

REFERENCES

- Bice, J-A. E., Paktar, S. D. and Okel, T. A. (1997). Effect of precipitated silicas in truck tire treads. Rubber World, 217, 658-86.
- Blow, C. W. and Hepburn, C. (1982). Raw Plastic Materials. Rubber Technology and Manufacture, 2nd ed. Butterworths: London, 77-80.
- Byers, J. T. and Patel, A. C. (1983). Carbon black's influence on treadwear and hysteresis. Rubber World, 188(3), 21-29.
- Chinpan, N. (1996). Comparison of Rubber Reinforcement using Various Surface Modified Silicas. M.S. Thesis in Petrochemical Technology Program, The Petroleum and Petrochemical College, Chulalongkorn University.
- Dannenbergh, E. M. (1986). Carbon black treadwear ratings from laboratory tests. Rubber Chemistry and Technology, 59, 497-511.
- Demirhan, E., Dincer, S., and Sarac, H. I. (1994). Selection of inorganic fillers for nontire rubber compounding. Polym.-Plast. Technol. Eng., 33(1), 83-88.
- Donnet, J-B. (1998). Black and white fillers and tire compound. Rubber Chemistry and Technology, 71, 323-341.
- Furtado, C. R. G., Nunes, R. C. R., and Filho, A. S. (1995). SBR-mica-silica compositions and their physico-mechanical behaviour. Polymer Bulletin, 34, 627-633.
- Ghosh, A. K., Maiti, S., Adhikari, B., Ray, G. S., and Mustafi, S. K. (1997). Effect of modified carbon black on the properties of natural rubber vulcanisate. Journal of Applied Polymer Science, 66, 683-693.

- González, L., Rodríguez, A., Benito, J. L., and Marcos, A. (1996). A new carbon black-rubber coupling agent to improve wet grip and rolling resistance of tires. Rubber Chemistry and Technology, 69(2), 266-272.
- Katz, H. S., and Milewski, J. V. (1987). Carbon Black. Handbook of Fillers for Plastics, Van Nostrand, 387-419.
- Katz, H. S., and Milewski, J. V. (1987). Synthetic Silica. Handbook of Fillers for Plastics, Van Nostrand, 165-201.
- Koshy, A. T., Kuriakose, B., Thomas, S., and Varghese, S. (1994). Viscoelastic properties of silica-filled natural rubber and ethylene-vinyl acetate copolymer blend. Polym.-Plast. Technol. Eng., 33(2), 149-159.
- Lebanc, J. L. (1997). A molecular explanation for the bound rubber in carbon black filled rubber compounds. Journal of Applied Polymer Science, 66, 2257-2268.
- Leelertsakulwong, A. (1992). Influence of Carbon Black Aggregate Structure on Agglomerate Dispersion Behavior. M.S. Thesis in Polymer Science, The Petroleum and Petrochemical College, Chulalongkorn University.
- Maingam, B. (1994). A Study of Structures-Properties of Rubber Vulcanisate by Dynamic Mechanical Analyzer. M.S. Thesis in Polymer Science, Mahodol University.
- Mark, H. F., Bikales, N. M., Overberger, C., G. and Menges, G. (1989). Carbon Black. Encyclopedia of Polymer Science and Engineering, 2nd ed., John Wiley & Sons, 7, 1037 -1074.
- Mark, H. F., Bikales, N. M., Overberger, C., G. and Menges, G. (1989). Silica. Encyclopedia of Polymer Science and Engineering, 2nd ed., John Wiley & Sons, 7, 977-1032.

- Mark, J. E., Erman, B. and Eiric, F. R. (1994). Dynamic Mechanical Properties. Science and Technology of Rubber, 2nd ed., New York: Academic Press.
- Okel, T. A. and Waddell, W. H. (1994). Silicas properties/rubber performance correlation carbon black-filled rubber compounds. Rubber Chemistry and Technology, 67(2), 217-236.
- Ono, S., Kiuchi, Y., Sawanoburi, J., and Ito, M. (1999). Structure development in silica-filled rubber composites. Polymer International, 48, 1035-1041.
- Pal, P. K., Bhowmick, A. K. and De, S. K. (1982). The Effects of carbon black-vulcanisation system interactions on natural rubber network structures and properties. Rubber Chemistry and Technology, 55, 23-40.
- Prasanleungilai, P. (1997). Influence of Carbon Black Aggregate Structure on Agglomerate Packing Characteristics. M.S. Thesis in Polymer Science, The Petroleum and Petrochemical College, Chulalongkorn University.
- Sau, K. P., Chaki, T. K. and Khastgir, D. (1999). Electrical and mechanical properties of conducting carbon black filled composites based on rubber and rubber blends. Journal of Applied Polymer Science, 71, 887-895.
- Sombatsompop, N. (1998). Dynamic mechanical properties of ground flexible polyurethane foam particles and carbon-black-filled rubber vulcanisates. Polymer-Plastastic Technology Engineering, 37(1), 1-18.
- Tanahashi, H., Osanai, S., Shigekuni, M., Murakami, K., Ikeda, Y. and Kohjiya, S. (1998). Reinforcement of acrylonitrile-butadiene rubber by silica generated *In situ*. Rubber Chemistry and Technology, 71 (1), 38-52.

- Takino, H., Nakayama, R., Yamada, Y., Kohjiya, S., and Matsuo, T. (1997). Viscoelastic properties of elastomers and tire wet skid resistance. Rubber Chemistry and Technology, 70, 584-594.
- Thammathadanukul, V., O'haver, J. H., Osuwan, S., Na-ranong, N. and Waddell, W. H. (1996). Comparison of rubber reinforcement using various surface-modified precipitated silicas. Journal of Applied Polymer Science, 59, 1741-1750.
- Wagner, M. P. (1976). Reinforcing silicas and silicates. Rubber Chemistry and Technology, 49, 703-774.
- Wang, M. J. (1997). Effect of polymer-filler and filler-filler interactions on dynamic properties of filled vulcanisates. Rubber Chemistry and Technology, 71, 520-589.
- Yoshimizu, H. and Asakara, T. (1990). The structure of *bombyx mori* silk fibroin membrane swollen by water studied with ESR, ¹³C-NMR, and FT-IR spectroscopies. Journal of Applied Polymer Science, 40, 1745-1756.

APPENDIX A

Calibration Data for Gel Permeation Chromatography (GPC)

Weight average molecular weight (\bar{M}_w), number average molecular weight (\bar{M}_n) and molecular weight distribution (MWD) of NR were determined by at room temperature gel permeation chromatography, Waters 600E. The column series of HT4 and HT5 were calibrated using narrow MWD polystyrene standard. By using flow rate 1 cm³/min, tetrahydrofuran (THF) was used as a solvent for natural rubber and the polystyrene standard. The temperature of the column was controlled at 35°C and the injection volume was 60 μ l.

Table A1 Retention time of standard polystyrene with known molecular weight at room temperature.

| Retention time (min) | Specified Molecular weight | Calculated Molecular Weight |
|----------------------|----------------------------|-----------------------------|
| 11.77 | 3840000 | 3687753 |
| 11.93 | 2890000 | 2958254 |
| 12.77 | 1090000 | 1159355 |
| 13.41 | 706000 | 688819 |
| 14.61 | 355000 | 338287 |
| 15.78 | 190000 | 191268 |
| 16.98 | 96400 | 100243 |
| 18.36 | 37900 | 38330 |
| 19.31 | 18100 | 16844 |
| 19.90 | 9100 | 9549 |
| 20.37 | 5970 | 5941 |

Curve Type: 4th Order

$$\text{Equation of Curve: } \log \text{ MW} = +7.40\text{E}+01 -1.55\text{E}+01*\text{R} +1.32\text{E}+00*\text{R}^2 \\ -4.99\text{E}-02*\text{R}^3 +6.89\text{E}-04*\text{R}^4$$

where R = retention time (min).

Correlation Coefficient: $r^2 = 0.99964536$

Standard Error of

Estimate: 0.02387588

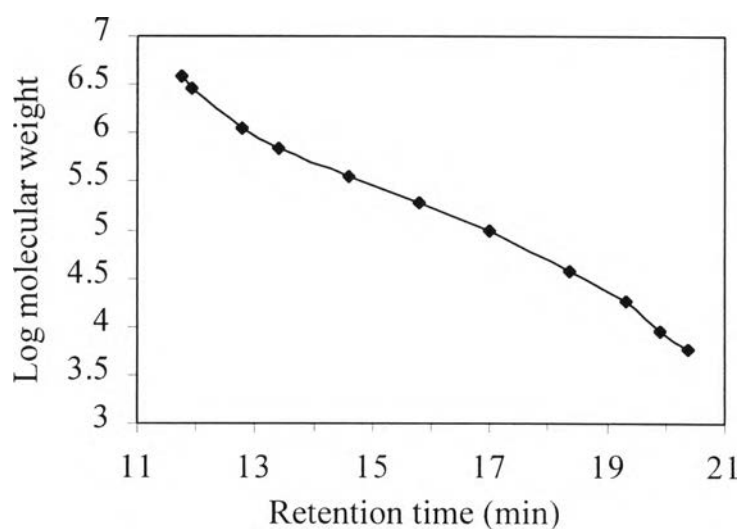


Figure A1 Calibration curve of standard polystyrene in THF at room temperature and flow rate of 1.0 ml/min.

Table A2 Effect of mastication time on molecular weight of NR.

| Mastication time (min) | M_n | M_w | MWD |
|------------------------|--------|---------|--------|
| 0 | 228517 | 1122573 | 4.9124 |
| 5 | 192404 | 582996 | 3.0301 |
| 10 | 183553 | 482715 | 2.6298 |
| 25 | 159783 | 365595 | 2.2881 |

Table A3 Retention time of standard polystyrene with known molecular weight at room temperature for the new lot of NR.

| Retention time (min) | Molecular weight |
|----------------------|------------------|
| 11.532 | 1290000 |
| 12.306 | 520000 |
| 13.237 | 172100 |
| 13.978 | 66000 |
| 15.427 | 10850 |
| 15.965 | 5460 |

$$\log MW = +1.23E+001 -5.37E-001 T^{\wedge}1$$

$$R^{\wedge}2 = 0.999772$$

$$R = 0.999886$$

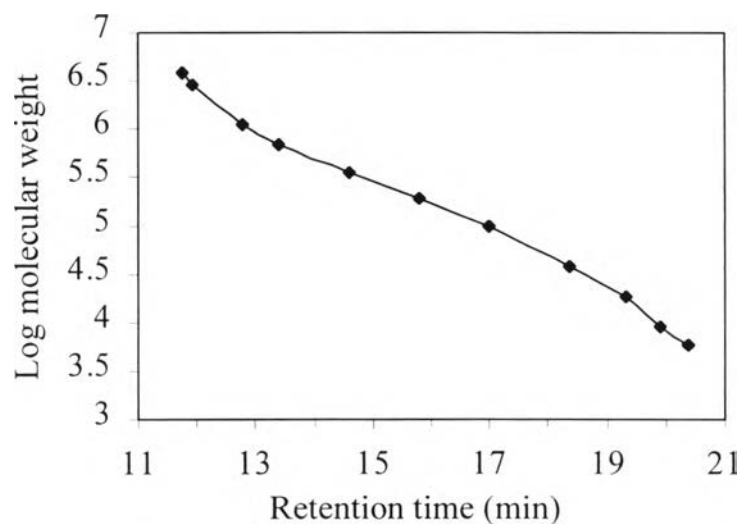


Figure A2 Calibration curve of standard polystyrene in THF at room temperature and flow rate of 1.0 ml/min for the new lot of NR

Table A4 Effect of mastication time on molecular weight for the new lot of NR.

| Mastication time (min) | M_n | M_w | MWD |
|------------------------|--------|---------|----------|
| 0 | 308210 | 2196993 | 7.128241 |
| 5 | 210461 | 1020572 | 4.849218 |
| 8 | 190221 | 786119 | 4.132652 |
| 10 | 205057 | 709579 | 3.460407 |
| 13 | 178759 | 656318 | 3.671518 |
| 15 | 176102 | 619219 | 3.515262 |
| 20 | 179575 | 519975 | 2.895584 |
| 25 | 165806 | 472335 | 2.848722 |

APPENDIX B

Torque-Time-Temperature Relationship of Filled-NR Compounds Prepared by Melt Technique using Brabender Plasticorder

Abbreviations

| | | |
|-----|---|----------------------------------|
| A | : | Loading peak |
| G | : | Inflection point |
| E | : | End |
| B | : | Minimum |
| X | : | Maximum |
| | | |
| A-B | : | Loading peak to Minimum |
| B-X | : | Minimum to Maximum |
| X-E | : | Maximum to End = Fusion time (t) |
| A-X | : | Loading peak to End |

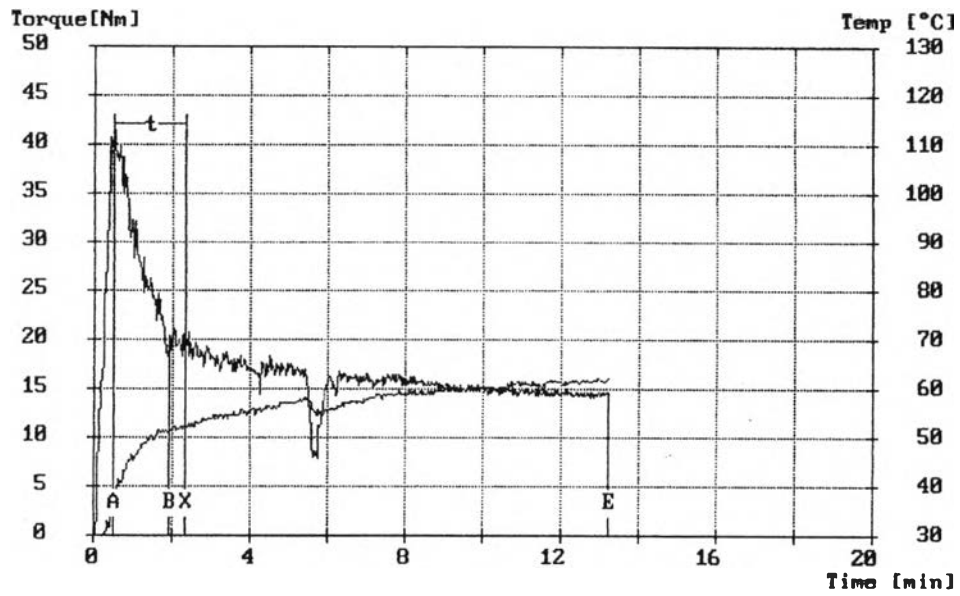


Figure B1 Torque-time-temperature relationship of NR compound

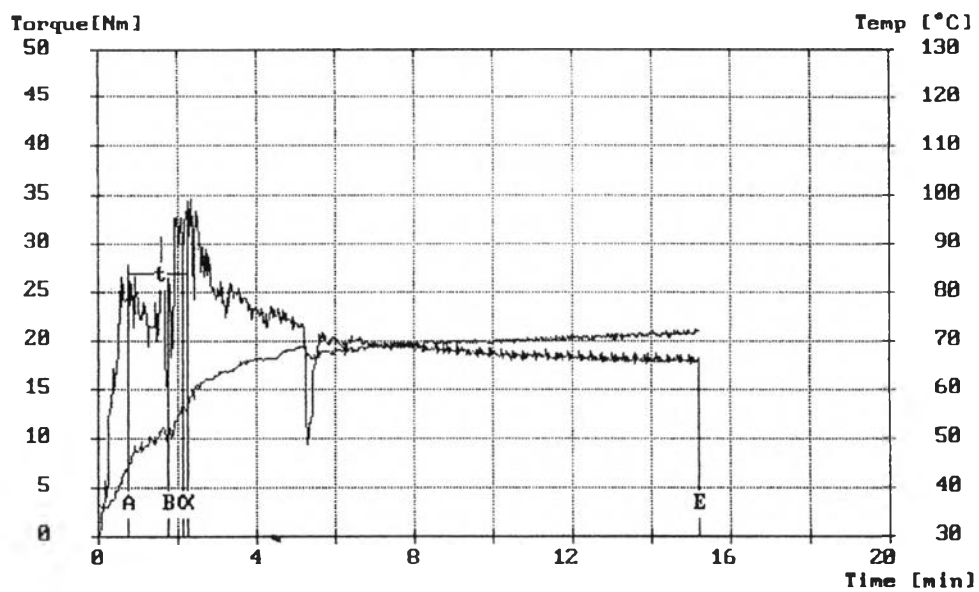


Figure B2 Torque-time-temperature relationship of NR/gypsum compound composition 80/20 in volume fraction

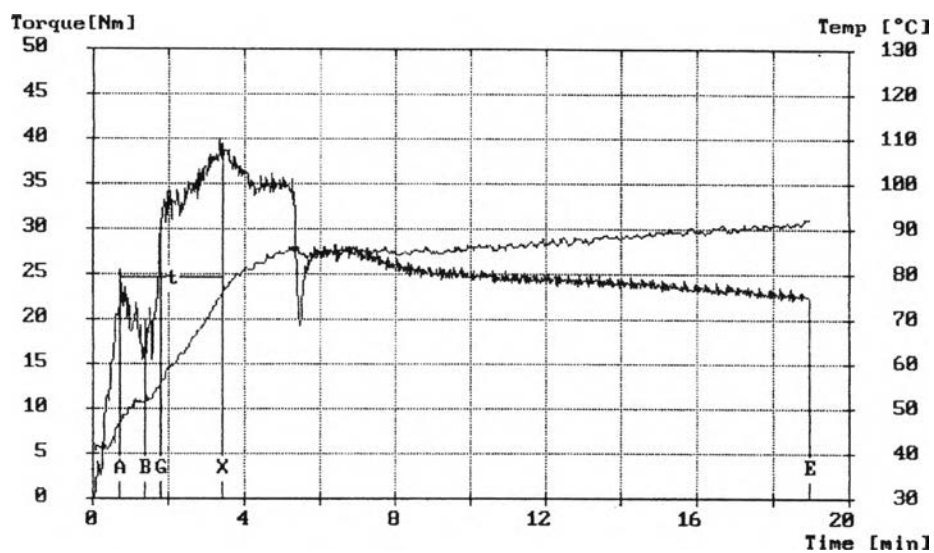


Figure B3 Torque-time-temperature relationship of NR/carbon black (N110) compound composition 80/20 in volume fraction

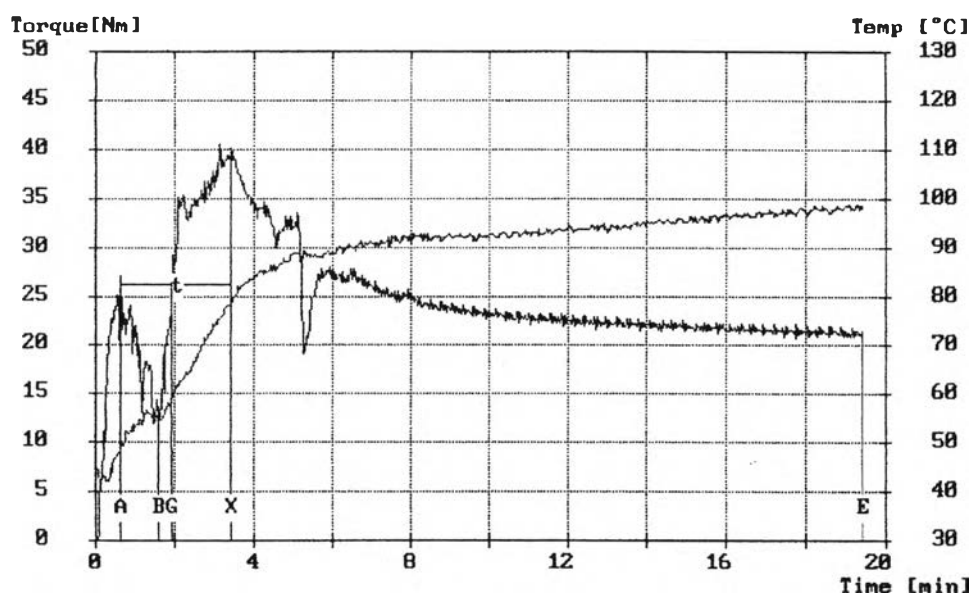


Figure B4 Torque-time-temperature relationship of NR/carbon black (N220) compound composition 80/20 in volume fraction

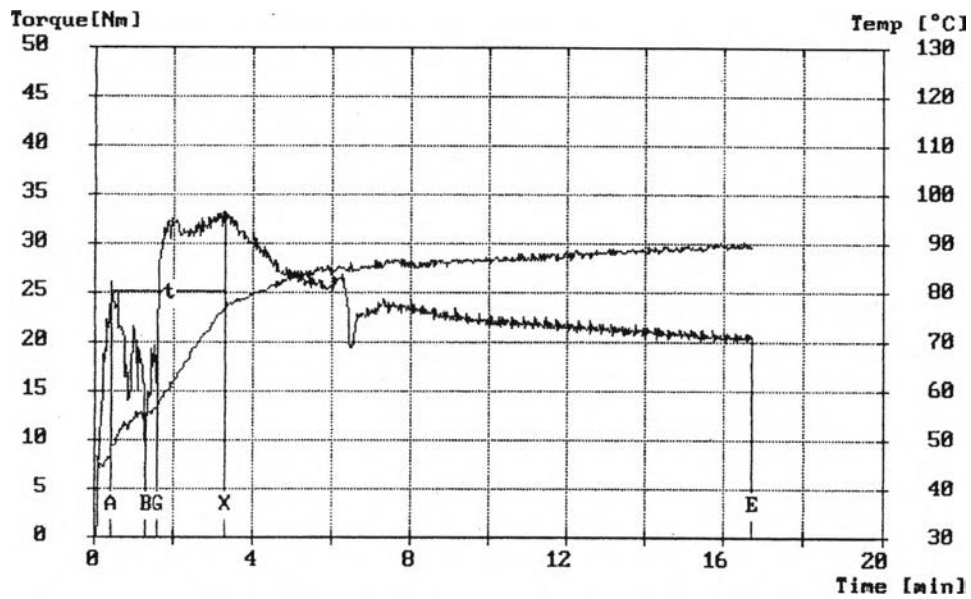


Figure B5 Torque-time-temperature relationship of NR/carbon black (N330) compound composition 80/20 in volume fraction

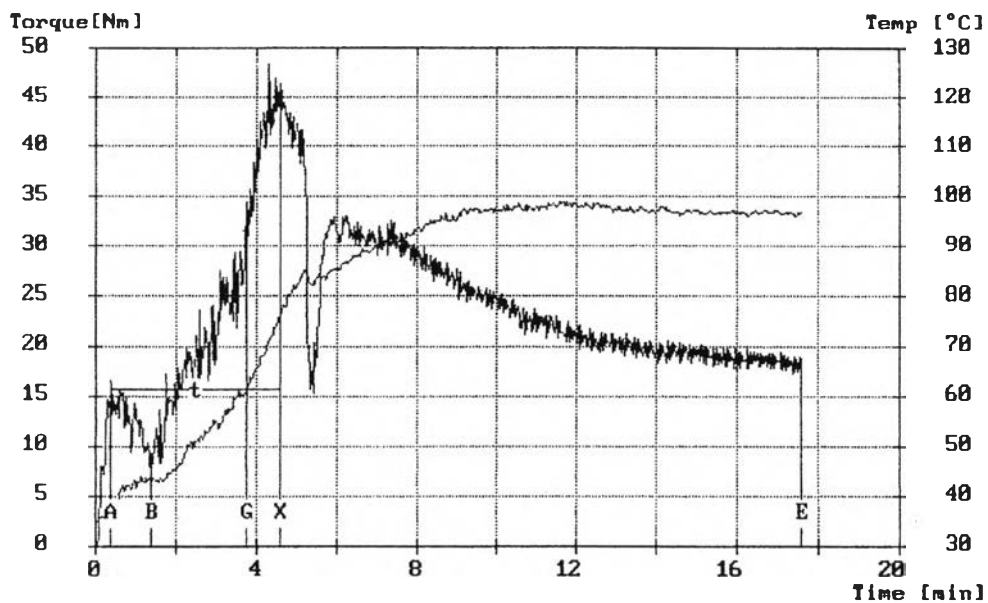


Figure B6 Torque-time-temperature relationship of NR/silica (Hi-Sil927) compound composition 80/20 in volume fraction

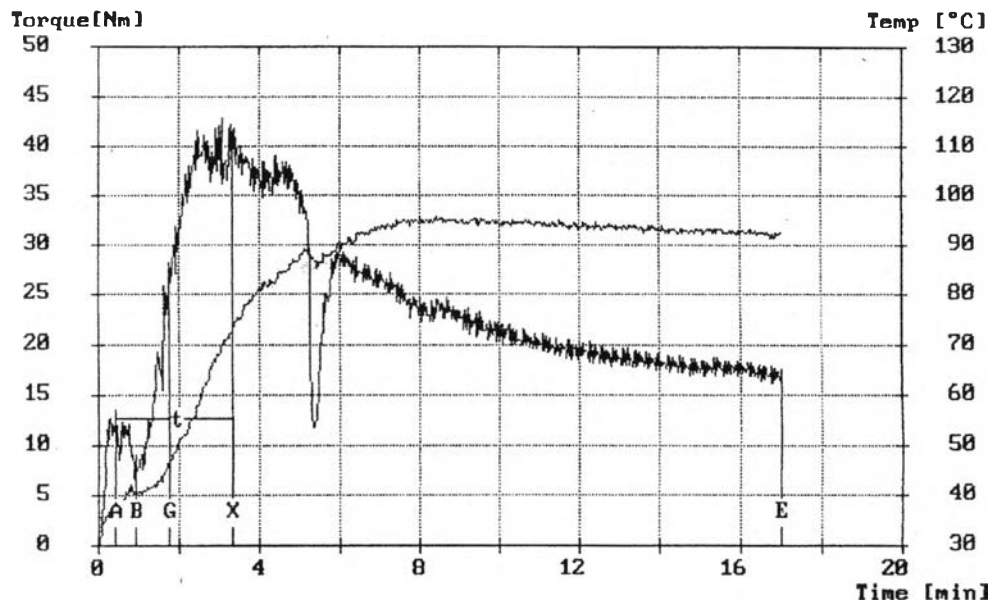


Figure B7 Torque-time-temperature relationship of NR/silica (Hi-Sil255) compound composition 80/20 in volume fraction

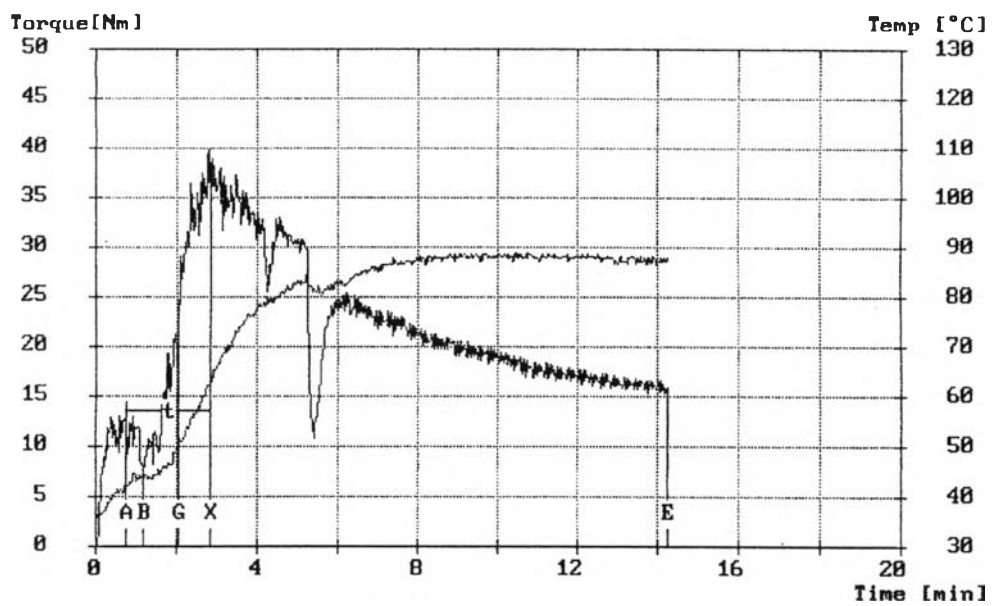


Figure B8 Torque-time-temperature relationship of NR/silica (Ultrasil-VN2) compound composition 80/20 in volume fraction

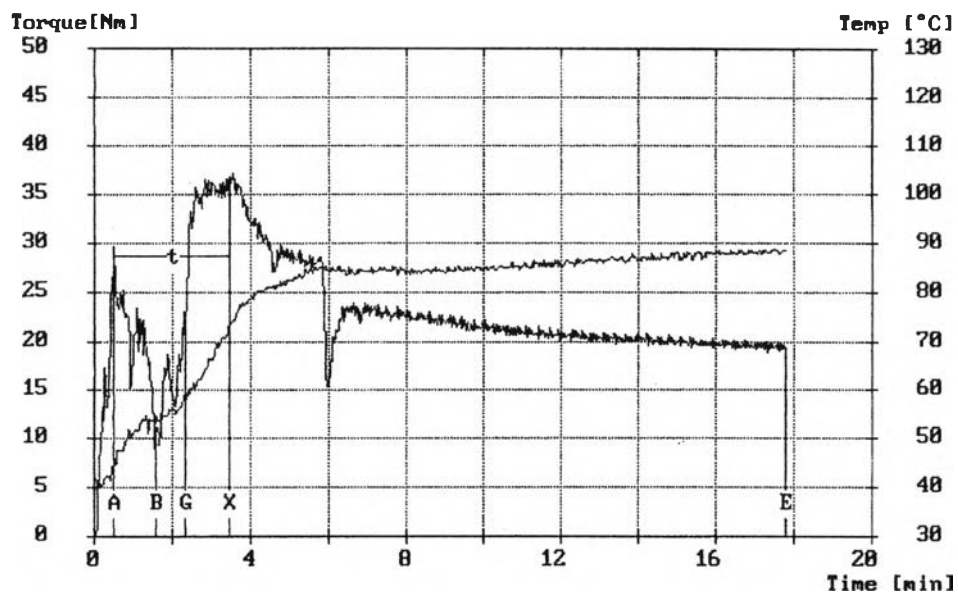


Figure B9 Torque-time-temperature relationship of NR/carbon black/gypsum compound composition 80/16/4 in volume fraction

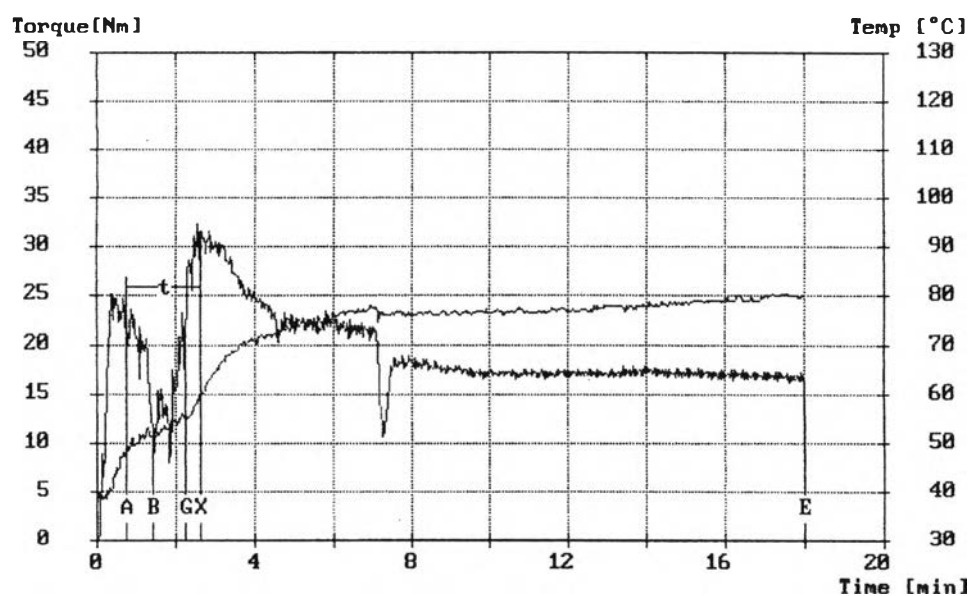


Figure B10 Torque-time-temperature relationship of NR/carbon black/gypsum compound composition 80/12/8 in volume fraction

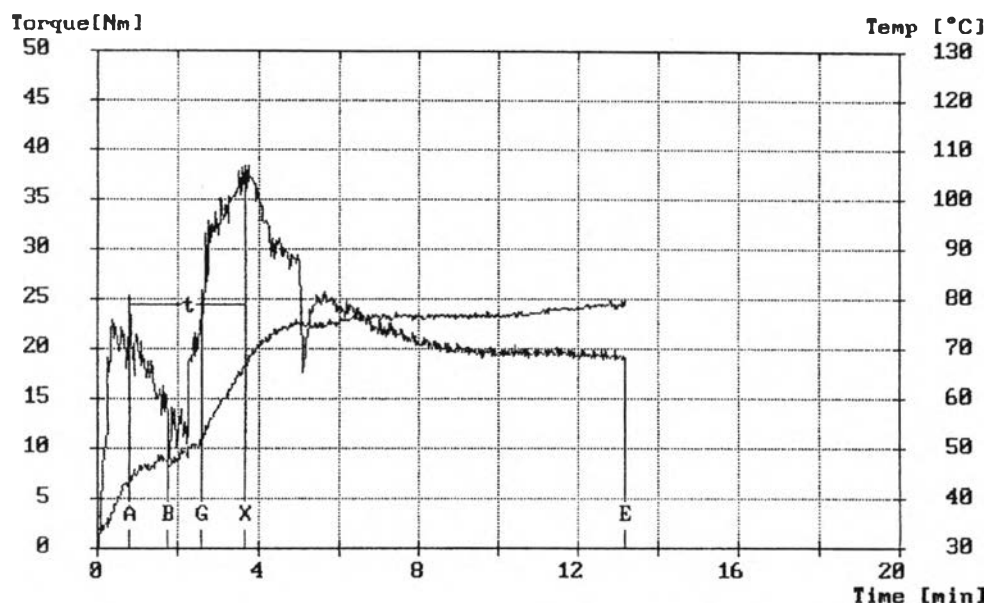


Figure B11 Torque-time-temperature relationship of NR/carbon black/gypsum/silica compound composition 80/16/2/2 in volume fraction

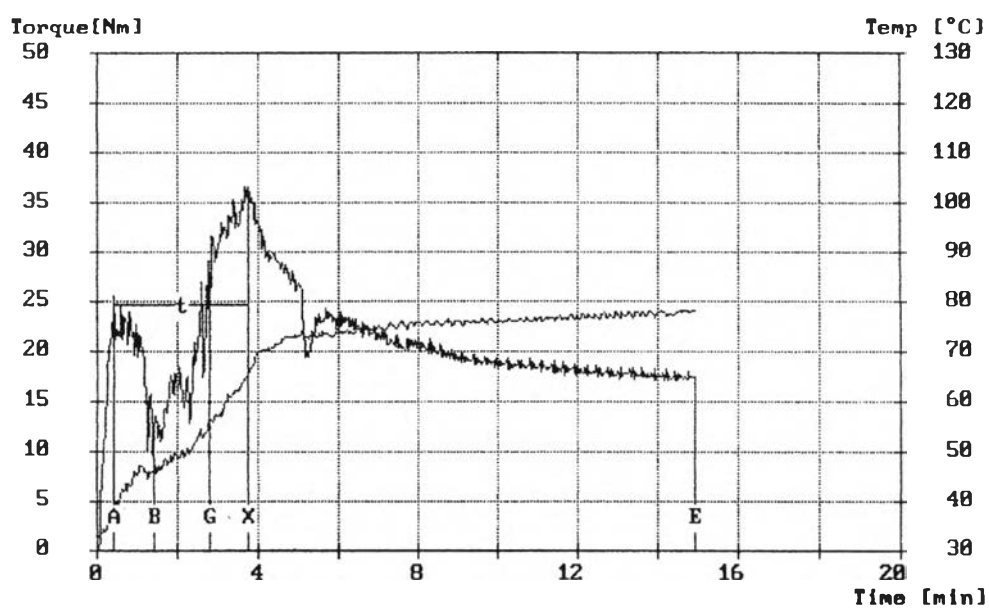


Figure B12 Torque-time-temperature relationship of NR/carbon black/gypsum/silica compound composition 80/12/4/4 in volume fraction

APPENDIX C

Calculation for Amount of Materials that used in Brabender Plasticorder

$$\text{From } D = M/V \quad (C.1)$$

$$\text{Then } D_{\text{total}} = M_{\text{total}}/V_{\text{total}} \quad (C.2)$$

$$\text{And } M_{\text{total}} = (M_x + M_y + M_z + \dots) \quad (C.3)$$

$$V_{\text{total}} = [(M_x/D_x) + (M_y/D_y) + (M_z/D_z) + \dots] \quad (C.4)$$

where D = density of material (g/cm^3)

M = weight of material (g)

V = volume of material (cm^3)

Example of calculation

For carbon black filled-NR compound consists of materials as shown below:

NR has density 0.9 g/cm^3 with loading 100 part

Carbon black has density 1.8 g/cm^3 with loading 50 part

Zinc oxide has density 5.67 g/cm^3 with loading 5 part

Stearic acid has density 0.94 g/cm^3 with loading 2 part

MBTS has density 1.54 g/cm^3 with loading 1.8 part

Sulfur has density 2.08 g/cm^3 with loading 3 part

From

$$D_{\text{total}} = M_{\text{total}}/V_{\text{total}}$$

$$D_{\text{total}} = \frac{[100+50+5+2+1.8+3]}{[(100/0.9)+(50/1.8)+(5/5.67)+(2/0.94)+(1.8/1.54)+(3/2.08)]}$$
$$= 1.1196 \text{ g/cm}^3$$

Due to a chamber of Brabender Plasticorder has volume 80 cm^3 and to achieve a good mixing the materials should be filled in 80 % of chamber volume that is

$$(80 \times 80) / 100 = 64 \text{ cm}^3$$

Then weight of materials that wanted in blending is

$$1.1196 \times 64 = 71.6544 \text{ g}$$

Materials have total amount at 161.8 part = 71.6544 g

$$\begin{aligned} \text{Then NR has 100 part} &= (100 \times 71.6544) / 161.8 \\ &= 44.2858 \text{ g} \end{aligned}$$

$$\begin{aligned} \text{Carbon black has 50 part} &= (50 \times 71.6544) / 161.8 \\ &= 22.1429 \text{ g} \end{aligned}$$

$$\begin{aligned} \text{ZnO has 5 part} &= (5 \times 71.6544) / 161.8 \\ &= 2.2143 \text{ g} \end{aligned}$$

$$\begin{aligned} \text{Stearic acid has 2 part} &= (2 \times 71.6544) / 161.8 \\ &= 0.8857 \text{ g} \end{aligned}$$

$$\begin{aligned} \text{MBTS has 1.8 part} &= (1.8 \times 71.6544) / 161.8 \\ &= 0.7971 \text{ g} \end{aligned}$$

$$\begin{aligned} \text{Sulfur has 3 part} &= (3 \times 71.6544) / 161.8 \\ &= 1.3286 \text{ g} \end{aligned}$$

Volume Fraction

In this thesis, the volume fraction is calculated only from the volume of NR and the volume of each filler or is not including the volume of the other additives such as zinc oxide, stearic acid, MBTS and sulfur.

$$\text{From } V_x = v_x / v_{\text{total}}$$

where V_x = the volume fraction of material x

$$v_x = (m_x / \rho_x) = \text{the volume of material x (cm}^3\text{)}$$

$$v_{\text{total}} = v_x + v_y + v_z + \dots$$

Example of calculation

For carbon black-filled NR compound consists of materials as shown below:

NR has density 0.9 g/cm^3 with loading 100 part

Carbon black has density 1.8 g/cm^3 with loading 50 part

$$\begin{aligned} V_{\text{carbon black}} &= v_{\text{carbon black}} / v_{\text{total}} \\ &= [(50/1.8) / ((50/1.8)+(100/0.9))] \\ &= 0.2 \end{aligned}$$

$$\begin{aligned} V_{\text{NR}} &= v_{\text{NR}} / v_{\text{total}} \\ &= [(100/0.9) / ((50/1.8)+(100/0.9))] \\ &= 0.8 \end{aligned}$$

APPENDIX D

Mechanical Properties Data of Pure and Filled NR Compounds

Each testing was done repeatedly. The average values of all tests are obtained from 3 runs.

Table D1 Tensile strength data of rubber compounds.

| Rubber compound | Tensile strength (MPa) |
|-----------------|------------------------|
| Mix 1 | 19.33 ± 1.43 |
| Mix 2 | 20.59 ± 0.18 |
| Mix 3 | 26.56 ± 0.38 |
| Mix 4 | 27.27 ± 0.52 |
| Mix 5 | 28.96 ± 0.44 |
| Mix 6 | 13.36 ± 0.60 |
| Mix 7 | 12.75 ± 0.34 |
| Mix 8 | 11.79 ± 0.35 |
| Mix 9 | 27.43 ± 0.37 |
| Mix 10 | 26.02 ± 0.66 |
| Mix 11 | 23.22 ± 0.28 |
| Mix 12 | 20.09 ± 0.53 |

Table D2 Elongation at break data of rubber compounds.

| Rubber compound | Elongation at break (%) |
|-----------------|-------------------------|
| Mix 1 | 763.20 ± 16.07 |
| Mix 2 | 616.66 ± 28.47 |
| Mix 3 | 560.05 ± 36.78 |
| Mix 4 | 544.47 ± 14.84 |
| Mix 5 | 524.08 ± 29.13 |
| Mix 6 | 550.70 ± 27.45 |
| Mix 7 | 556.48 ± 23.49 |
| Mix 8 | 576.66 ± 18.45 |
| Mix 9 | 572.68 ± 27.07 |
| Mix 10 | 584.65 ± 45.00 |
| Mix 11 | 602.34 ± 14.03 |
| Mix 12 | 623.84 ± 22.92 |

Table D3 300% Modulus data of rubber compounds.

| Rubber compound | 300% Modulus (MPa) |
|-----------------|--------------------|
| Mix 1 | 3.45 ± 0.02 |
| Mix 2 | 4.17 ± 0.28 |
| Mix 3 | 11.39 ± 1.40 |
| Mix 4 | 15.27 ± 0.92 |
| Mix 5 | 16.64 ± 0.96 |
| Mix 6 | 5.00 ± 0.28 |
| Mix 7 | 5.02 ± 0.23 |
| Mix 8 | 4.23 ± 0.20 |
| Mix 9 | 10.17 ± 0.97 |
| Mix 10 | 8.20 ± 1.31 |
| Mix 11 | 7.97 ± 0.13 |
| Mix 12 | 5.54 ± 0.36 |

Table D4 Hardness data of rubber compounds.

| Rubber compound | Hardness (Shore A) |
|-----------------|--------------------|
| Mix 1 | 39.42 ± 0.19 |
| Mix 2 | 49.04 ± 0.59 |
| Mix 3 | 69.20 ± 0.91 |
| Mix 4 | 68.98 ± 1.75 |
| Mix 5 | 70.72 ± 1.78 |
| Mix 6 | 68.30 ± 3.30 |
| Mix 7 | 69.52 ± 8.47 |
| Mix 8 | 70.04 ± 1.90 |
| Mix 9 | 63.04 ± 3.37 |
| Mix 10 | 62.04 ± 1.95 |
| Mix 11 | 57.44 ± 1.13 |
| Mix 12 | 52.02 ± 0.69 |

Table D5 Resilience data of rubber compounds.

| Rubber compound | Resilience (%) |
|-----------------|------------------|
| Mix 1 | 80.5 ± 6.69 |
| Mix 2 | 77 ± 2.37 |
| Mix 3 | 47 ± 0.53 |
| Mix 4 | 48.31 ± 1.79 |
| Mix 5 | 47.89 ± 3.46 |
| Mix 6 | 49.9 ± 1.46 |
| Mix 7 | 48.1 ± 1.13 |
| Mix 8 | 46.3 ± 0.32 |
| Mix 9 | 47.9 ± 0.55 |
| Mix 10 | 48.6 ± 0.04 |
| Mix 11 | 49.04 ± 0.4 |
| Mix 12 | 49.46 ± 0.54 |

Table D6 Abrasion loss data of rubber compounds.

| Rubber compound | Abrasion loss (mm ³) |
|-----------------|----------------------------------|
| Mix 1 | 81.01 ± 6.69 |
| Mix 2 | 73.13 ± 4.68 |
| Mix 3 | 48.31 ± 5.58 |
| Mix 4 | 43.6 ± 5.58 |
| Mix 5 | 43.0 ± 5.53 |
| Mix 6 | 65.91 ± 10.88 |
| Mix 7 | 75.97 ± 5.48 |
| Mix 8 | 84.03 ± 5.39 |
| Mix 9 | 48.31 ± 5.58 |
| Mix 10 | 57.97 ± 5.58 |
| Mix 11 | 49.6 ± 5.73 |
| Mix 12 | 70.07 ± 5.78 |

Table D7 Tan delta data of rubber compounds.

| Rubber compound | G' (N/m ²) | G''(N/m ²) | Tan delta |
|-----------------|---|---|---------------------|
| Mix 5 | $4.15 \times 10^9 \pm 1.20 \times 10^6$ | $3.85 \times 10^8 \pm 1.13 \times 10^4$ | 0.0927 ± 0.0216 |
| Mix 9 | $5.39 \times 10^9 \pm 4.38 \times 10^6$ | $3.70 \times 10^8 \pm 3.04 \times 10^4$ | 0.0687 ± 0.0095 |
| Mix 10 | $2.09 \times 10^9 \pm 7.07 \times 10^3$ | $6.06 \times 10^7 \pm 58.05$ | 0.0290 ± 0.0185 |
| Mix 11 | $2.21 \times 10^9 \pm 1.14 \times 10^4$ | $1.99 \times 10^8 \pm 1.41 \times 10^3$ | 0.0899 ± 0.0182 |
| Mix 12 | $2.47 \times 10^9 \pm 7.07 \times 10^3$ | $1.44 \times 10^8 \pm 7.07 \times 10^2$ | 0.0582 ± 0.0047 |

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