5.55	6.79	8.98	0.850	0.413	--
90	2.2987	5.2838	6.93	6.59	7.21	0.777	0.890	0.693
100	2.4902	6.2011	7.15	6.60	6.53	0.746	0.861	0.894
110	2.6628	7.0903	5.89	6.04	6.05	1.000	0.984	1.000
120	2.8151	7.9245	5.77	5.93	5.80	1.000	1.000	1.000

(iii)  $c_{HTAC} = 300 \text{ mM}$ 

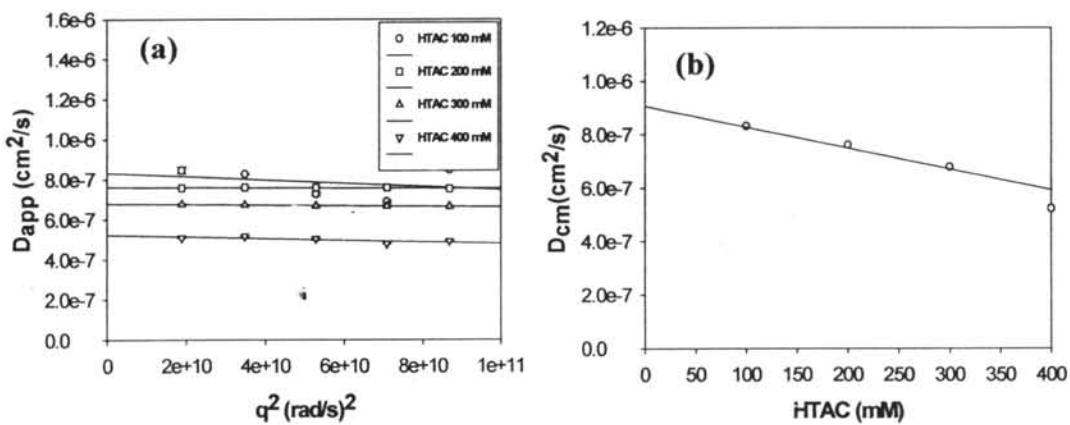
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	7.66	7.22	7.61	-	-	-
90	2.2987	5.2838	6.56	6.49	7.39	0.735	0.781	0.538
100	2.4902	6.2011	6.78	6.71	7.68	1.000	1.000	1.000
110	2.6628	7.0903	7.18	6.80	7.14	0.884	0.987	0.896
120	2.8151	7.9245	6.37	6.78	6.45	1.000	1.000	1.000

(iv)  $c_{HTAC} = 400 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	6.81	--	--	--	--	--
90	2.2987	5.2838	6.67	6.69	--	0.617	0.649	0.566
100	2.4902	6.2011	6.60	5.71	--	0.666	0.853	0.708
110	2.6628	7.0903	6.10	6.01	6.04	1.000	0.773	0.762
120	2.8151	7.9245	5.86	5.27	6.51	0.813	0.999	0.658

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	HTAC 0.7 mM		
		$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
100	9.61			
200	8.67			
300	8.29	99.8	2.23	0.17
400	8.03			

B3.3 HTAC+ [NaSal]/[HTAC] = 5 in aqueous solution



**Figure 3.3** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of HTAC + [NaSal]/[HTAC] = 5 at 30°C.

(i)  $c_{HTAC} = 100 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	8.62	8.15	8.63	0.032	0.111	0.064
70	1.8646	3.4769	8.28	8.22	8.34	0.084	0.087	0.037
90	2.2987	5.2838	7.10	7.39	7.34	0.183	0.182	0.180
110	2.6628	7.0903	6.86	6.77	7.03	0.192	0.169	--
130	2.9459	8.6784	8.53	8.44	8.47	0.175	--	--

(ii)  $c_{HTAC} = 200 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	7.57	7.57	7.59	0.180	0.201	0.186
70	1.8646	3.4769	7.59	7.61	7.64	0.205	0.198	0.185
90	2.2987	5.2838	7.60	7.61	7.58	0.183	0.168	0.190
110	2.6628	7.0903	7.59	7.59	7.61	0.162	0.177	0.170
130	2.9459	8.6784	7.53	7.57	7.51	0.172	0.128	0.173

(iii)  $c_{HTAC} = 300 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	6.74	6.75	6.80	0.108	0.103	0.100
70	1.8646	3.4769	6.75	6.68	6.76	0.112	0.112	0.090
90	2.2987	5.2838	6.72	6.69	6.68	0.115	0.075	0.103
110	2.6628	7.0903	6.70	6.65	6.65	0.117	0.142	0.114
130	2.9459	8.6784	6.66	6.63	6.64	0.097	0.099	0.110

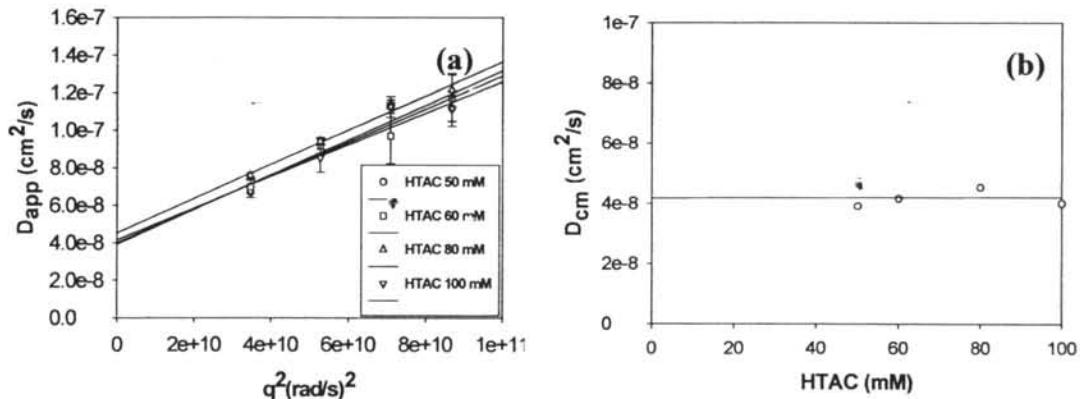
(iv)  $c_{HTAC} = 400 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	5.11	5.08	5.07	0.080	0.103	0.102
70	1.8646	3.4769	5.16	5.20	5.15	0.073	0.053	0.103
90	2.2987	5.2838	4.95	5.17	4.98	0.063	0.060	0.065
110	2.6628	7.0903	4.81	4.78	4.75	0.034	0.019	0.016
130	2.9459	8.6784	4.85	5.00	4.89	0.085	0.032	0.081

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	HTAC 0.6 mM		
		$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
100	8.32			
200	7.61			
300	6.79	90.7	2.45	0.17
400	5.23			

#### B4 Dynamic light scattering data for aqueous PEO - HTAC solutions at 30°C

##### B4.1 PEO6\_40 + HTAC in aqueous solution



**Figure 4.1** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of PEO6\_40 + HTAC at 30°C.

(i)  $c_{HTAC} = 50 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 (\text{cm}^2/\text{s})$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
70	1.8646	3.4769	0.65	0.63	0.72	0.812	0.863	0.823
90	2.2987	5.2838	0.88	0.92	0.97	0.840	0.888	0.892
110	2.6628	7.0903	1.16	1.09	--	0.854	0.876	0.881
130	2.9459	8.6784	1.21	1.02e	--	0.842	0.832	0.868

(ii)  $c_{HTAC} = 60 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 (\text{cm}^2/\text{s})$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
70	1.8646	3.4769	0.77	0.63	0.72	0.821	0.811	0.886
90	2.2987	5.2838	0.98	0.92	0.97	0.889	0.850	0.837
110	2.6628	7.0903	0.70	1.09	--	0.845	0.859	--
130	2.9459	8.6784	1.39	1.02	--	0.871	0.826	0.840

(iii)  $c_{HTAC} = 80 \text{ mM}$ 

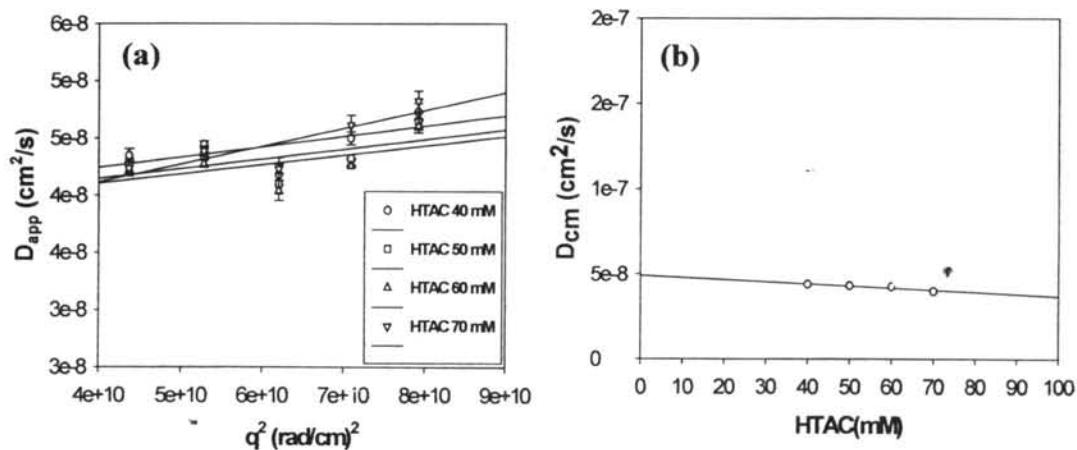
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
70	1.8646	3.4769	0.76	0.72	0.80	0.861	0.829	--
90	2.2987	5.2838	0.91	0.98	0.93	0.857	--	--
110	2.6628	7.0903	1.13	1.14	1.15	0.822	0.823	0.822
130	2.9459	8.6784	1.33	1.04	1.27	0.839	--	--

(iv)  $c_{HTAC} = 100 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\Gamma^2}$
			Run 1	Run 2	Run 3	
70	1.8646	3.4769	0.67	--	--	0.834
90	2.2987	5.2838	0.83	0.71	0.80	0.872
110	2.6628	7.0903	1.22	1.12	1.03	0.815
130	2.9459	8.6784	1.18	1.18	0.98	0.835

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	PEO60_40+HTAC 5 mM		
		$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\Gamma^2}$
50	3.90			
60	4.15			
80	4.53	3.98	55.9	0.83
100	3.99			

B4.2 PEO6\_40 + [NaSal]/[HTAC] = 1 in aqueous solution



**Figure 4.2** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of PEO6\_40 + [NaSal]/[HTAC] = 1 at 30°C.

(i)  $c_{HTAC} = 40 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\Gamma^2}$			
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3	Run 4
80	2.0896	4.3664	4.96	4.76	4.82	0.149	--	--	--
90	2.2987	5.2838	4.99	4.89	4.95	0.153	0.139	0.180	0.120
100	2.4902	6.2011	4.85	4.55	4.65	0.101	--	--	--
110	2.6628	7.0903	5.00	4.90	5.10	0.319	0.053	0.310	0.102
120	2.8151	7.9245	5.11	5.21	5.37	0.226	--	--	--

(ii)  $c_{HTAC} = 50 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$			
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3	Run 4
80	2.0896	4.3664	4.88	4.68	4.70	0.149	--	--	--
90	2.2987	5.2838	4.91	4.81	4.80	0.143	--	--	--
100	2.4902	6.2011	4.77	4.47	4.57	0.103	--	--	--
110	2.6628	7.0903	4.82	4.81	4.83	0.131	0.141	0.149	0.085
120	2.8151	7.9245	5.03	5.13	5.29	0.125	--	--	--

(iii)  $c_{HTAC} = 60 \text{ mM}$ 

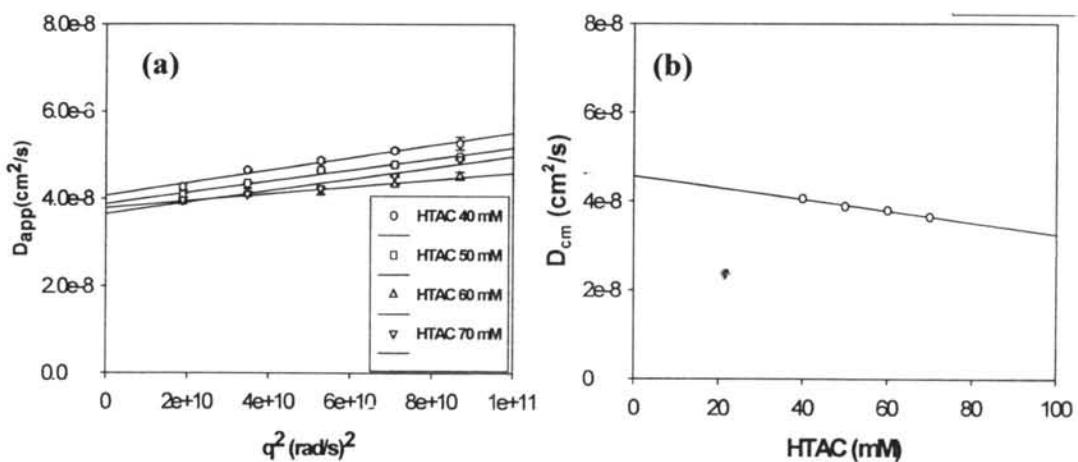
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$	
			Run 1	Run 2	Run 3	Run 1	Run 2
80	2.0896	4.3664	4.82	4.62	4.74	0.222	0.248
90	2.2987	5.2838	4.85	4.75	4.74	0.190	0.285
100	2.4902	6.2011	4.71	4.41	4.51	0.219	--
110	2.6628	7.0903	4.76	4.75	4.77	0.216	0.293
120	2.8151	7.9245	5.03	5.07	5.23	0.294	0.290

(iv)  $c_{HTAC} = 60 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$	
			Run 1	Run 2	Run 3	Run 1	Run 2
80	2.0896	4.3664	4.74	4.84	4.62	0.280	--
90	2.2987	5.2838	4.87	4.97	4.82	0.150	0.251
100	2.4902	6.2011	4.93	4.63	4.63	0.200	0.203
110	2.6628	7.0903	5.08	4.98	5.28	0.300	0.357
120	2.8151	7.9245	5.19	5.29	5.49	0.270	0.219

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	PEO60_40+HTAC 5 mM + [NaSal]/[HTAC] = 1		
		$D_0 \times 10^{12}$ (m <sup>2</sup> /s)	R <sub>h</sub> (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
40	4.40			
50	4.32			
60	4.2	4.92	45.1	
70	4.00			0.21

B4.3 PEO6\_40 + [NaSal]/[HTAC] = 5 in aqueous solution



**Figure 4.3** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of PEO6\_40 + [NaSal]/[HTAC] = 5 at 30°C.

(i)  $c_{HTAC} = 40 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	4.41	4.21	4.18	0.312	0.315	0.322
70	1.8646	3.4769	4.67	4.61	4.68	0.324	0.334	0.327
90	2.2987	5.2838	4.87	4.77	4.97	0.341	0.337	0.347
110	2.6628	7.0903	5.15	5.05	--	0.365	0.364	0.361
130	2.9459	8.6784	5.42	5.12	--	0.385	0.381	0.388

(ii)  $c_{HTAC} = 50 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	4.13	4.10	4.00	0.331	0.333	0.337
70	1.8646	3.4769	4.34	4.32	4.39	0.337	0.416	0.344
90	2.2987	5.2838	4.65	4.61	4.69	0.352	0.398	0.322
110	2.6628	7.0903	4.78	4.71	4.85	0.461	0.432	0.449
130	2.9459	8.6784	5.01	4.91	4.97	0.400	0.422	0.432

(iii)  $c_{HTAC} = 60 \text{ mM}$ 

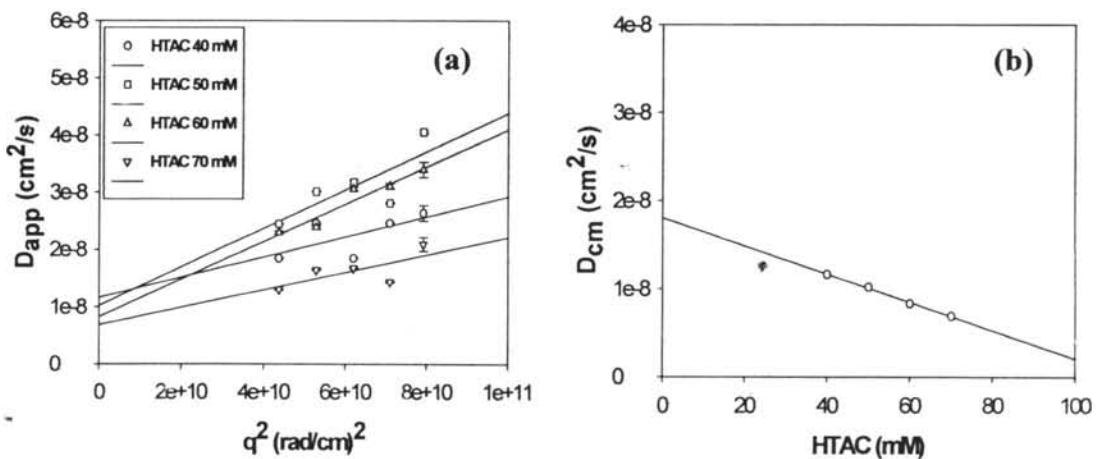
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	3.87	3.92	3.99	0.387	0.337	0.346
70	1.8646	3.4769	3.99	4.19	4.26	0.379	0.341	0.350
90	2.2987	5.2838	4.14	4.24	4.04	0.390	0.350	0.341
110	2.6628	7.0903	4.34	4.33	4.32	0.421	0.411	0.434
130	2.9459	8.6784	4.56	4.66	4.36	0.465	0.425	0.423

(iv)  $c_{HTAC} = 70 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
50	1.3739	1.8877	3.89	3.94	4.05	0.410	0.368	0.379
70	1.8646	3.4769	4.00	4.11	4.19	0.341	0.334	0.333
90	2.2987	5.2838	4.25	4.21	--	0.415	0.481	0.438
110	2.6628	7.0903	4.54	4.50	--	0.450	0.436	0.465
130	2.9459	8.6784	4.92	4.90	--	0.500	0.422	0.412

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	PEO60_40+HTAC 5 mM + [NaSal]/[HTAC] = 5		
		$D_o \times 10^{12}$ (m <sup>2</sup> /s)	R <sub>h</sub> (nm)	$\frac{\mu_2}{\Gamma^2}$
40	4.06			
50	3.89			
60	3.79	4.59	48.4	0.23
70	3.65			

B4.4 PEO20\_15 + HTAC in aqueous solution



**Figure 4.4** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of PEO20\_15 + HTAC at 30°C.

(i)  $c_{HTAC} = 40 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	1.84	1.86	1.84	0.835	0.809	0.742
90	2.2987	5.2838	2.49	2.46	2.43	0.779	0.782	0.796
100	2.4902	6.2011	2.63	2.40	2.88	0.700	0.841	0.750
110	2.6628	7.0903	3.20	3.13	3.01	0.676	0.710	0.790
120	2.8151	7.9245	3.19	3.09	3.02	0.659	0.731	0.711

(ii)  $c_{HTAC} = 50 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.44	2.47	2.43	0.812	0.765	0.780
90	2.2987	5.2838	3.02	3.00	3.02	0.796	0.730	0.791
100	2.4902	6.2011	3.15	3.24	3.13	0.728	0.723	0.706
110	2.6628	7.0903	2.79	2.81	2.83	0.677	0.679	0.687
120	2.8151	7.9245	4.04	4.03	4.11	0.619	0.645	0.606

(iii)  $c_{HTAC} = 60 \text{ mM}$ 

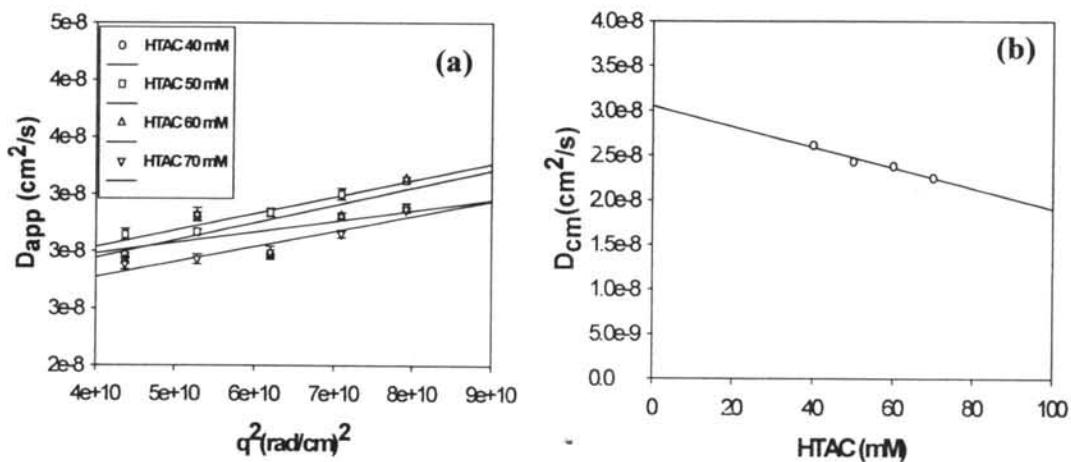
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.34	2.26	2.30	0.913	0.942	0.955
90	2.2987	5.2838	2.37	2.36	2.43	0.908	0.907	0.989
100	2.4902	6.2011	3.00	3.05	3.12	0.932	0.908	0.915
110	2.6628	7.0903	3.03	3.21	3.08	0.962	0.911	0.935
120	2.8151	7.9245	3.14	3.45	3.60	0.939	0.917	0.958

(iv)  $c_{HTAC} = 70 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	1.29	1.29	1.32	0.963	0.930	0.920
90	2.2987	5.2838	1.64	1.63	1.67	0.944	0.957	0.952
100	2.4902	6.2011	1.66	1.67	1.69	0.902	0.983	0.978
110	2.6628	7.0903	1.42	1.43	1.46	0.904	0.878	0.910
120	2.8151	7.9245	1.97	1.97	2.33	0.949	0.848	0.927

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	PEO20_15+HTAC 5 mM		
		$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
40	1.16			
50	1.02			
60	8.32	2.40	92.7	0.61
70	6.90			

B4.5 PEO20\_15 + [NaSal]/[HTAC] = 1 in aqueous solution



**Figure 4.5** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of PEO20\_15 + [NaSal]/[HTAC] = 1 at 30°C.

(i)  $c_{\text{HTAC}} = 40 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 (\text{cm}^2/\text{s})$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.99	2.96	2.94	0.317	0.312	0.322
90	2.2987	5.2838	3.28	3.38	3.26	0.333	0.342	0.322
100	2.4902	6.2011	3.33	3.46	3.36	0.361	0.338	0.318
110	2.6628	7.0903	3.66	3.56	3.69	0.288	0.294	0.342
120	2.8151	7.9245	3.96	3.91	3.82	0.386	0.335	0.335

(ii)  $c_{\text{HTAC}} = 50 \text{ mM}$

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 (\text{cm}^2/\text{s})$			$\frac{\mu_2}{\Gamma^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	3.07	3.24	3.12	0.389	0.333	0.329
90	2.2987	5.2838	3.18	3.19	3.12	0.365	0.341	0.367
100	2.4902	6.2011	3.32	3.41	3.29	0.356	0.359	0.369
110	2.6628	7.0903	3.52	3.41	3.58	0.354	0.415	0.400
120	2.8151	7.9245	3.62	3.68	3.58	0.370	0.433	0.411

(iii)  $c_{HTAC} = 60 \text{ mM}$ 

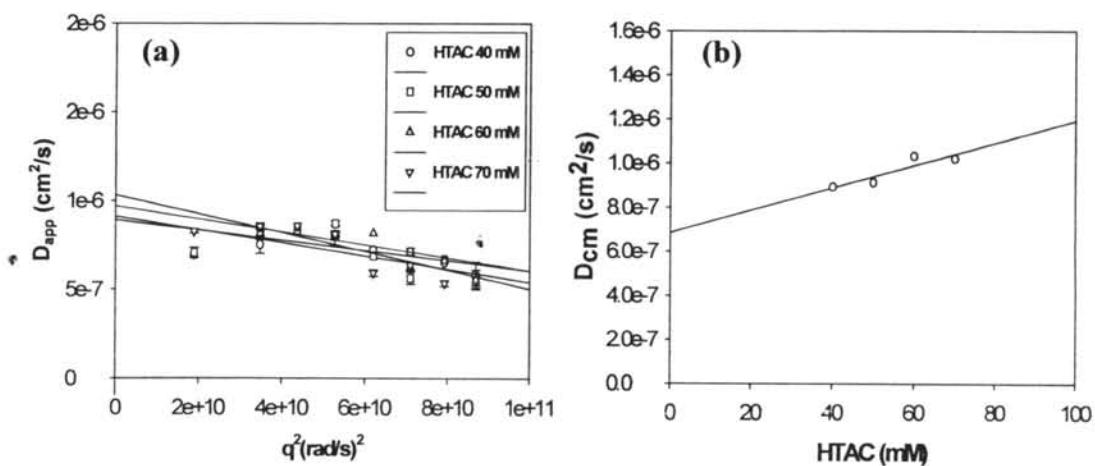
Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.86	2.93	2.97	0.399	0.369	0.363
90	2.2987	5.2838	3.21	3.34	3.41	0.444	0.476	0.460
100	2.4902	6.2011	2.98	--	--	0.450	0.489	0.436
110	2.6628	7.0903	3.31	--	--	0.440	0.434	0.527
120	2.8151	7.9245	3.64	--	--	0.480	0.405	0.400

(iv)  $c_{HTAC} = 70 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^8 \text{ (cm}^2/\text{s)}$			$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 1	Run 2	Run 3
80	2.0896	4.3664	2.97	2.87	2.81	0.356	0.354	0.333
90	2.2987	5.2838	3.01	2.92	2.86	0.363	0.370	0.347
100	2.4902	6.2011	3.09	2.98	2.89	0.376	0.375	0.356
110	2.6628	7.0903	3.12	3.22	3.12	0.389	0.355	0.385
120	2.8151	7.9245	3.35	3.39	3.37	0.360	0.395	0.376

HTAC (mM)	$D_{cm} \times 10^8$ (cm <sup>2</sup> /s)	PEO20_15+HTAC 5 mM + [NaSal]/[HTAC] = 1		
		$D_o \times 10^{12}$ (m <sup>2</sup> /s)	$R_h$ (nm)	$\frac{\mu_2}{\bar{\Gamma}^2}$
40	2.61			
50	2.43			
60	2.38	3.08	72.2	0.25
70	2.25			

B4.6 PEO20\_15 + [NaSal]/[HTAC] = 5 in aqueous solution



**Figure 4.6** (a) Apparent diffusion coefficient,  $D_{app}$  as a function of square of scattering wave vector,  $q^2$  at different HTAC concentrations and (b) Center of mass diffusion coefficient,  $D_{cm}$  as a function of HTAC concentration for aqueous solution of PEO20\_15 + [NaSal]/[HTAC] = 5 HTAC at 30°C.

(i)  $c_{HTAC} = 40$  mM

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7$ (cm <sup>2</sup> /s)				$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 4	Run 1	Run 2	Run 3
50	1.3739	1.8877	6.93	--	--	--	0.539	0.553	0.546
70	1.8646	3.4769	7.00	7.08	8.50	--	0.296	0.284	0.286
80	2.0896	4.3664	8.28	--	--	--	0.158	--	--
90	2.2987	5.2838	8.05	8.22	8.29	7.91	0.019	0.069	0.076
100	2.4902	6.2011	7.23	--	--	--	0.357	--	--
110	2.6628	7.0903	7.17	6.89	7.73	6.82	0.286	0.336	0.202
120	2.8151	7.9245	6.53	--	--	--	0.512	--	--
130	2.9459	8.6784	7.56	4.03	6.03	5.77	0.176	0.400	0.509

(ii)  $c_{HTAC} = 50 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$				$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 4	Run 1	Run 2	Run 3
50	1.3739	1.8877	6.97	7.63	6.62	--	0.316	0.239	0.327
70	1.8646	3.4769	8.12	8.38	8.73	7.41	0.237	--	--
80	2.0896	4.3664	8.54	--	--	--	0.247	--	--
90	2.2987	5.2838	8.59	9.09	8.64	8.59	0.307	--	--
100	2.4902	6.2011	6.90	--	--	--	0.328	--	--
110	2.6628	7.0903	4.80	5.54	5.75	6.45	0.434	--	--
120	2.8151	7.9245	6.70	--	--	--	0.429	--	--
130	2.9459	8.6784	5.10	5.49	5.19	6.22	0.408	--	--

(iii)  $c_{HTAC} = 60 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$				$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 4	Run 1	Run 2	Run 3
70	1.8646	3.4769	8.58	8.61	8.53	7.01	0.281	--	--
90	2.2987	5.2838	8.14	8.69	8.10	6.72	0.334	--	--
100	2.4902	6.2011	8.18	--	--	--	0.263	--	--
110	2.6628	7.0903	6.60	6.16	5.67	6.72	0.421	0.511	0.634
120	2.8151	7.9245	6.65	--	--	--	0.406	--	--
130	2.9459	8.6784	6.86	4.95	6.09	4.36	0.365	0.523	--

(iv)  $c_{HTAC} = 70 \text{ mM}$ 

Angle (degree)	$q \times 10^{-5}$ (rad/cm)	$q^2 \times 10^{-10}$ (rad/cm) <sup>2</sup>	$D_{app} \times 10^7 \text{ (cm}^2/\text{s)}$				$\frac{\mu_2}{\bar{\Gamma}^2}$		
			Run 1	Run 2	Run 3	Run 4	Run 1	Run 2	Run 3
50	1.3739	1.8877	8.18	8.15	8.51	--	0.160	0.158	0.179
70	1.8646	3.4769	8.75	8.75	8.74	7.95	0.208	--	--
80	2.0896	4.3664	8.58	--	--	--	0.218	--	--
90	2.2987	5.2838	8.45	8.01	7.62	8.38	0.238	--	--
100	2.4902	6.2011	5.82	5.60	5.65	5.95	0.338	--	--
110	2.6628	7.0903	6.37	--	--	--	0.473	--	--
120	2.8151	7.9245	5.02	5.40	5.82	5.18	0.514	--	--

HTAC (mM)	$D_{cm} \times 10^8$ ( $\text{cm}^2/\text{s}$ )	PEO20_15+HTAC 5 mM + [NaSal]/[HTAC] = 5		
		$D_0 \times 10^{12}$ ( $\text{m}^2/\text{s}$ )	$R_h$ (nm)	$\frac{\mu_2}{\Gamma^2}$
40	0.89			
50	0.91			
60	1.03	2.90	76.4	0.22
70	1.02			

**Appendix C Surface tension and Conductivity Data for Aqueous HTAC and PEO-HTAC and PEO-HTAC-NaSal solutions at 30°C**

*C1 Data from surface tension measurement at 30°C*

(C1.1) HTAC in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)			
	Run 1	Run 2	Run 3	Run 4
0.01	49.90	50.70	50.30	51.80
0.02	49.20	48.70	-	-
0.04	47.90	47.20	-	-
0.06	45.50	46.00	-	-
0.08	44.50	44.90	-	-
0.10	43.40	42.50	-	-
0.20	39.40	38.90	-	-
0.40	36.60	36.40	-	-
0.60	35.30	35.10	-	-
0.80	34.80	34.60	-	-
1.00	34.00	34.20	35.00	34.90
1.20	32.90	32.80	-	-
1.40	32.10	32.20	-	-
2.00	32.50	32.40	-	-
3.00	32.30	33.00	-	-
4.00	32.50	32.90	-	-
5.00	32.90	31.00	-	-

## (C1.2) PEO1\_40+ HTAC in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)	
	Run 1	Run 2
0.00	57.00	57.10
0.01	47.60	47.70
0.03	44.60	44.50
0.05	40.40	40.30
0.10	37.50	37.40
0.15	36.10	36.30
0.20	35.20	35.10
0.25	35.20	35.10
0.30	35.10	35.00
0.40	35.30	35.30
0.50	32.20	32.10
0.60	30.80	30.60
0.70	29.40	29.30
0.80	28.70	28.80
0.90	28.60	28.50
1.00	28.50	28.40
1.70	28.80	28.80
5.00	28.60	28.50

## (C1.3) PEO1\_200 + HTAC in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)	
	Run 1	Run 2
0.00	53.20	53.00
0.01	48.00	47.80
0.05	42.90	42.80
0.10	37.60	37.50
0.15	36.20	36.10
0.20	35.60	35.70
0.30	35.50	35.40
0.40	35.10	35.00
0.50	33.60	33.70
0.60	31.70	31.00
0.70	29.90	29.80
0.80	29.70	29.70
0.90	29.00	28.90
1.00	29.10	29.00
2.00	30.10	30.00
3.00	30.60	30.50
5.00	30.30	30.30

## (C1.4) PEO6\_40 + HTAC in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)				
	Run 1	Run 2	Run 3	Run 4	Run 5
0.00	63.06	63.07	63.09	63.04	62.93
0.02	62.15	62.20	62.15	62.08	62.17
0.05	61.36	61.23	60.99	60.94	60.94
0.10	58.62	58.39	58.17	58.03	58.85
0.12	59.13	59.05	59.00	58.96	58.87
0.15	58.93	58.81	59.66	59.60	--
0.18	59.93	59.81	59.66	60.60	--
0.20	60.11	59.98	59.89	59.78	59.69
0.30	58.56	58.32	58.22	58.09	58.48
0.40	57.26	57.06	56.92	56.79	56.70
0.50	56.88	56.11	55.96	55.76	55.61
0.60	55.29	55.70	54.90	54.54	54.43
0.70	53.99	53.39	54.43	54.31	54.14
0.80	53.00	52.86	52.72	52.44	52.25
0.90	51.06	50.85	50.67	50.57	50.44
1.00	50.33	49.81	49.63	49.18	48.98
1.50	45.60	45.32	45.10	45.06	45.55
1.80	42.36	42.79	42.62	42.25	42.07
2.00	42.34	42.88	42.59	42.28	42.10
3.00	41.87	41.97	41.69	42.45	42.18
4.00	42.03	41.88	41.73	41.59	41.50
5.00	40.48	40.35	40.44	40.27	40.34

(C1.5) PEO6\_40 + HTAC + [NaSal]/[HTAC] = 1 in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)				
	Run 1	Run 2	Run 3	Run 4	Run 5
0.00	63.17	62.97	63.36	62.99	62.89
0.02	61.56	61.41	61.29	61.19	61.84
0.05	61.04	61.21	60.86	60.48	60.77
0.10	58.95	58.78	58.66	58.92	58.84
0.12	58.94	58.76	59.19	58.88	59.36
0.15	56.97	56.22	55.94	57.01	56.36
0.20	56.68	56.59	55.79	56.09	57.14
0.30	56.07	56.48	56.42	56.24	56.98
0.40	54.42	54.59	55.72	54.32	54.66
0.50	53.72	53.63	54.07	53.78	52.79
0.60	52.23	52.01	51.68	51.66	52.40
0.70	51.12	51.80	51.06	51.49	50.94
0.80	49.62	50.52	49.37	50.15	49.47
0.90	47.92	47.36	48.49	48.48	47.31
1.00	44.92	45.05	44.89	45.03	44.33
1.50	41.68	41.42	41.12	41.54	41.19
2.00	42.01	41.69	41.92	41.60	41.92
3.00	41.27	41.38	41.50	41.06	40.94
4.00	41.12	41.54	41.29	41.18	41.44
5.00	39.95	40.01	40.21	40.03	40.03

(C1.6) PEO6\_40 + HTAC + [NaSal]/[HTAC] = 5 in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)				
	Run 1	Run 2	Run 3	Run 4	Run 5
0.00	63.17	62.97	63.36	62.99	62.89
0.02	60.59	60.69	60.82	60.64	61.02
0.05	60.02	60.21	60.33	60.47	59.99
0.10	58.44	58.57	59.20	58.68	59.24
0.12	58.57	58.19	57.92	57.76	57.50
0.15	55.48	55.31	56.14	55.51	55.28
0.20	55.98	55.97	55.67	55.95	55.95
0.30	55.63	55.92	55.16	55.50	55.79
0.40	52.63	52.17	51.68	51.97	51.48
0.50	51.30	50.68	51.16	51.60	51.55
0.60	48.64	49.11	48.60	48.73	49.05
0.70	44.76	44.44	44.11	44.74	44.38
0.80	42.49	42.86	42.85	42.63	42.30
0.90	41.95	41.59	41.03	41.77	41.32
1.00	40.82	40.40	40.68	40.19	40.94
1.50	40.01	40.00	40.30	40.05	40.09
2.00	39.62	39.37	39.68	40.09	39.45
3.00	39.14	39.63	39.03	39.88	39.73
4.00	38.47	38.63	38.40	38.36	38.51
5.00	38.48	38.21	38.50	38.32	38.13

## (C1.7) PEO6\_200 + HTAC in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)				
	Run 1	Run 2	Run 3	Run 4	Run 5
0.00	64.06	64.47	64.26	65.06	64.42
0.02	62.47	62.50	62.99	62.26	62.86
0.05	61.59	61.46	61.36	61.32	61.21
0.10	60.87	60.18	60.69	59.30	60.39
0.12	59.83	59.61	59.26	59.11	59.04
0.15	58.23	58.21	58.26	58.31	58.24
0.18	57.46	57.41	57.36	57.32	57.25
0.20	57.39	57.26	57.21	57.16	57.09
0.30	56.83	56.51	56.32	56.07	56.05
0.40	55.92	55.81	55.71	55.66	55.55
0.50	54.68	54.94	54.64	54.47	54.39
0.60	54.98	54.75	54.64	54.43	54.32
0.70	53.19	53.12	53.09	53.01	52.84
0.80	53.21	52.96	52.80	52.60	52.54
0.90	50.51	50.69	50.82	51.01	50.91
1.00	50.45	50.21	50.08	49.89	49.66
1.50	44.75	44.55	44.35	44.11	43.77
1.80	41.54	41.03	40.76	40.97	40.34
2.00	41.33	41.13	40.96	40.77	40.35
3.00	40.77	40.86	40.74	40.57	40.30
4.00	40.78	40.59	40.49	40.36	40.28
5.00	40.07	40.05	40.01	40.00	40.00

## (C1.8) PEO20\_15 + HTAC in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)	
	Run 1	Run 2
0.00	55.40	55.40
0.01	53.40	53.40
0.05	45.70	45.60
0.10	42.50	42.40
0.15	41.30	41.20
0.20	40.50	40.60
0.30	40.40	40.00
0.40	39.90	39.70
0.50	38.50	38.20
0.60	37.00	36.90
0.70	35.60	35.40
0.80	34.90	34.70
0.90	34.00	34.90
1.00	33.70	33.60
1.50	32.20	32.10
2.00	31.50	31.40
3.00	31.90	32.00
4.00	32.40	32.50
5.00	32.50	32.50

(C1.9) PEO20\_15 + HTAC + [NaSal]/[HTAC] = 1 in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)				
	Run 1	Run 2	Run 3	Run 4	Run 5
0.00	64.75	63.12	64.17	63.83	63.73
0.02	60.82	60.18	61.04	60.90	60.68
0.05	60.46	59.78	60.02	60.29	59.99
0.10	58.26	58.26	58.28	58.12	58.09
0.12	57.59	57.84	58.14	58.33	58.64
0.15	58.00	58.62	58.25	57.77	57.97
0.20	57.59	58.30	58.34	57.96	58.47
0.30	55.02	55.84	55.19	55.14	55.09
0.40	53.38	53.49	53.60	53.80	54.27
0.50	52.90	52.81	52.81	52.81	52.81
0.60	51.42	51.81	51.48	51.80	52.23
0.70	48.38	48.29	48.24	48.91	47.85
0.80	47.33	46.99	48.00	47.58	47.31
0.90	44.56	44.79	45.22	44.35	44.95
1.00	43.72	43.87	43.00	43.28	42.93
1.50	40.34	40.13	40.84	39.45	39.31
2.00	39.03	39.34	39.18	38.94	38.41
3.00	38.82	38.79	39.60	38.58	39.36
4.00	37.53	37.96	37.45	38.41	38.25
5.00	38.22	38.37	38.19	38.63	38.57

(C1.10) PEO20\_15 + HTAC + [NaSal]/[HTAC] = 5 in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)				
	Run 1	Run 2	Run 3	Run 4	Run 5
0.00	63.75	64.12	64.17	63.83	64.73
0.02	60.91	60.63	60.49	60.38	60.01
0.05	59.18	59.99	59.80	59.62	59.50
0.10	58.45	58.45	56.04	58.56	56.46
0.12	58.03	57.83	57.55	57.20	56.77
0.15	57.26	58.04	57.79	57.62	57.42
0.20	57.24	57.14	57.07	57.78	57.25
0.30	52.72	52.59	53.36	53.84	50.56
0.40	49.98	46.69	49.47	49.27	48.90
0.50	47.70	46.46	47.68	47.56	47.98
0.60	46.35	46.05	45.76	45.48	45.71
0.70	44.93	44.68	44.85	44.26	44.23
0.80	42.72	42.43	42.22	43.10	42.77
0.90	39.88	39.47	39.94	40.06	40.35
1.00	40.30	40.60	40.98	40.75	40.03
1.50	41.45	41.17	40.99	40.76	40.61
2.00	40.68	40.30	40.75	40.30	40.21
3.00	38.69	38.85	38.49	39.25	38.07
4.00	38.17	38.33	37.42	38.45	37.96
5.00	38.07	37.97	37.81	37.69	37.65

## (C1.11) PEO20\_200 + HTAC in aqueous solution

HTAC (mM)	$\gamma$ (mN/m)	
	Run 1	Run 2
0.00	55.30	55.60
0.01	54.40	--
0.05	47.50	47.50
0.10	43.80	43.80
0.20	40.40	40.30
0.30	40.60	40.50
0.40	40.10	40.00
0.50	40.40	40.40
0.60	39.80	39.70
0.70	39.90	39.80
0.80	38.10	38.00
0.90	37.40	37.30
1.00	35.00	35.10
2.00	34.20	34.10
3.00	35.20	35.10
5.00	35.20	35.10

*C2 Data from conductivity measurement at 30°C*

## (C2.1) HTAC in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	Run 1	Run 2
0.10	13.50	13.70
0.20	22.20	22.50
0.30	30.20	30.50
0.40	34.90	35.00
0.60	58.20	58.50
0.80	73.30	73.50
1.00	93.30	93.70
1.30	115.60	116.00
1.50	122.60	124.80
2.00	146.40	145.40
2.50	153.00	154.40
3.00	178.10	179.00
4.00	205.90	206.90
5.00	238.00	240.00

## (C2.2) HTAC + NaSal in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	[NaSal/[HTAC] = 1	[NaSal/[HTAC] = 5
0.00	10.87	10.87
0.10	175.20	797.00
0.20	331.00	1436.00
0.30	472.00	2070.00
0.50	762.00	3350.00
0.70	1049.00	4380.00
0.90	1312.00	5870.00
1.00	1451.00	6430.00
2.00	2650.00	12300.00
3.00	4000.00	17730.00
4.00	5340.00	23000.00
5.00	6300.00	28300.00

## (C2.3) PEO1\_40 + HTAC in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	Run 1	Run 2
0.00	10.72	10.75
0.05	17.50	17.80
0.10	21.20	21.30
0.15	26.80	26.90
0.20	31.50	31.90
0.25	34.80	34.70
0.30	38.60	--
0.40	45.80	--
0.50	52.40	52.20
0.60	59.90	59.60
0.70	65.10	64.90
0.80	71.70	71.60
0.90	80.20	80.30
1.00	88.10	88.30
3.00	181.40	181.00
5.00	243.00	242.00

## (C2.4) PEO1\_200 + HTAC in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )			
	Run 1	Run 2	Run 3	Run 4
0.00	12.07	12.37	13.46	13.54
0.05	15.02	15.01	--	--
0.10	20.06	20.08	20.23	20.34
0.15	26.50	26.40	--	--
0.20	28.40	28.60	--	--
0.30	36.30	36.40	--	--
0.40	43.30	43.40	--	--
0.50	50.50	50.80	--	--
0.60	57.00	57.00	--	--
0.70	63.00	62.90	--	--
0.80	73.30	73.20	72.90	73.00
0.90	81.60	81.50	81.80	--
1.00	88.50	88.60	88.30	88.40
2.00	144.80	145.80	147.60	--
3.00	181.70	181.00	178.00	--
5.00	240.00	241.00	--	--

## (C2.5) PEO6\_40 + HTAC in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )		
	Run 1	Run 2	Run 3
0.00	13.65	--	--
0.05	16.71	--	--
0.06	17.77	17.44	--
0.08	18.98	18.00	17.58
0.09	19.80	18.01	18.55
0.14	22.70	--	--
0.23	32.90	30.80	--
0.25	36.20	--	--
0.30	38.90	37.80	--
0.35	45.80	45.70	46.00
0.36	45.90	45.20	--
0.40	48.90	49.10	--
0.50	55.70	53.60	--
0.55	60.80	59.70	--
0.60	65.00	66.40	--
0.72	78.00	77.20	76.60
0.91	95.30	96.30	94.50
1.00	95.30	96.40	--
1.30	138.90	139.00	--
1.50	145.60	145.80	--
3.00	177.60	175.90	--
5.00	239.00	240.00	--

## (C2.6) PEO6\_40 + HTAC + NaSal in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	[NaSal/[HTAC] = 1]	[NaSal/[HTAC] = 5]
0.00	13.65	13.65
0.10	45.30	98.05
0.20	64.30	173.85
0.30	93.20	261.00
0.50	132.70	424.00
0.70	181.40	584.00
0.90	248.00	746.00
1.00	252.00	817.33
2.00	430.00	1495.50
3.00	590.00	2170.00
4.00	766.00	2850.00
5.00	918.00	3500.00

## (C2.7) PEO6\_200 + HTAC in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	Run 1	Run 2
0.00	9.12	9.13
0.02	10.83	10.97
0.04	12.05	12.15
0.06	14.12	14.04
0.08	15.37	15.62
0.10	16.96	16.72
0.20	25.50	25.90
0.30	35.10	35.20
0.40	43.50	43.60
0.50	50.10	49.90
1.00	97.00	95.80
3.00	183.50	184.60
5.00	242.00	243.00
7.00	302.00	303.00
10.00	389.00	390.00
20.00	659.00	661.00
30.00	960.00	958.00
50.00	1516.00	1518.00

## (C2.8) PEO6\_200 + HTAC + NaSal in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	[NaSal/[HTAC] = 1]	[NaSal/[HTAC] = 5]
0.00	9.13	9.13
0.10	49.30	138.00
0.20	76.40	203.00
0.30	102.10	301.00
0.50	141.15	460.00
0.70	208.50	623.00
0.90	247.00	782.50
1.00	281.50	883.50
2.00	462.50	1586.50
3.00	622.00	2180.00
4.00	772.00	2900.00
5.00	920.50	3565.00

## (C 2.9) PEO20\_15 + HTAC in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )		
	Run 1	Run 2	Run 3
0.00	12.80	12.99	13.00
0.05	15.97	15.80	--
0.15	28.70	29.60	29.40
0.20	39.60	39.40	30.30
0.30	42.10	41.90	42.20
0.40	51.90	52.00	51.60
0.50	60.90	61.00	61.20
0.60	68.70	69.10	71.90
0.80	86.50	86.00	86.30
0.90	90.50	90.20	112.20
1.00	102.30	104.30	--
2.00	170.70	172.80	181.00
3.00	222.30	220.20	219.50
5.00	298.00	296.00	--

(C2.10) PEO20\_15 + HTAC + NaSal in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	[NaSal/[HTAC] = 1]	[NaSal/[HTAC] = 5]
0.00	12.93	12.93
0.10	40.43	101.70
0.20	76.20	146.87
0.30	87.40	278.75
0.50	141.07	439.50
0.70	193.55	588.50
0.90	229.50	727.00
1.00	253.00	816.25
2.00	435.00	1489.00
3.00	602.33	2195.00
4.00	773.67	2850.00
5.00	961.50	3505.00

## (C2.11) PEO20\_200 + HTAC in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )		
	Run 1	Run 2	Run 3
0.00	17.54	17.55	--
0.05	24.20	24.19	--
0.10	32.70	32.90	--
0.20	47.80	48.00	--
0.30	59.00	59.20	--
0.40	70.00	70.10	--
0.50	77.60	77.70	--
0.60	86.80	86.90	--
0.70	96.40	95.30	--
0.80	106.10	109.10	--
0.90	114.10	119.80	116.10
1.00	121.60	120.80	--
2.00	184.70	188.00	187.00
3.00	228.00	226.00	227.00
5.00	294.00	296.00	297.00

(C2.12) PEO20\_200 + HTAC + NaSal in aqueous solution

HTAC (mM)	Conductance ( $\mu\text{S}/\text{cm}$ )	
	[NaSal/[HTAC] = 1	[NaSal/[HTAC] = 5
0.00	17.55	17.55
0.10	48.40	135.20
0.20	90.30	201.00
0.30	101.00	289.00
0.50	155.10	452.00
0.70	207.00	611.50
0.90	244.00	758.50
1.00	268.00	807.00
2.00	436.00	1590.00
3.00	602.00	2360.00
4.00	762.50	2730.00
5.00	991.50	3640.00

## Appendix D Rheological Data of Water at 30°C

$$\tau_w = (M_{DCU} - M_{SCU})K_\tau$$

$$K_\tau = \frac{1}{2\pi L(R_{IB})^2}$$

$$\dot{\gamma} = \dot{\theta} K_\gamma$$

$$\%DR = \frac{f_o - f}{f_o} \times 100$$

$$K_\gamma = \frac{2}{\left(1 - \left(\frac{R_{IC}}{R_{IB}}\right)^2\right)}$$

$$Re = \frac{\dot{\theta} R_{IC} (R_{IB} - R_{IC})}{\nu}$$

$$f = \frac{2\tau_w}{\rho (\dot{\theta} R_{IC})^2}$$

where  $\tau_w$  = inner wall shear stress ( $N/m^2$ )

$M_{DCU}$  = total torque measuring from double Couette cell (N.m)

$M_{SCU}$  = total torque measuring from single Couette cell (N.m)

$K_\tau$  = stress constant =  $12207.62\ m^3$

$L$  = bob length (m)

$R_{IB}$  = inner radius of bob (m)     $R_{IC}$  = inner radius of cub (m)

$\dot{\gamma}$  = shear rate ( $m^{-1}$ )     $\dot{\theta}$  = motor angular velocity (rad/m)

$K_\gamma$  = strain constant = 6.61

$\nu$  = kinematic viscosity ( $m^2/s$ )

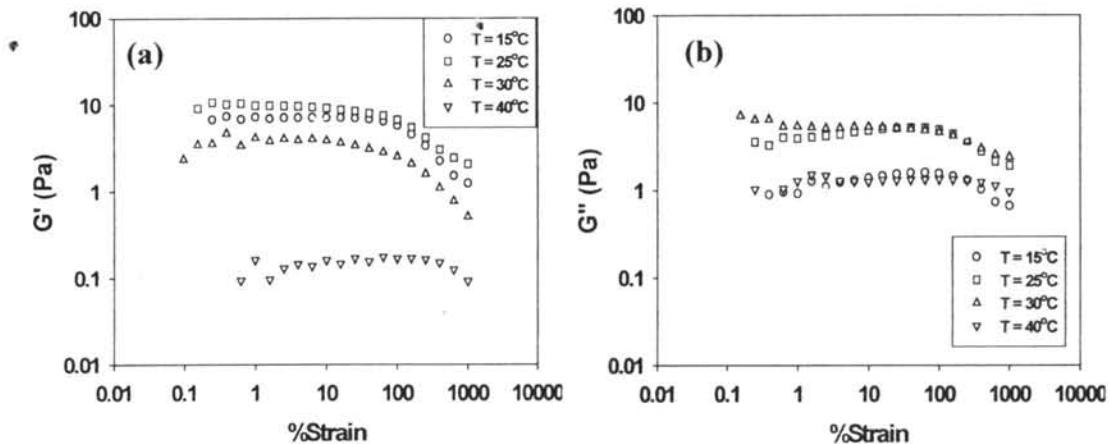
$f$  = friction factor of solution     $f_0$  = friction factor of solvent

$\rho$  = density of solvent ( $kg/m^3$ )

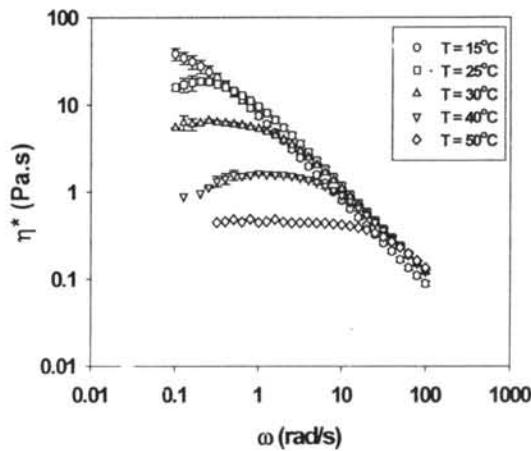
M <sub>DCU</sub>			M <sub>SCU</sub>			τ <sub>inner</sub>			ẏ	θ̇	Re	f		
Run 1	Run 2	Run 3	Run 1	Run 2	Run 3	Run 1	Run 2	Run 3				Run 1	Run 2	Run 3
1.433e-6	1.46e-6	1.69e-6	1.79e-7	2.52e-7	2.16e-7	0.015	0.015	0.018	6.31	0.95	93.21	0.650	0.626	0.763
1.637e-6	1.76e-6	1.88e-6	2.22e-7	3.24e-7	2.69e-7	0.017	0.017	0.020	7.36	1.11	108.68	0.540	0.546	0.615
1.899e-6	2.03e-6	2.16e-6	2.45e-7	3.58e-7	2.84e-7	0.020	0.020	0.023	8.58	1.30	126.71	0.464	0.469	0.528
2.219e-6	2.31e-6	2.49e-6	2.58e-7	3.50e-7	3.10e-7	0.024	0.024	0.027	10.00	1.51	147.73	0.405	0.406	0.450
2.505e-6	2.77e-6	2.81e-6	3.08e-7	3.93e-7	3.67e-7	0.027	0.029	0.030	11.66	1.76	172.24	0.334	0.361	0.371
2.988e-6	3.16e-6	3.28e-6	3.67e-7	4.19e-7	3.94e-7	0.032	0.033	0.035	13.59	2.06	200.82	0.293	0.306	0.322
3.488e-6	3.70e-6	3.80e-6	4.43e-7	4.74e-7	4.68e-7	0.037	0.039	0.041	15.85	2.40	234.14	0.250	0.265	0.274
4.051e-6	4.30e-6	4.45e-6	4.93e-7	5.50e-7	5.40e-7	0.043	0.046	0.048	18.48	2.80	272.99	0.215	0.227	0.237
4.702e-6	4.98e-6	5.16e-6	5.48e-7	6.38e-7	6.28e-7	0.051	0.053	0.055	21.54	3.26	318.28	0.185	0.193	0.202
5.468e-6	5.89e-6	6.02e-6	6.22e-7	7.18e-7	7.58e-7	0.059	0.063	0.064	25.12	3.80	371.09	0.159	0.169	0.172
6.451e-6	6.93e-6	7.00e-6	7.40e-7	8.36e-7	8.90e-7	0.070	0.074	0.075	29.29	4.43	432.66	0.138*	0.147	0.147
7.573e-6	8.12e-6	8.28e-6	8.71e-7	9.72e-7	1.03e-6	0.082	0.087	0.089	34.15	5.17	504.44	0.119	0.127	0.128
8.977e-6	9.52e-6	9.69e-6	1.04e-6	1.14e-6	1.25e-6	0.097	0.102	0.103	39.81	6.02	588.14	0.103	0.109	0.110
10.55e-6	1.12e-5	1.14e-5	1.26e-6	1.33e-6	1.44e-6	0.113	0.120	0.121	46.42	7.02	685.72	0.089	0.094	0.095
12.43e-6	1.32e-5	1.34e-5	1.49e-6	1.56e-6	1.73e-6	0.134	0.142	0.143	54.12	8.19	799.49	0.077	0.082	0.082
14.71e-6	1.56e-5	1.57e-5	1.78e-6	1.82e-6	2.04e-6	0.158	0.168	0.167	63.10	9.55	932.13	0.067	0.071	0.071
17.42e-6	1.84e-5	1.87e-5	2.13e-6	2.18e-6	2.42e-6	0.187	0.199	0.199	73.56	11.13	1086.79	0.058	0.062	0.062
20.73e-6	2.19e-5	2.22e-5	2.51e-6	2.55e-6	2.85e-6	0.223	0.236	0.237	85.77	12.98	1267.10	0.051	0.054	0.054
24.55e-6	2.60e-5	2.64e-5	2.97e-6	3.01e-6	3.35e-6	0.264	0.280	0.281	100.00	15.13	1477.33	0.045	0.047	0.048
29.23e-6	3.09e-5	3.12e-5	3.54e-6	3.58e-6	3.97e-6	0.314	0.334	0.333	116.59	17.64	1722.44	0.039	0.042	0.041
34.97e-6	3.69e-5	3.73e-5	4.21e-6	4.24e-6	4.71e-6	0.376	0.399	0.398	135.94	20.57	2008.23	0.034	0.037	0.036
41.94e-6	4.41e-5	4.45e-5	5.03e-6	5.03e-6	5.62e-6	0.451	0.477	0.474	158.49	23.98	2341.41	0.030	0.032	0.032
50.12e-6	5.26e-5	5.29e-5	5.97e-6	6.05e-6	6.72e-6	0.539	0.568	0.564	184.79	27.96	2729.89	0.027	0.028	0.028
60.19e-6	6.27e-5	6.31e-5	7.13e-6	7.23e-6	7.99e-6	0.648	0.678	0.673	215.44	32.60	3182.82	0.024	0.025	0.025
72.31e-6	7.49e-5	7.55e-5	8.43e-6	8.64e-6	9.45e-6	0.780	0.808	0.807	251.19	38.01	3710.90	0.021	0.022	0.022
86.66e-6	8.93e-5	8.99e-5	9.81e-6	1.00e-5	1.12e-5	0.938	0.967	0.961	292.87	44.32	4326.59	0.019	0.019	0.019
104.1e-6	1.06e-4	1.07e-4	1.18e-5	1.19e-5	1.32e-5	1.127	1.147	1.149	341.46	51.67	5044.43	0.016	0.017	0.017

**Appendix E Rheological Data on Isotropic Phase of Wormlike Micelles in Aqueous Solutions Containing Cationic Surfactant, Sodium Salicylate and Poly(ethylene oxide)**

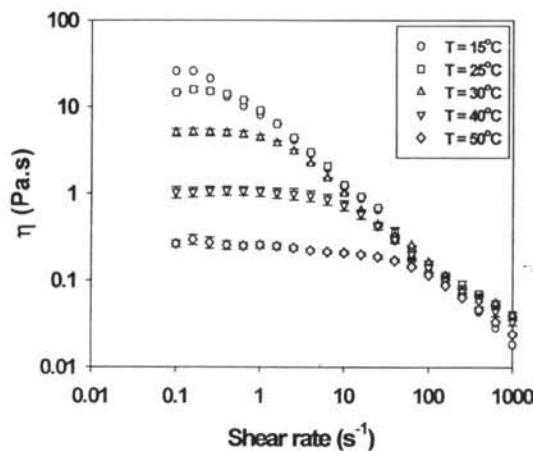
E1 Temperature effect data for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1 without PEO



**Figure 1.1** The plots of storage modulus,  $G'$  (a) and loss modulus,  $G''$  (b) on %strain at different temperatures for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1, the mole ratio of NaSal to HTAC equal to one.

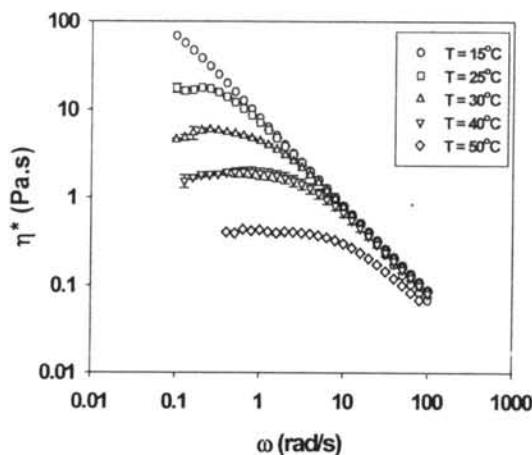


**Figure 1.2** Dependence of dynamic viscosity,  $\eta^*$  on frequency,  $\omega$  at different temperatures for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1, the mole ratio of NaSal to HTAC equal to one.

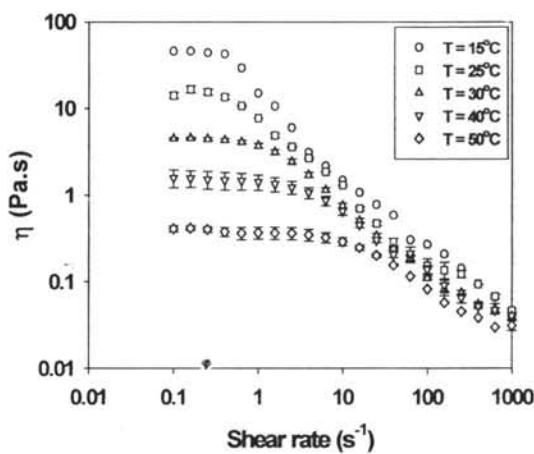


**Figure 1.3** Dependence of shear viscosity,  $\eta$  on shear rate,  $\dot{\gamma}$  at different temperatures for aqueous solutions of HTAC 50 mM +  $[\text{NaSal}]/[\text{HTAC}] = 1$ , the mole ratio of NaSal to HTAC equal to one.

E2 Temperature effect data for aqueous solutions of HTAC 50 mM +  $[\text{NaSal}]/[\text{HTAC}] = 1$  in the presence of PEO

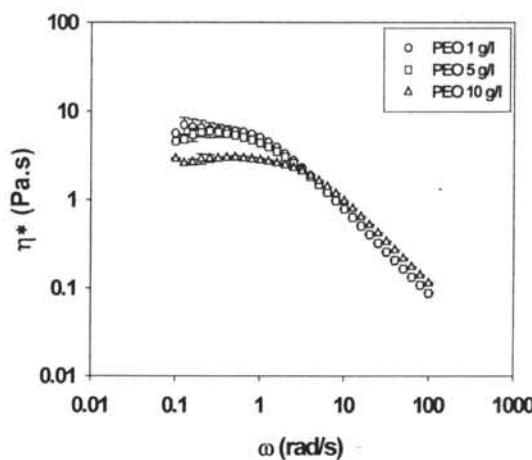


**Figure 2.1** Dependence of dynamic viscosity,  $\eta^*$  on frequency,  $\omega$  at different temperatures for aqueous solutions of HTAC 50 mM +  $[\text{NaSal}]/[\text{HTAC}] = 1 + \text{PEO } 5 \text{ g/l}$ , the mole ratio of NaSal to HTAC equal to one and PEO  $M_w 1 \times 10^5 \text{ g/mol}$ .

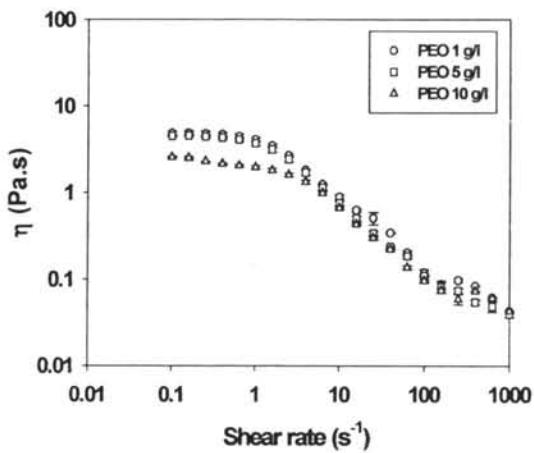


**Figure 2.2** Dependence of shear viscosity,  $\eta$  on shear rate,  $\dot{\gamma}$  at different temperatures for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1 + PEO 5 g/l, the mole ratio of NaSal to HTAC equal to one and PEO  $M_w$   $1 \times 10^5$  g/mol.

E3 PEO concentration effect data for aqueous solutions of HTAC 50 mM + PEO + [NaSal]/[HTAC] = 1 at 30°C

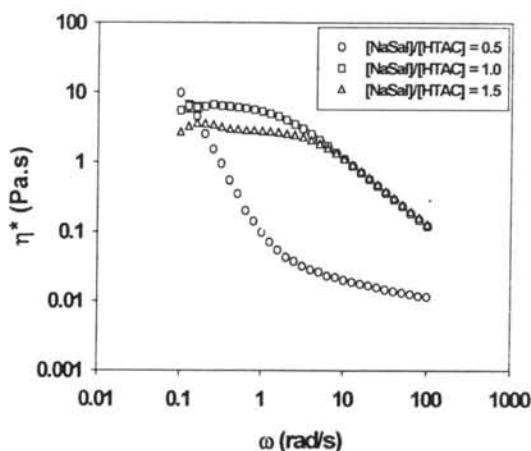


**Figure 3.1** Dependence of dynamic viscosity,  $\eta^*$  on frequency,  $\omega$  at different PEO concentrations for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1 + PEO at 30°C, the mole ratio of NaSal to HTAC equal to one and PEO  $M_w$   $1 \times 10^5$  g/mol.

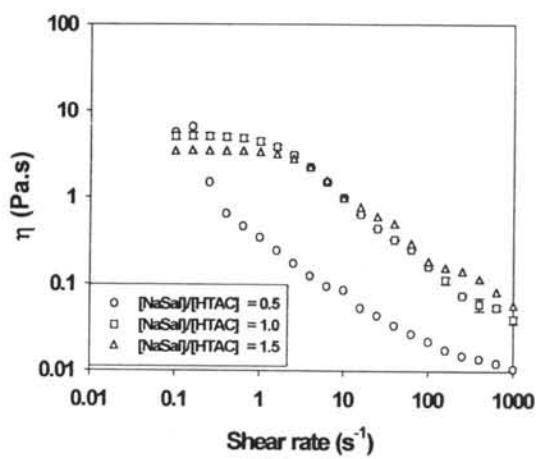


**Figure 3.2** Dependence of shear viscosity,  $\eta$  on shear rate,  $\dot{\gamma}$  at different PEO concentrations for aqueous solutions of HTAC 50 mM +  $[NaSal]/[HTAC] = 1$  + PEO at 30°C, the mole ratio of NaSal to HTAC equal to one and PEO  $M_w 1 \times 10^5$  g/mol.

E4 Salt concentration effect data for aqueous solutions of HTAC 50 mM + NaSal without PEO at 30°C

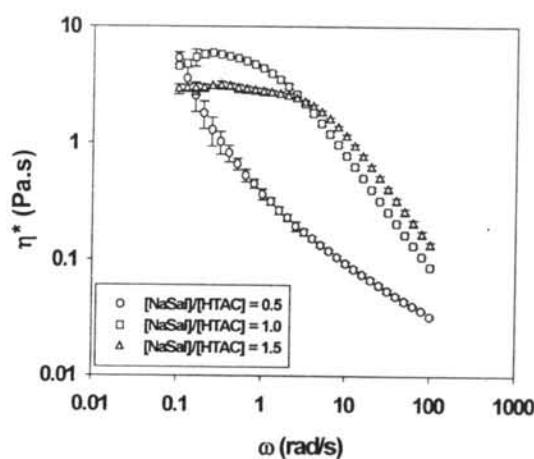


**Figure 4.1** Dependence of dynamic viscosity,  $\eta^*$  on frequency,  $\omega$  at different mole ratios of NaSal to HTAC for aqueous solutions of HTAC 50 mM and NaSal at 30°C.

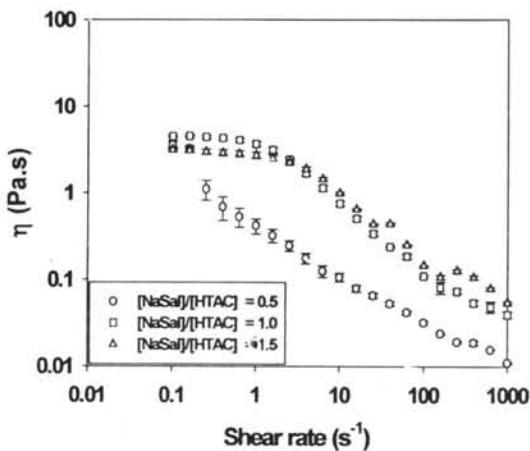


**Figure 4.2** Dependence of shear viscosity,  $\eta$  on shear rate,  $\dot{\gamma}$  at different mole ratios of NaSal to HTAC for aqueous solutions of HTAC 50 mM and NaSal at 30°C.

E5 Salt concentration effect data for aqueous solutions of HTAC 50 mM + NaSal in the presence of PEO at 30°C

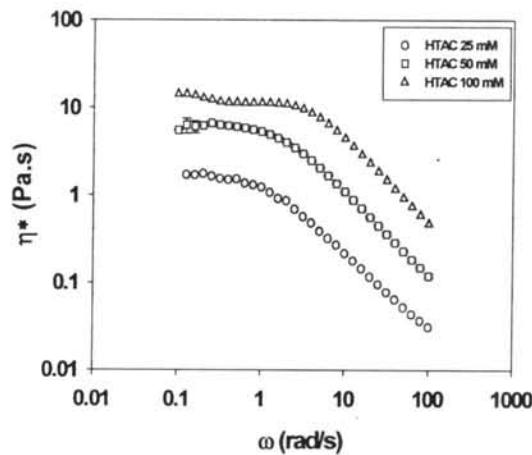


**Figure 5.1** Dependence of dynamic viscosity,  $\eta^*$  on frequency,  $\omega$  at different mole ratios of NaSal to HTAC for aqueous solutions of HTAC 50 mM + NaSal + PEO 5 g/l at 30°C, PEO  $M_w$   $1 \times 10^5$  g/mol.

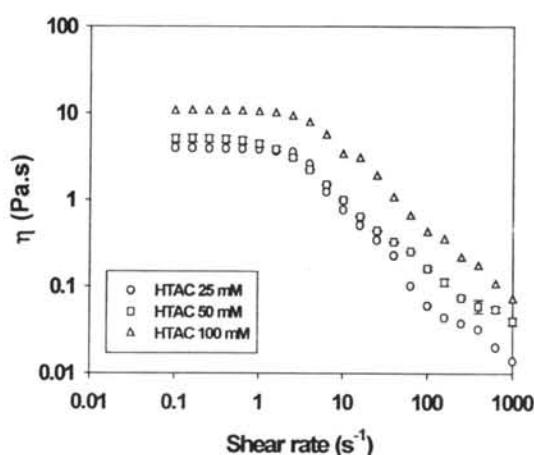


**Figure 5.2** Dependence of shear viscosity,  $\eta$  on shear rate,  $\dot{\gamma}$  at different mole ratios of NaSal to HTAC for aqueous solutions of HTAC 50 mM + NaSal + PEO 5 g/l at 30°C, PEO  $M_w$   $1 \times 10^5$  g/mol.

E6 HTAC concentration effect data for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1 without PEO at 30°C

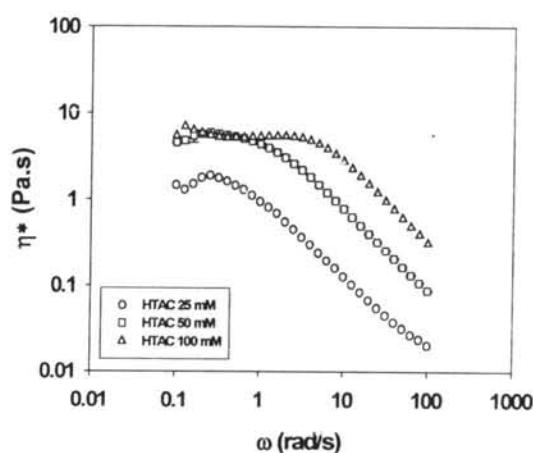


**Figure 6.1** Dependence of dynamic viscosity,  $\eta^*$  on frequency,  $\omega$  at different HTAC concentrations for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1 at 30°C, the mole ratio of NaSal to HTAC equal to one.

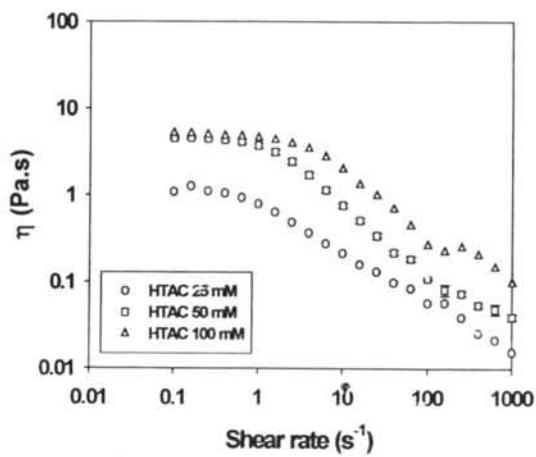


**Figure 6.2** Dependence of shear viscosity,  $\eta$  on shear rate,  $\dot{\gamma}$  at different HTAC concentrations for aqueous solutions of HTAC 50 mM +  $[\text{NaSal}]/[\text{HTAC}] = 1$  at  $30^\circ\text{C}$ , the mole ratio of NaSal to HTAC equal to one.

E7 HTAC concentration effect data for aqueous solutions of HTAC 50 mM +  $[\text{NaSal}]/[\text{HTAC}] = 1$  in the presence of PEO at  $30^\circ\text{C}$



**Figure 7.1** Dependence of dynamic viscosity,  $\eta^*$  on frequency,  $\omega$  at different HTAC concentrations for aqueous solutions of HTAC 50 mM +  $[\text{NaSal}]/[\text{HTAC}] = 1$  + PEO 5 g/l at  $30^\circ\text{C}$ , the mole ratio of NaSal to HTAC equal to one and PEO  $M_w 1 \times 10^5$  g/mol.



**Figure 7.2** Dependence of shear viscosity,  $\eta$  on shear rate,  $\dot{\gamma}$  at different HTAC concentrations for aqueous solutions of HTAC 50 mM + [NaSal]/[HTAC] = 1 + PEO 5 g/l at 30°C, the mole ratio of NaSal to HTAC equal to one and PEO M<sub>w</sub> 1 × 10<sup>5</sup> g/mol.

## Appendix F Critical Reynolds number, Re for Taylor Instability and Turbulent Flow Transition

**Table 1** Critical values of  $R_{c,1}((r_o - r_i)/r_i)^{1/2}$  for different values of  $\eta = r_i/r_o$  and  $\mu = \Omega_o/\Omega_i = 0$

Radius ratio, $\eta$	$R_{c,1}((r_o - r_i)/r_i)^{1/2}$	References
1.00	41.18	J. Walowit et al. 1964 <sup>a</sup>
0.95	42.44	P.H. Roberts. 1965 <sup>b</sup>
0.90	43.87	P.H. Roberts. 1965
0.85	45.50	P.H. Roberts. 1965
0.80	47.37	J. Walowit et al. 1964
0.75	49.52	P.H. Roberts. 1965
0.70	52.04	J. Walowit et al. 1964
0.65	55.01	P.H. Roberts. 1965
0.60	58.56	J. Walowit et al. 1964
0.50	68.19	P.H. Roberts. 1965
0.40	83.64	J. Walowit et al. 1964
0.30	118.89	J. Walowit et al. 1964
0.20	176.26	P.H. Roberts. 1965
0.10	423.48	E.M. Sparrow et al. 1974 <sup>c</sup>

Note:  $R_{c,1}$  = a critical Reynolds number for Taylor instability

$$R_{c,1} = \Omega_1 r_i (r_o - r_i) / v$$

$r_o$  = a radius of outer cylinders

$r_i$  = a radius of inner cylinders

$\eta$  = a dimensionless radius ratio

$\Omega_o$  = an angular velocity of outer cylinders

$\Omega_i$  = an angular velocity of inner cylinders

$\mu$  : a dimensionless angular ratio

$v$  : a kinematic viscosity of solution

- <sup>a</sup>J. Walowit, S. Tsao, R.C. DiPrima: Stability of flow between arbitrarily spaced concentric cylindrical surfaces including the effect of a radial temperature gradient. *Trans. Am. Soc. Mech. Eng., J. Appl. Mech.* 31, 585-593 (1964)
- <sup>b</sup>P.H. Roberts: The solution of the characteristic value problems. *Proc. R. Soc. London A*, 283, 550-556 (1965)
- <sup>c</sup>E.M. Sparrow, W.D. Munro, V.K. Jonsson: Instability of the flow between rotating cylinders: the wide gap problem. *J. Fluid Mech.* 20, 35-46 (1964)

**Table 2** Critical values of  $T_{c,1}$  for instability of the flow between rotating cylinders for different values of  $\eta = r_i/r_o$  and  $\mu = \Omega_o/\Omega_i = 0$

Radius ratio $\eta$	Critical Taylor number $T_{c,1}$	References
0.95	15170000	
0.75	20930	
0.50	74390	E.M. Sparrow, W.D. Munro and V.K. Jonsson. 1964 <sup>a</sup>
0.35	176400	
0.25	679000	
0.10	3460000	

Note:  $T_{c,1}$  = a critical Taylor number for Taylor instability ,  $T_{c,1} = \Omega_i^2 r_0^4 / v^2$

$r_o$  = a radius of outer cylinders

$r_i$  = a radius of inner cylinders

$\eta$  = a dimensionless radius ratio

$\Omega_o$  = an angular velocity of outer cylinders

$\Omega_i$  = an angular velocity of inner cylinders

$\mu$  = a dimensionless angular ratio

$v$  = a kinematic viscosity of solution

<sup>a</sup>E.M. Sparrow, W.D. Munro, V.K. Jonsson: Instability of the flow between rotating cylinders: the wide gap problem. *J. Fluid Mech.* 20, 35-46 (1964)

**Table 3** Critical values of  $R_{c,2}$  for wavy vortex flow

Radius ratio $\eta$	Critical Reynolds number $R_{c,2}$	References
0.95	$1.05 R_{c,1} - 1.10 R_{c,1}$	H.A. Snyder (1969) <sup>a</sup> , H.A. Snyder and R. B. Lambert (1966) <sup>b</sup> , W. Debler et al. (1969) <sup>c</sup>
0.50	$1.0 R_{c,1}$	

Note:  $R_{c,1}$  = a critical Reynolds number for Taylor instability

$R_{c,2}$  = a critical Reynolds number for wavy vortex flow (the flow at which the axisymmetric Taylor vortex flow becomes unstable)

<sup>a</sup>H.A. Snyder: Change in waveform and mean flow associated with wavelength variations in rotating Couette flow. Part 1. *J. Fluid Mech.* 35, 337-352 (1969)

<sup>b</sup>H.A. Snyder, R.B. Lambert: Harmonic generation in Taylor vortices between rotating cylinders. *J. Fluid Mech.* 26, 545-562 (1966)

<sup>c</sup>W. Debler, E. Funer, B. Schaaf: "Torque and Flow Patterns in Supercritical Circular Couette Flow", in Proceedings of the Twelf<sup>th</sup> International Congress of Applied Mechanics, 1968, ed. By M. Hetenyi, W.G. Vincenti (Springer, Berlin, Heidelberg, New York, 1969)

**Table 4** Experiments on the transition to turbulence between concentric cylinders with the inner cylinder rotating ( $\eta \cong 7/8$ )

Radius ratio $\eta$	Aspect ratio $h/(r_o - r_i)$	$R_{c,1}$	$R_{c,2}$	$R_{c,3}$	$R_{c,4}$	References
0.840	50	105.1	$\approx 1051.0$	-	$\approx 1891.8 - 3993.8$	Schultz-Grunow and Hein (1956) <sup>a</sup>
0.874	27.9	117.7	$\approx 1294.7$	-	-	Coles (1965) <sup>b</sup>
0.877	20	119.1	$\approx 1429.2$	-	2608.3	Gollub and Swinney (1975) <sup>c</sup> and Fenstermacher (1979) <sup>d</sup>
0.875	18 to 80	118.2	$\approx 1300.2$	-	$2482.2 - 2955$	Walden and Donelly (1979) <sup>e</sup>
0.880	-	$R_{c,1}$	10.4 $R_{c,1}$	12.3 $R_{c,1}$	$23.50 R_{c,1}$	E.L. Koschmieder (1979) <sup>f</sup> , D. Coles (1965) <sup>b</sup> , P.R. Fenstermacher et al. (1979) <sup>d</sup>
0.909	40	137.8	$\approx 1653.6$	-	2687.1	Bouabdallah and Cognet (1980) <sup>g</sup>
0.896	123	129.1	$\approx 1291.0$	-	3356.6	Koschmieder (1979) <sup>f</sup>
0.908	65	137.1	$\approx 754.1$	-	2879.1	Mobbs et al. (1979) <sup>h</sup> Barcilon et al. (1979) <sup>i</sup>

Note:  $R_{c,1}$  = The critical Reynolds number for Taylor vortex flow

$R_{c,2}$  = The critical Reynolds number for wavy vortex flow

$R_{c,3}$  = The critical Reynolds number for the first appearance of randomness in wavy vortex flow

$R_{c,4}$  = The critical Reynolds number for disappearance of the azimuthal waves and the flow becomes turbulent

$h$  = a height of cylindrical couette cell

$\eta$  = a dimensionless radius ratio =  $r_i/r_o$

- <sup>a</sup>F. Schultz-Grunow, H. Hein: Beitrag zur Couettestromung. *Z. Flugwiss.* 4, 28-30 (1956)
- <sup>b</sup>D. Coles: Transition in circular Couette flow. *J. Fluid Mech.* 21, 385-425 (1965)
- <sup>c</sup>J.P. Gollub, H.L.Swinney: Onset of turbulence in a rotating fluid. *Phys. Rev. lett.* 35, 927-930 (1975)
- <sup>d</sup>P.R. Fenstermacher, H. L. Swinney, J.P. Gollub: Dynamic instabilities and the transition to chaotic Taylor vortex flow. *J. Fluid Mech.* 94, 103-129 (1979)
- <sup>e</sup>R.W. Walden, R.J. Donnelly: Reemergent order of chaotic circular Couette flow. *Phys. Rev. Lett.* 35, 927-930 (1975)
- <sup>f</sup>E.L. Koschmieder: Turbulent Taylor vortex flow. *J. Fluid Mech.* 93, 515-527 (1979)
- <sup>g</sup>A. Bouabdallah, G. Cognet: "Laminar-turbulent transition in Taylor-Couette flow", in Laminar-Turbulent Transition, ed. By R. Eppler and H. Fasel (Springer, Berlin, Heidelberg, New York 1980) pp. 368-377
- <sup>h</sup>F. R. Mobbs, S. Preston, M.S. Ozogun: *An experimental investigation of Taylor vortex waves*. Taylor Vortex Flow Working Party, Leeds (1979)
- <sup>i</sup>A. Barcilon, J. Brindley, M. Leesen, F. R. Mobbs: Marginal instability in Taylor-Couette flow at very high Taylor number. *J. Fluid Mech.* 94, 453-463 (1979)

**Appendix G The number of polymer chains per one eddy at Re = 5000 for poly(ethylene oxide) in aqueous solutions at 30°C**

System	PEO M <sub>w</sub>	c * PEO	$\tau_w$	f	u *	$\mu$	$l_d \times 10^5$	$V_{ed} \times 10^{13}$	$N \times 10^{-6}$	$V_h \times 10^{21}$	$NV_h \times 10^{15}$	% NV_h/V <sub>ed</sub>
PEO1	91,000	-	-	-	-	-	-	-	-	0.0195	-	-
PEO3	304,000	0.05	0.8287	0.0119	0.0288	0.0008	3.9712	0.3278	3.2452	0.1334	0.4328	1.32
PEO6	606,000	0.04	0.3205	0.0046	0.0179	0.0008	6.4127	1.3801	5.4839	0.2464	1.3515	0.98
PEO9	803,000	0.03	0.1446	0.0021	0.0120	0.0008	9.5339	4.5351	10.200	0.4806	4.9019	1.08
PEO20	1,790,000	0.015	0.1444	0.0021	0.0120	0.0008	9.5258	4.5236	2.2820	1.4484	3.3052	0.73

$$\frac{N}{V} = \frac{cN_a}{M_w}$$

$$N = V_{ed} \left( \frac{cN_a}{M} \right)$$

$$l_d = \frac{(\sqrt{2} \cdot v)}{u^*}$$

$$\tau_w = \rho u^{*2}$$

Note: PEO  $M_w$  = PEO molecular weight (g/mol)  
 $c^*$ PEO = the optimum PEO concentration (kg/m<sup>3</sup>)  
 $\tau_w$  = wall shear stress (N/m<sup>2</sup>)  
 $f$  = friction factor  
 $u^*$  = friction velocity (m/s)  
 $\mu$  = solution viscosity (Pa.s)  
 $l_d$  = dissipative length (m)  
 $V_{ed}$  = volume of one eddy (m<sup>3</sup>)  
 $N$  = the number of polymer chains per one eddy  
 $V_h$  = hydrodynamic volume of one chain (m<sup>3</sup>)  
 $NV_h$  = total hydrodynamic volume (m<sup>3</sup>)  
 $NV_h/V_{ed}$  = the ratio of total hydrodynamic volume to  
the volume of one eddy  
 $N_A$  = Avogadro's number  
 $M_w$  = molecular weight of PEO (kg/mol)  
 $\rho$  = density of water at 30°C

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2. Suksamranchit, S., Sirivat, A., and Jamieson, A. M. (2005). Polymer-surfactant complex formation and its effect on turbulent wall shear stress. Accepted and to be published in Journal of Colloid and Interface Science.
3. Suksamranchit , S., Sirivat, A., and Jamieson, A. M. (2005) Influence of Ionic Strength on Complex Formation Between Poly(ethylene oxide) and Cationic Surfactant and Turbulent Wall Shear Stress in Aqueous Solution. Submitted to Journal of Colloids and Surfaces A.
4. Suksamranchit, S., Sirivat, A., and Jamieson, A. M. Effect of Poly(ethylene oxide) and Cationic Surfactant Complex Structure on Turbulent Friction Factor. In preparation
5. Suksamranchit, S., Sirivat, A., and Jamieson, A. M. Influence of Polyethylene Oxide on the Rheological Properties of Semi-Dilute, Wormlike Micellar Solutions of Hexadecyltrimethylammonium Chloride and Sodium Salicylate. To be accepted by J.Colloids and Interface Science.

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1. Suksamranchit, S., Sirivat, A., Jamieson, A.M. (2003, November 24-27) Turbulent drag reduction by poly(ethylene oxide) and cationic surfactant complexes in aqueous solutions. Proceedings of 8<sup>th</sup> Pacific Polymer Conference, Bangkok, Thailand.
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4. Suksamranchit, S., Sirivat A., Jamieson, A.M. (2004, August 10-11) Turbulent drag reduction in aqueous solutions of PEO and cationic surfactant complexes: Effect of polymer concentration, molecular weight, surfactant concentration and ionic strength. Proceedings of MSAT 2004, Bangkok, Thailand.
5. Suksamranchit, S., Sirivat, A., Jamieson, A.M. (2004, October 17-21) Influence of complex formation between PEO and cationic surfactant on turbulent drag reduction in aqueous solution. Proceedings of the 10<sup>th</sup> APCChE 2004, Kitakyushu, Japan.
6. Suksamranchit, S., Sirivat, A., Jamieson, A.M. (2005, July 10-14) Turbulent drag reduction in aqueous solution of complexes between poly(ethylene oxide) and cationic surfactant. Proceedings of the 7<sup>th</sup> World Congress of Chemical Engineering, Glasgow, Scotland.

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- 2.) Suksamranchit, S., Sirivat, A., Jamieson, A.M. Turbulent Drag Reduction in Poly(ethylene oxide) Solution. RGJ-PhD Congress III, Pattaya, Chonburi, Thailand, 25-27 April 2002.
- 3.) Suksamranchit, S., Sirivat, A., Jamieson, A.M. Turbulent Drag Reduction in Poly(ethylene oxide) Solution. Congress on 28<sup>th</sup> Science and Technology of Thailand (STT 28<sup>th</sup>), Bangkok, Thailand, 22-25 October 2002
- 4.) Suksamranchit, S., Sirivat, A., Jamieson, A.M. Influence of Complex Formation on Turbulent Drag Reduction between Poly(ethylene oxide) and Cationic Surfactant in Aqueous Solution. RGJ-PhD Congress V, Pattaya, Chonburi, Thailand, 23-25 April 2004.
- 5) Suksamranchit, S., Sirivat, A., Jamieson, A.M. Turbulent Drag Reduction in aqueous solutions containing Poly(ethylene oxide) and Cationic Surfactant. Graduate Student Seminars, Spring 2005, Cleveland, Ohio, USA, 4 February 2005.