



## CHAPTER III

### Experimental

#### 3.1 Materials

Methyl Butyrate ( $C_3H_7COOCH_3$ , 99%), 4-Heptanone ( $C_3H_7COC_3H_7$ ,  $\geq 98\%$ ), Dibutyl ether ( $C_4H_9OC_4H_9$ , 99%), and Butyl butyrate ( $C_4H_9COOC_4H_9$ ,  $\geq 98\%$ ) were purchased from Aldrich Co., Ltd., Butyric acid ( $C_3H_7COOH$ , 99%) was purchased from Fluka Co., Ltd., Butanal ( $C_3H_7CHO$ , 99%), and n-Butanol ( $C_4H_9OH$ ,  $>99.4\%$ ) were purchased from Sigma-Aldrich Co., Ltd., n-Heptane ( $C_7H_{16}$ , 99.5%) was purchased from Carlo Erba Co., Ltd., n-Octane ( $C_8H_{18}$ , 99%) was purchased from Labscan Asia Co., Ltd. The commercial NiMo/Al<sub>2</sub>O<sub>3</sub> (KF-840, containing 12-16 wt% molybdenum and 3-5 wt% nickel) was supported by PTT Research and Technology Institute, PTT Public Company Limited, Thailand. The commercial 5wt% Pd/C was purchased from Sigma-Aldrich Co., Ltd.

#### 3.2 Equipment

- High pressure packed-bed continuous flow reactor
- Mass flow controller (Brooks instrument 5850E)
- High pressure liquid pump (Waters 515 HPLC)
- Gas chromatograph (HP GC 5890)
- Gas chromatograph (HP GC 6890)
- Back pressure regulator (SIEMENS)
- Oven

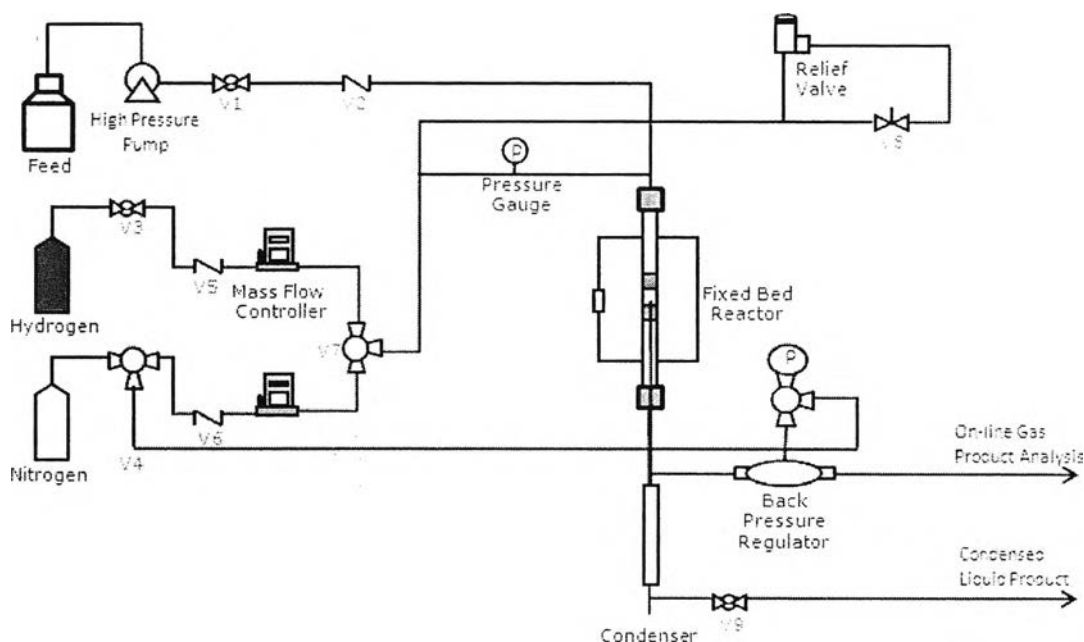
#### 3.3 Methodology

### 3.3.1 Catalyst Pretreatment

The commercial catalyst with particle size 40/20 mesh is placed in the reactor and reduced in a flowing hydrogen at 400 psig for 3.5 h. The temperature is increased with a heating rate of 10 °C/min until reaching the reduction temperature, typically, 200 °C for Pd/C, and 360 °C for NiMo/Al<sub>2</sub>O<sub>3</sub>.

### 3.3.2 Hydrogenation Experiments

The hydrogenations of oxygen-containing C4 compounds are carried out in a 3/4 inch O.D., continuous flow fixed-bed reactor under high pressure conditions. The catalytic activity measurements are conducted by feeding stream of oxygen-containing C4 compound to reactor by using a high pressure pump. The reaction pressure is controlled by a mass flow controller and a back pressure regulator. The liquid product was trapped and collected in a condenser while the gas product was sent directly to sample loop of 10-port valve. Both gas product and liquid product were collected and analyzed hourly. The gas product was injected automatically to a gas chromatograph, Hewlett Packard 5890 equipped with a thermal conductivity detector (TCD) and flame ionization detector (FID). The liquid product was analyzed by a gas chromatograph, Hewlett Packard 6890 equipped with a flame ionization detector (FID).



**Figure 3.1** A schematic flow diagram of high pressure experiment set.

### 3.3.3 Products Analysis

In experiment for oxygen-containing C4 compounds, the composition of gas and liquid products was analyzed qualitatively on-line in interval of 1 h, GC/FID and GC/TCD (HP 5890) is used for gas phase products. While the liquid phase products is analyzed by using GC/FID (HP 6890), The GC operating condition is summarized as follows:

#### For on-line gas phase product:

Injection temperature :	200°C
Detector temperature :	300°C
Carrier gas :	He
Column type :	Packed column

(Hyasep D: diameter 1/8 inch, length 10 m)

Injection temperature : 200°C  
 Detector temperature : 300°C  
 Carrier gas : He  
 Column type : Capillary column  
 (HP-PLOT U: diameter 0.53mm length 30 m)

For liquid phase product:

Injection temperature : 200°C  
 Detector temperature : 270°C  
 Carrier gas : He  
 Column type : Capillary column  
 (Stabilwax: diameter 0.32mm length 30 m)

The following chromatographic temperature program is used for product analysis:

**Table 3.1** The chromatographic temperature program for gas phase product analysis

Step	Temperature (°C)	Rate (°C/min)	Hold time (min)
1	40	-	5
2	180	10	10

**Table 3.2** The chromatographic temperature program for liquid phase product analysis

Step	Temperature (°C)	Rate (°C/min)	Hold time (min)
1	40	-	5
2	180	8	5

For the quantitative calculations of liquid products, n-octane (C<sub>8</sub>H<sub>18</sub>) was used as the standard. The response factors of each product are calculated based on the following formula, as shown in Equation 1:

$$R_x = \left( \frac{m_{is}}{A_{is}} \right) \left( \frac{A_x}{m_x} \right) \quad (1)$$

Where

$R_x$  is response factor of reference substance x

$m_{is}$  is mass in g of internal standard

$m_x$  is mass in g of reference substance x

$A_x$  is peak area of reference substance x

$A_{is}$  is peak area of internal standard

The conversion and product selectivity percentage are calculated by Equations 2 and 3, respectively. Conversion of feed is defined as the moles ratio of C atom in product to moles of C atom in feed, as shown in Equation 2. Selectivity is defined as the moles ratio of C atom of product i to moles of C atom of overall product, as shown in Equation 3.

$$\text{Conversion (\%)} = \frac{\text{moles of C atom in product (wt\%)}}{\text{moles of C atom in feed (wt\%)}} \times 100 \quad (2)$$

$$\text{Selectivity of product i (\%)} = \frac{\text{moles of C atom in product i (wt\%)}}{\text{moles of C atom in overall product (wt\%)}} \times 100 \quad (3)$$